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Coordinate Conversion Technique for OTH
Backscatter Radar,

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TERENCE J. ELKINS
JOSEPH GIBBS

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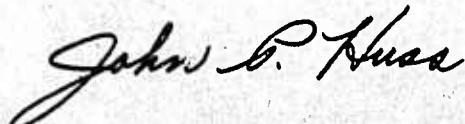
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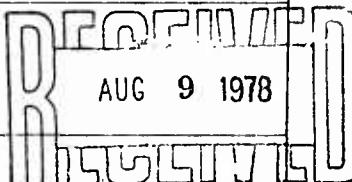
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FOR THE COMMANDER:



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20 ABSTRACT (Continue on reverse side if necessary and identify by block number) A radio propagation simulation computer program, known as WIMP (World-Wide Ionospheric Modelling Program), has been studied and documented. The purpose of the program is to permit the transformation from Over-The-Horizon (OTH) Backscatter radar coordinates to geographic coordinates, given a vertical incidence and a backscatter ionogram measured at the radar site. The program consists of a three-dimensional ionospheric modelling algorithm, which contains a provision for updating on the basis of the ionograms, followed by a ray-tracing procedure. These algorithms have		

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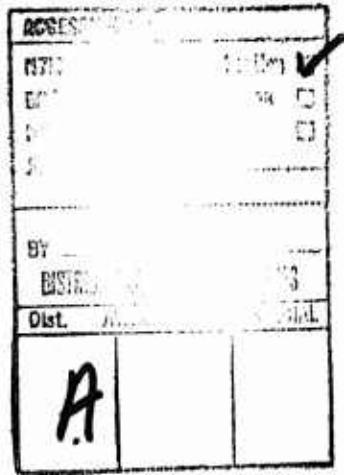
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been deduced from a program source deck and the program structure has been documented in terms of mathematical algorithms and flow charts, together with program listings.

The algorithms have been compared with others in use at RADC and quantitative results of this comparison are presented. These consist of ionospheric model comparisons for representative ranges of the model parameters. Finally, a measured backscatter ionogram is simulated, using the RADC program, and the ionospheric structure along the sounder boresight is deduced.

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Coordinate Conversion Technique for OTH Backscatter Radar

1. INTRODUCTION

The WIMP Program is a complex algorithm which purports to permit accurate conversion from radar target range coordinates to geographic target coordinates in OTH Backscatter HF radar applications; the complexity is fundamentally due to a deeply developed iterative and reiterative algorithm that ultimately involves the user. The program consists of three main components:

- (a) A set of subprograms which construct a three-dimensional three-layer ionospheric model.
- (b) A set of subprograms which simulate HF radio wave propagation in the ionosphere constructed in (a).
- (c) One of three driving programs controlling the calling sequence to the radio wave propagation simulator in (b); these driving programs perform the following tasks: (1) From a given ionosphere, generate the leading edge of a simulated oblique ionogram including scale factors to the F_2 -layer parameters to force agreement with a given vertical ionogram; (2) from a comparison of the simulation in (1) to a given oblique ionogram generate range gradient factors to apply to $f_0 F_2$ and $M(3000)F_2$ to force agreement; (3) from the final ionosphere generated in (1) and (2), simulate predicted radio frequency propagation paths, from which range vs group path functions may be tabulated.

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We first describe in some detail the WIMP three-dimensional three-layer ionospheric model, followed by a general description of the radio wave propagation simulation subprogram (ray-tracing algorithm). A functional description is given of the three driving programs; the operating instructions for their use are included next.

Program block diagrams, flow charts, and program listings are included in Appendixes A, B, and C.

Comparisons have been made of the results of the WIMP ray tracings with techniques developed at RADC. The description and results of these studies are reported in Sections 19 through 21.

2. THE WIMP 3-D IONOSPHERIC MODEL

A complete three-dimensional ionospheric model generally consists of three fundamental aspects: (1) How many distinct layers are to be included, (2) How shall the layer parameters be modelled, (3) How shall the electron density profile be erected from the modelled parameters? A collateral question, equally important is, what ray-tracing technique is to be used, that is, which aspect dominates the simulation of HF propagation? To put the following discussion in proper perspective the latter question will be considered here in general, reserving a more detailed treatment to a latter section.

The WIMP ray-tracing algorithm, SUBROUTINE TRISL, is a control point technique based on layer parameters as in the ITS-78 program¹ and the DEVAN program.^{2,3} The treatment of gradients of electron density, however, differs: ITS-78 does not consider gradients explicitly, DEVAN constructs an equivalent tilted reflecting surface from variations in virtual height, while WIMP constructs the tilt of the reflecting layer from the gradients of electron density. The predictions of the WIMP model are primarily sensitive to the layer parameter predictions, and only weakly sensitive to the electron density profile model. This latter dependence only enters the calculation at the reflection point (which generally is within the F_2 layer), and involves the horizontal gradients of the electron density which are determined primarily by the gradients of the F_2 -layer parameters.

The WIMP model ray tracing considers three distinct layers, E , F_1 , and F_2 ; an optional D-layer tail may be appended to the E layer. The E -layer critical

1. Barghausen, A. F., et al (1969) Predicting Long-Term Operational Parameters of High-Frequency Sky-Wave Telecommunication Systems, ESSA Technical Report ERL 110-ITS-78, Institute for Telecommunication Sciences, Boulder, CO.
2. Beckwith, R. I., Bailey, A. D., and Rao, N. N. (1972) An Investigation of Directional Propagation Effects in High-Frequency Radio Source Location, RRL Publication No. 409.
3. Beckwith, R. I. (1973) A Computer Program for the Rapid Prediction of Angles of Arrival of HF Radio Waves, RRL Publication No. 442.

frequency is determined from the local solar zenith angle. The model employed for the latter is sufficiently unique to describe in some detail below. The F_1 critical frequency is 25 percent larger than $f_o E$ with an additional 0.5 MHz.

The ITS model provides predictions for the F_2 critical frequency and $M/3000$ factor. These parameters may be modified by ad hoc scale factors to force agreement with a given vertical ionogram, and ad hoc gradient factors to force agreement with a given oblique ionogram. The F_2 semithickness is determined from a linear sunspot model. All parameters thus far mentioned are used to generate the F_2 -layer height.

The F_1 layer is fitted between the E and F_2 layers such that the F_1 bottom coincides with the E-layer height and the F_1 -layer height coincides with the F_2 -layer bottom.

A more detailed description of the layer parameters and electron density model follows.

3. MODEL FOR SOLAR ZENITH ANGLE

The model for $f_o E$ requires the solar zenith angle. From the law of cosines of a spherical triangle, this quantity is given by:

$$\cos Z = \sin \delta \sin \theta + \cos \delta \cos \theta \cos (\phi - \phi_s) , \quad (1)$$

where

Z is the solar zenith angle,
 δ is the solar declination (=latitude of the subsolar point),
 ϕ_s is the east longitude of the subpolar point,
 θ is the geographic latitude of the field point,
 ϕ is the east longitude of the subsolar point.

The field point (θ, ϕ) is given, and the subsolar point (δ, ϕ_s) is required.

The subsolar point may be determined from the solution of the Kepler problem using mean elements from the American Ephemeris and Nautical Almanac. Such a solution, to second order in the eccentricity of the earth's orbit and neglecting lunar perturbations, produces an ephemeris accurate to within a nautical mile.

Alternatively, a simplified model for the solar ephemeris may be constructed, accurate to one degree of arc, as follows:

$$\begin{aligned} \delta &= E \sin \Lambda, \quad \Lambda = 2\pi(d-80)/365.25 , \\ \phi_s &= \pi - UT , \end{aligned} \quad (2)$$

where, E is the obliquity of the earth's equator ($= 23.45^\circ$), Λ is the mean longitude of the sun measured in the ecliptic counterclockwise from the first point of Aries, UT is the universal time, and d the day of year.

Clearly, models between these two may be constructed; in particular, the annual variation of the equation of time may be modelled as a correction to the subsolar longitude. (The equation of time is the correction to be added to "sundial time" to reduce it to local mean time.) Such an approach is used in the WIMP program, with the following algorithm implemented in subroutine PTHP each time it is called. The solar declination ("zenith correction angle for day of year") is approximated by:

$$\delta' = E \sin(2\pi(d-82.5)/364). \quad (3)$$

The equation of time in hours is modelled by:

$$X_j = a Y^x [A_1/(B_1 + X_1)] - [A_2/(B_2 + X_2)], \quad (4)$$

where

$$\begin{aligned} a &= 0.0235 \text{ hours;} \\ Y &= +1., X_2 = d + 21., \quad 0.0 < d < 162.5; \\ Y &= -1., X_2 = 344.5 - d, \quad 162.5 \leq d < 344.5; \\ Y &= +1., X_2 = d - 344.5, \quad 344.5 \leq d < 366.5; \\ X_1 &= (X_2/45.)^3; \\ A_1 &= 64., \quad A_2 = 240., \quad B_1 = 4., \quad B_2 = 15. \end{aligned}$$

The following angle is defined, X_j being converted to radians:

$$D = \phi' + X_j - \phi, \quad (5)$$

where

$$\phi' = \pi - UT, \quad UT \geq \pi,$$

$$\phi' = \pi + UT, \quad UT < \pi.$$

The following approximation to the solar zenith angle is constructed:

$$Z_a^2 = [(D * \cos(0.6(\phi + \delta')))]^2 + (\theta - \delta')^2, \quad (6)$$

and the cosine of the solar zenith angle is approximated by:

$$\cos Z = \cos (0.932 Z_a) . \quad (7)$$

In the above description, angles are considered in radians, including UT; furthermore, longitudes are conventionally taken to be positive east. In the coding of PTHP, angles are conventionally in degrees, UT in hours, and longitudes are positive west.

4. MODEL FOR THE E-LAYER PARAMETERS

The E-layer critical frequency f_E , layer height h_E , semithickness y_E , and bottom altitude h_b are required. If the simple parabolic E-layer model is selected,

$$\begin{aligned} h_b &= 100 \text{ km,} \\ h_E &= 115 \text{ km,} \\ y_E &= 15 \text{ km.} \end{aligned} \quad (8a)$$

If, on the other hand, the "parabolic E- with D-layer tail" electron density model is selected,

$$\begin{aligned} h_b &= 100 - 4. F_1 F_2, \\ h_E &= 115 \text{ km,} \\ y_E &= h_E - h_b. \end{aligned} \quad (8b)$$

where

$$\begin{aligned} F_1 &= 1 - (1 - R/3000)^2 & R < 6000 \text{ km;} \\ F_1 &= 0 & R \geq 6000 \text{ km;} \\ F_2 &= \cos(A) & A < \pi/2; \\ F_2 &= 0 & A \geq \pi/2; \\ R &= \text{DIST}(\theta, \phi, 76.0^\circ \text{ N}, 102.0^\circ \text{ W}); \\ A &= \phi + \frac{1}{2} |t - \pi| - \frac{1}{2} \pi; \end{aligned}$$

and (θ, ϕ) is the geographic north latitude and east longitude of the field point; DIST is the great circle distance (in km) between the two points specified in the argument list.

The critical frequency f_E is modelled from the sunspot number N_s and the cosine of the solar zenith angle $\cos Z$ [as modelled by Eq. (7)]. Let

$$C_1 = \frac{1}{4} (1 + \cos Z)^2, \quad S_1 = (1 + 0.004 N_s)^{\frac{1}{2}}.$$

$$f_n = 0.75 S_1 C_1, \quad f_x = 3.17 S_1 (\cos Z)^a, \quad (9a)$$

$$f_d = (f_x^2 + f_n^2)^{\frac{1}{2}}, \quad a = 1/3.775.$$

Then, at night ($\cos Z$ negative) f_E is given by f_n ; during the day ($\cos Z$ positive) f_E is given by f_d , unless f_d exceeds f_2 ($f_o F_2$ as modelled by the ITS-78 model) in which case f_n is taken. Furthermore, f_E is constrained not to exceed

$$f_{E \max} = (0.99 f_2 - 0.5)/1.26. \quad (9b)$$

5. MODEL FOR THE F_1 -LAYER CRITICAL FREQUENCY

The F_1 -layer critical frequency f_1 is given by

$$f_1 = 0.5 + 1.26 f_E, \quad (10)$$

(10)

and is constrained [Eq. (9b)] not to exceed $0.99 f_2$.

6. MODEL FOR $f_o F_2$ AND $M(3000)F_2$

These two parameters, f_2 and M_3 , are given by the ITS-78 parameter prediction model. This model is sufficiently well known that it will not be described in detail herein. Generally, the model consists in reducing a set of coefficients for each modelled parameter to a given phase of the solar cycle, season of the year, universal time, and geographic position. The solar cycle is represented by the sunspot number, and the parameters are fitted to a first or second order polynomial. The seasonal variation of the various parameters is represented by different sets of coefficients for each month, except for $f_o F_2$. The latter is represented as a Fourier sum (9 terms) in the day of the year. The diurnal variation is represented by a Fourier expansion (up to 13 terms) and the global variation is represented by a (modified) spherical harmonic expansion. Parameters modelled are $f_o F_2$, $M(3000)F_2$, $h_b F_2$, $f_o E$, upper decile $f_o E_s$, median $f_o E_s$, and the lower decile $f_o E_s$. Only the first two parameters are used herein.

7. MODEL FOR THE F_2 -LAYER SEMITHICKNESS

The F_2 -layer semithickness y_2 is given by

$$y_2 = F_y (56 + 0.489 N_s). \quad (11)$$

The model allows for a correction scale factor F_y , which is initialized to unity; no provision is made for its redefinition.

8. MODEL FOR THE F_2 -LAYER HEIGHT

The model employed for the construction of the F_2 -layer height uses all of the parameters thus far described: f_E , f_1 , f_2 , M_2 , y_2 , h_b , h_m . The following frequencies are defined:

$$\begin{aligned} f'_q &= f_2 - \frac{1}{4} (f_2 - f_1), \\ f''_q &= f_2 - 0.01 f_2 y_2, \\ f_q &= \max (f'_q, f''_q), \\ f_3 &= f_2 M_3, \\ f_o &= 4 f_q - 3 f_2, \\ f_a &= f_o + 3.78 f_E + 1.5, \\ f_b &= 1.26 f_E + 0.5, \\ f_c &= f_o + 8.82 f_E + 3.5, \\ f_d &= f_o - 1.26 f_E - 0.5 = f_o - f_1, \\ f_e &= 8.00 f_E, \\ f_f &= f_o + 7.78 f_E + 1.5, \\ f_h &= f_o - 0.22 f_E + 1.5, \\ f_i &= f_2 + f_q, \\ f_j &= f_2 - f_q. \end{aligned} \quad (12)$$

The following parameters are defined (these are stored for later use in the construction of the $M(3000)F_2$ correction factor):

$$\begin{aligned} H_3 &= 70 + 3100 (f_q/f_3)^2, \\ F_q &= f_q/f_2, \end{aligned} \quad (13)$$

$$P_3 = (f_a/f_b) \log (f_c/f_d),$$

$$Z_1 = y_E (f_a/f_e) \log (f_f/f_h),$$

$$Z_2 = \frac{1}{2} y_2 (f_q/f_2) \log (f_i/f_j).$$

The F_2 -layer height is given by:

$$h_2 = 8.0 (H_3 - Z_1 - Z_2 - h_b)/P_3 + y_2 + h_E. \quad (14)$$

9. MODEL FOR THE F_1 -LAYER HEIGHT AND SEMITHICKNESS

The F_1 -layer height h_1 and semithickness y_1 are given by:

$$h_1 = h_2 - y_2, \quad (15)$$

$$y_1 = h_1 - h_E.$$

10. MODEL FOR F_2 -LAYER CORRECTION FACTORS – VERTICAL IONOGRAM

The following information had been extracted from a vertical incidence ionogram as input to the program from which correction factors to the F_2 layer parameters are to be derived:

- t_r – universal time of ionogram,
- L_r – geographic north latitude of sounding station,
- W_r – geographic west longitude of sounding station,
- F_1 – $f_o F_1$ from ionogram,
- F_2 – $f_o F_2$ from ionogram,
- $F_q = F_1 + \frac{1}{4} (F_2 - F_1),$
- $F'_q = F_2 - \frac{1}{4} (F_2 - F_1),$
- H_v – F_2 virtual height at frequency F_q ,
- H'_v – F_2 virtual height at frequency F'_q ,
- N_s – sunspot number,
- D_y – day of year.

The ionospheric parameters at the given event are constructed from the parameter prediction model; let these parameters be represented by the following notation:

f_E , f_1 , f_2	— critical frequencies,
h_E , h_1 , h_2	— layer heights,
y_E , y_1 , y_2	— semithickness,
h_b	— bottom of ionosphere,
M_3	— $M(3000)F_2$,
f_q	— "quarter point frequency", Eq. (14),
Z_1 , Z_2 , P_3	— Eq. (15) parameters.

Define the following frequencies:

$$\begin{aligned}
 f'_q &= f_1 + \frac{1}{4}(f_2 - f_1), \\
 f_a &= f_2 + 3.78 f_E + 1.5, \\
 f_c &= f_2 + 8.82 f_E + 3.5, \\
 f_d &= f_2 - f_1, \\
 f_f &= f_2 + 7.78 f_E + 1.5 \\
 f_h &= f_2 - 0.22 f_E + 1.5, \\
 f_i &= f_2 + f'_q, \\
 f_j &= f_2 - f'_q.
 \end{aligned}$$

Define the following quantities:

$$\begin{aligned}
 Z'_1 &= (y_E/8)*(f_a/f_E)* \log(f_f/f_h), \\
 Z'_2 &= (y_2/2)*(f'_q/f_2)* \log(f_1/f_j), \\
 P'_3 &= (f_a/f_1)* \log(f_c/f_d), \\
 H'_3 &= (P'_3/P_3)*(H_v - Z'_1 - Z'_2 - h_b) + Z_1 + Z_2 + h_b, \\
 M'_3 &= (f'_q/f_2)*(3100/H'_3 - 70)^2.
 \end{aligned}$$

Then the correction factors R_f and R_m purporting to correct predicted $f_0 F_2$ and $M(3000)F_2$ parameters are given by:

$$\begin{aligned}
 R_f &= F_2/f_2, \\
 R_m &= M'_3/M_3.
 \end{aligned} \tag{16}$$

11. MODEL FOR F_2 -LAYER CORRECTION FACTORS - OBLIQUE IONOGRAM

Factors FR and MR are calculated in one run of the OBLFACT program, and are used as input for the next run of OBLFACT to be stored in elements 3 and 5 of /PERTC/. The reference point is also input directly into elements 1 and 2 of /PERTC/; the remaining elements are established by DATA statements. In the following description, the elements of /PERTC/ are referenced by the elements of (C_i ; $i = 1, 16$). The field point north latitude and west longitude (N, W) are arguments of PERTC, the algorithm for the calculation of the oblique correction factors. The reference latitude and longitude, C_1 and C_2 , are alternatively referenced as N_r and W_r , respectively.

The algorithm commences by computing the distance and azimuth to the field point (N, W) from the reference point (N_r, W_r); let these two quantities be D and Z_o , respectively.

Define the following quantities:

$$\begin{aligned} Z &= Z_o - C_{16}, \\ Z_1 &= (\pi/180)*(C_{13} - C_{12} - 90), \\ S &= \csc(Z_1), \\ Y &= 3600 C_9 C_{11} S, \\ W &= C_{10} S \\ Z_2 &= (\pi/180)*((D + Y)/360 W), \\ X &= \sin(Z_2). \end{aligned}$$

The following correction factors are then calculated:

$$R_a = (1 + C_i X) * (1 + C_j D/C_k) * (1 + C_m Z) \quad (17)$$

where the $f_o F_2$ and $M(3000)F_2$ corrections are specified by the index set (a; i, j, k, m) being assigned values (f; 7, 3, 4, 14) and (m; 8, 5, 6, 15), respectively. These factors are then applied to the appropriate F_2 -level parameter.

12. ELEMENTS OF COMMON BLOCK/PERTC/

This common block is linked to the INPUT file via NAMELIST inputs in the main programs MAIN and FTDBLB; OBLFACT links elements of NAMELIST input (FRO and MRO) as arguments of subroutines SKIP and/or PEAK; the latter two routines

then define elements 3 and 5 of /PERTC/ equal to FRO and MRO, respectively. OBLFACT also links the first two elements NLREF and WLREF to the input NAMELIST. All elements are assigned default values in a BLOCK DATA program; presumably, these defaults may be assigned different values by replacing the BLOCK DATA program. The elements of /PERTC/ are used by SUBROUTINE PERTC which computes additional corrections to $f_o F_2$ and $M(3000)F_2$ based on information extracted from an oblique ionogram. The reference point (NLREF, WLREF) is the same reference point used in the construction of the updating correction factors to $f_o F_2$ and $M(3000)F_2$ effected in SUBROUTINE FACTO.

Table 1. The Elements of /PERTC/ with the Mnemonic Names Used in PERTC and the Default Values Assigned in the BLOCK DATA Program

Element	Mnemonic	Default	Element	Mnemonic	Default
1	NLREF		2	WLREF	
3	FR	0.0	4	FD	1000.0
5	MR	0.0	6	MD	1000.0
7	FZ	0.0	8	MZ	0.0
9	DUT	0.0792	10	DW	148.5
11	X	0.225	12	GAMMA	180.0
13	AZM	38.808	14	DFAC	0.0
15	DMAC	0.0	16	AZREF	0.0

13. ELECTRON DENSITY MODEL

A continuous electron density profile is constructed from the predicted ionospheric parameters. Slope discontinuities may occur in the model at the critical points of the profile. The model allows for either a parabolic model for the lower E-layer (below the critical altitude) or an E-layer with a D-layer tail; these two models will be described first.

In the parabolic E-layer model, the base altitude, layer height, and semi-thickness are modelled to be 100, 115, and 15 km, respectively. Below the E-layer height h_E , the electron density N_e is given by:

$$N_e = 12400 f_E^2 (1 - y^2), \quad h_b < h < h_E; \quad (18)$$

$$N_e = 0, \quad h < h_b,$$

where

$Y = (h_E - h)/y_E$; h is the altitude; h_E , y_E , and f_E are the E-layer height, semithickness, and critical frequency.

In the E-layer/D-layer tail model the semithickness may increase by up to 4 km, h_b will lower correspondingly, and h_E remains at 115 km. First, an electron density N_{eo} is calculated by Eq. (20) with Y , however, constructed as follows:

$$\begin{aligned} Y' &= 2(h_E - h)/y_E, \\ x &= 1.5 [1.7/(1.7 + Y')]^{\frac{1}{2}}, \\ z &= [1 + 0.1(Y' - 1)|Y' - 1|]/[1 - 0.1/(Y' + 1)^2], \\ Y'' &= 2 - \log(1 + 1.72(Y')^x), \\ Y &= 1, Y'' \text{ negative,} \\ Y &= 1 - \frac{1}{2}(Y'')^z, Y'' \text{ not negative.} \end{aligned}$$

Then

$$N_{eo} = 12400 f_E^2 (1 - Y^2). \quad (19)$$

Calculate the correction for the D-layer tail N_d as follows:

$C = \cos(0.85 X)$, where X is the solar zenith angle;

$$\begin{aligned} N_d &= 0, C \text{ negative; } \\ N_d &= (1 + 0.004 N_s) C^{\frac{1}{4}} / (1 + 81 W^4); \end{aligned} \quad (20)$$

where

$$W = (65 - h)/y_E, \text{ and } N_s \text{ is the sunspot number.}$$

The electron density is finally given by:

$$N_e = N_{eo} + N_d. \quad (21)$$

Between h_E and H_2 , the plasma frequency F_p is taken as the positive solution of a quadratic equation:

$$aF_p^2 + bF_p + c = 0 \quad (22)$$

and the electron density is taken as

$$N_e = 12400 (F_p)^2. \quad (23)$$

The coefficients a , b , and c are calculated as follows:

First, define three reference heights h_a , h_b , h_c :

$$h_a = h_1 - y_1 (1 - (f_E/f_1)^2)^{\frac{1}{2}},$$

$$h_b = h_2 - y_2 (1 - (f_1/f_2)^2)^{\frac{1}{2}},$$

$$h_c = \frac{1}{2} (h_1 + h_b).$$

For h between h_c and h_2 , define coefficients B_1 , B_2 , B_3 , B_4 as follows:

$$B_1 = \frac{1}{2} (h_a - h_E + h_b - h_1)/(f_1 - f_E),$$

$$B_2 = (h_1) - \frac{1}{2} (f_1(h_a - h_E) + f_E(h_b - h_1)/(f_1 - f_E),$$

$$B_3 = y_1/f_1,$$

$$B_4 = y_1.$$

For h between h_c and h_2 , the B_i 's are given by:

$$B_1 = \frac{1}{2} (h_b - h_1)/(f_2 - f_1), \quad B_2 = h_2 - f_2 B_1;$$

$$B_3 = y_2/f_2, \quad B_4 = y_2.$$

The coefficients a , b , c of the quadratic Eq. (22) are defined as:

$$a = B_1^2 + B_3^2,$$

$$b = 2 B_1 (B_2 - h),$$

$$c = (B_2 - h)^2 - B_4^2.$$

The topside model (h greater than h_2) is a modified Chapman profile. Let $Y = 2(h - h_2)/y_2$; then,

$$N_e = 12400 \left\{ (f_2)^2 \exp [1 - Y - \exp (-Y)] + (0.5 + 0.1 f_2) h_2 (h - h_2)/h^2 \right\}. \quad (24)$$

14. MODEL FOR THE GRADIENT OF THE ELECTRON DENSITY

Any ray-tracing technique will require the gradient of the electron density at a field point (r, θ, ϕ) . Clearly, the complications of the model described above for the electron density mitigate against any attempt to derive analytic expressions for the gradient, even neglecting variations in the ionospheric parameters. Furthermore, should one desire to replace the electron density model with some other, either more or less complicated, a general numerical algorithm for the gradient is desired.

The gradient model employed in the WIMP program places the field point at the center of a cubical volume, and computes the electron density at each of the nine points so defined. The coordinates of these nine points are listed in the following table.

Table 2. Coordinates of Points Used for Gradient Calculation

Point	Radial Coordinate	Theta	Phi
1	r	θ	ϕ
2	$r + D_r$	$\theta + D_\theta$	$\phi + D_\phi$
3	$r + D_r$	$\theta - D_\theta$	$\phi + D_\phi$
4	$r + D_r$	$\theta + D_\theta$	$\phi - D_\phi$
5	$r + D_r$	$\theta - D_\theta$	$\phi - D_\phi$
6	$r - D_r$	$\theta + D_\theta$	$\phi + D_\phi$
7	$r - D_r$	$\theta - D_\theta$	$\phi + D_\phi$
8	$r - D_r$	$\theta + D_\theta$	$\phi - D_\phi$
9	$r - D_r$	$\theta - D_\theta$	$\phi - D_\phi$

(r, θ, ϕ) are the coordinates of the field point,

(D_r, D_θ, D_ϕ) are the grid spacings,

$$D_\theta = D_r / r,$$

$$D_\phi = D_r / r \sin \theta.$$

Given a function $f(x)$ evaluated at three points, x_0 , $x_+ = x_0 + dx$, and $x_- = x_0 - dx$, then the best estimate of the derivative of f at x_0 is given numerically by:

$$f'_0 = \frac{1}{2} (f_+ - f_-) / dx^2 \quad (25)$$

where f_- , f_0 , and f_+ represent $f(x_-)$, $f(x_0)$, and $f(x_+)$. The best estimate of the second derivative is given by:

$$f''_o = \frac{1}{2} (f_+ - 2f_o + f_-) / dx^2. \quad (26)$$

Unfortunately, the defined set of points does not contain quite the correct subset to implement the numerical model for the derivative specified by Eq. (25). However, appropriate partial derivatives may be evaluated at the center of each side of the defined cube. Each coordinate then has four approximations to the appropriate partial derivative of the electron density; for instance, the r partial derivative will use pairs (2, 6), (3, 7), (4, 8), and (5, 9).

The algorithm adopted to represent the partial derivatives is the average of the four approximate values.

The value chosen for the grid space is 1 / 3-1/2 km.

15. THE WIMP 3-D RAY-TRACING TECHNIQUE

The ray-tracing model employed in the WIMP program depends upon the application of Bouger's rule and parabolic electron density models in multiple layers; the gradient of the electron density at the reflection height is employed to determine the tilt of the reflecting layer.

The program allows for refraction and/or reflecting in the E , F_1 , and F_2 layers. The F_1 layer is inserted between the E and F_2 such that the bottom of the F_1 layer is at the E -layer height and the F_1 -layer height is at the bottom of the F_2 layer.

The ray tracing is accomplished in SUBROUTINE TRISL.

15.1 Bouger's Rule

Bouger's rule states that in a refracting medium with spherical symmetry electromagnetic radiation propagates in such a way that the quantity $\mu r \cos \beta$ remains constant where μ is the local index of refraction, r is the distance to the field point from the center of symmetry, and β is the local elevation angle.

15.2 Refraction Through a Layer

Refraction through a layer is depicted in Figure 1. The group path correction $\Delta P'$, phase path correction ΔP , and range correction Δ are given by

$$\begin{aligned} \Delta P' &= \left(\frac{y}{\sin \beta_c} \right) \left\{ \frac{1}{2} u \log \left(\frac{u+1}{u-1} \right) - 1 \right\}, \\ \Delta P &= \left\{ 1 - \frac{1}{2} \sin^2 \beta_c (1 + 1/u^2) \right\} \Delta P' - \frac{1}{2} y \sin \beta_c / u^2, \\ \Delta &= \Delta P' \cos \beta_c / (R_o + h_m), \end{aligned} \quad (27)$$

where $u = f \sin \beta_c / f_c$ and f is the operating frequency, f_c the critical frequency, R_o the radius of the earth, h_m the layer height, y the layer semithickness, and β_c the local elevation angle of the unrefracted ray at the layer height.

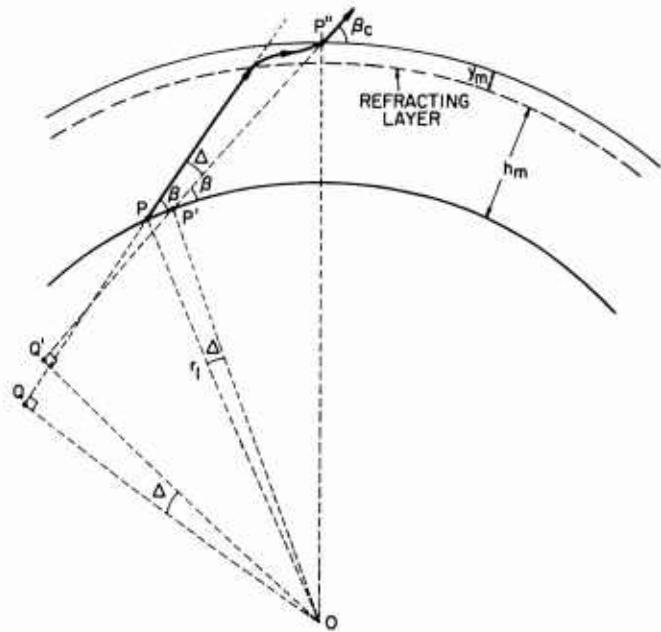


Figure 1. Refraction Through Layer

The group path length P' and phase path length P upon exiting the layer are given by

$$\begin{aligned} P' &= D_0 + \Delta P', \\ P &= D_0 + \Delta P, \end{aligned} \tag{28}$$

where D_o is the distance $P'P''$ in Figure 1.

15.3 Reflection from a Layer

Reflection from a layer is depicted in Figure 2. The group path corrections ΔP are given by

$$\Delta P' = \frac{y}{\sin \beta_r} \frac{1}{2} u \log \frac{u+1}{u-1}, \quad (29)$$

$$\Delta P = \frac{1}{2} y \sin \beta_r + \left\{ 1 - \frac{1}{2} \sin^2 \beta_r (1 + 1/u^2) \right\} \Delta P',$$

where $u = f \sin \beta_r / f_c$, and β_r is the local elevation angle at the virtual height P'' . These corrections apply for the upward trace to the reflection point; equal corrections obtain for the downward trace.

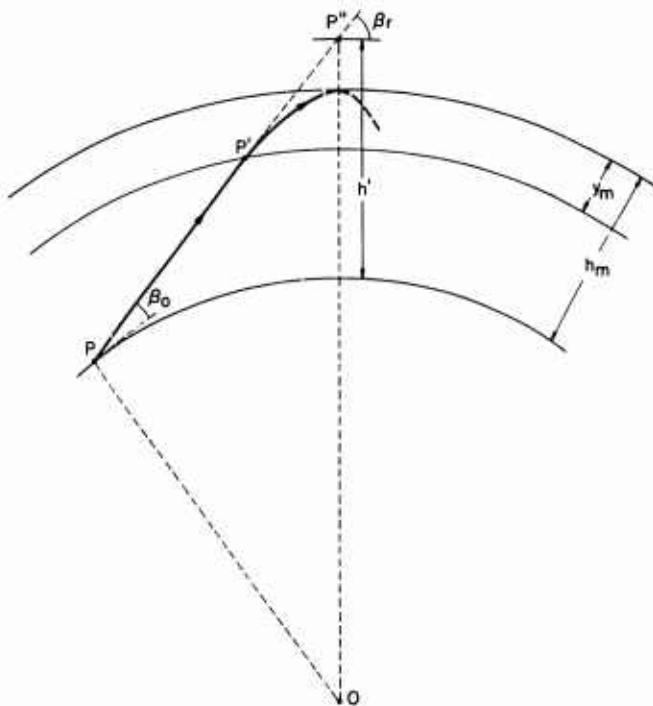


Figure 2. Reflection From Layer

15.4 Tilted Reflection Layer

The gradient of the electron density at the ray reflection point is evaluated and employed to construct an effective tilted reflecting layer. Underlying refracting layers are considered concentric with the earth; however, gradients in these layers are taken into account in that the upward and downward legs of the ray trace through the underlying layers are spatially separated.

The introduction of a tilted reflecting layer, of course, generates considerable complication in the ray trace in that the ray direction, layer normal, and radius vector are no longer coplanar. The program accounts for these bookkeeping complications by setting up orthonormal triads as the ray attacks successive layers.

The y axis is taken parallel to the ray direction. The yz plane contains the center of curvature of the tilted reflecting layer (or the center of the earth in a refracting layer).

15.5 Iteration Scheme

In each hop of the ray trace, the various calculations are iterated to refine the location of the profiles at which refraction through a layer and reflection from a layer occur. In the reflecting layer, the layer tilt is included within the iteration scheme.

At each stage of the ray-trace tests are made for pathological cases such as convergence failures in the allotted number of iterations, inconsistencies between stages, extremely tilted reflecting layers, ducting of the ray between layers, and so forth. Error diagnostic messages are printed prior to returning the main program should TRISL be required to abort the task.

16. FUNCTIONAL DESCRIPTION OF PROGRAM OBLFACT

16.1 Initialization (Block I)

This part of the program clears the INPUT file (NAMELIST INPUT). The elements of the NAMELIST are listed in Table 3 including the mnemonic name used, definition, and default value. A call to RIIP clears the INPUT file of the ITS parameter prediction coefficients. A call to FACTO calculates the F_2 layer correction factors from $f_0 F_2$ and $h'_{\min} F_2$ scaled from the vertical ionogram and appearing in the NAMELIST input. Successive calls to PEAK and SKIP with the remote correction factors $FR\phi$ and $MR\phi$, calculated from a previous run of OBLFACT, check that the ray tracing proceeds as expected (ground-to-ground mode). If not, the mission is aborted and the next task is initiated.

Table 3. Elements of NAMELIST/INPUT/

Mnemonic	Definition	Unit	Notes
SN	Sunspot Number		UNDEF
YRMD	Year & Month, concatenated		UNDEF
DOY	Day of Year	day	UNDEF
ZT	Universal Time, Vertical Ionogram (VI)	hours	UNDEF
RI	Geocentric Distance, VI	km	6370.
NL1	North Latitude, VI	degrees	
WL1	West Longitude, VI	degrees	

Table 3. ELEMENTS OF NAMELIST/INPUT/ (Cont)

Mnemonic	Definition	Unit	Notes
ZIREF	Universal Time, Oblique Ionogram (OI)	hours	UNDEF
RS	Geocentric Distance to ray end point	km	6370.
NLREF	North Latitude, OI Sounder	degrees	
WLREF	West Longitude, OI Sounder	degrees	
AZ	Bore sight azimuth	degrees	
ELSTEP	Elevation step for SKIP search	degrees	1.0
FCF2R	$f_o F_2$ from VI	MHz	UNDEF
HMINR	$h'_{\min} F_2$ from VI	km	UNDEF
FP	Peak Frequency	MHz	*
DELP	Peak Group Path Error	km	*
FS	Skip Frequency	MHz	*
DELS	Skip Group Path Error	km	*
DCHK	Tolerance in Group Path Deviations		10.0
MR ϕ	Gradient Correction Factor, M(3000)F2		#
FR ϕ	Gradient Correction Factor, $f_o F_2$	MHz	#
MODE	MODE = number of hops		?
IRSTRRT	Termination Flag (STOP if ϕ)		1

Explanation of Terms Used in Table 3

NOTES - A numerical value of this column is the default value set in OBLFACT.

UNDEF - Implies that OBLFACT does not establish a default value.

* - These values are determined from a comparison between the observed oblique ionogram (OOI) and the predicted oblique ionogram (POI) generated from a previous run of the BLOBZ driving program. Refer to "Step 5" of the Operating Instructions. Default values of ϕ are assigned to F and iDELP.

- For the first run of OBLFACT, these parameters are set to ϕ . Corrected values will be part of the output of OBLFACT to be used as inputs of a new run of OBLFACT at the user level of iteration. Refer to Steps 4 to 7 of the Operating Instructions.

? - This parameter is an element of the argument list of the ray tracing program TRISL. Neither the operating instruction or the program flow chart illuminate the meaning of its sign. OBLFACT assigns a default value of -1.

16.2 Refinement of MR (Block II)

This part of the program iterates calls to PEAK in order to refine the M(3000) gradient correction factor MR. Since the peak frequency depends on antenna pattern and, thus upon elevation, it therefore depends primarily on the height of the layer. The Block II iteration maintains the $f_0 F_2$ gradient correction factor fixed. The value of MR is adjusted initially by 0.001 and subsequently by a Newton iterative technique until the predicted peak group path agrees with that from the oblique ionogram to within the specified tolerance (DCHK, nominally 10 km), at which point transfer is made to Block III.

Block II is ultimately reentered from Block IV after refinement of the $f_0 F_2$ gradient correction factor. A call to PEAK establishes whether further refinement is required. If the resultant group path is within tolerance, the task is terminated and the results printed.

Should the required information to effect this refinement be not available, the default values of ϕ assigned to FP and DELP automatically cause this part of the program to be bypassed. Thus, only the $f_0 F_2$ gradient correction is determined; the M(3000) F_2 gradient remains by default the same as that of the parameter model (ITS-78), which, presumably, is the best available in the absence of evidence to the contrary.

16.3 Refinement of FR (Block III and IV)

This part of the program iterates calls to SKIP in order to refine the $f_0 F_2$ gradient correction factor FR. In SKIP, rays are traced at frequency FS from 0° to 20° in steps given by ELSTEP (nominally 1° and must not be less than $1/2^\circ$). The array of group paths is searched to locate the minimum. This is compared with the minimum group path extracted from the leading edge of the oblique ionogram at frequency FS. If the difference is within tolerance, the MR iteration is re-entered. If not, FR is corrected for the next iteration.

Since OBLFACT is in a late user stage of simulation and a previous stage BLOB 2 produces the general ray-trace results, the user should have limiting information on the elevations between which the minimum group path should be located. The built-in 0° to 20° may not be sufficient to properly locate the minimum group path. The using facility might consider modifying the program to allow the user to specify the elevation domain to be searched. This may be accomplished as follows:

- (a) Link the initial elevation, ELBEG and number of elevations to be traced, NELM to NAMELIST/INPUT/ in OBLFACT.
- (b) Add ELBEG and NELM to COMMON/FIDDLE/ in OBLFACT, SKIP, and PEAK.

(c) Modify the elevation DO loop in SKIP as follows:

PRESENT VERSION	RECOMMENDED VERSION
NELM=20, D0/ELSTEP + 1.D0	(delete)
.	
.	EL=ELBEG
DO 10 IEL=1, NELM	DO 10 IEL=1, NELM
EL=(IEL-1)* ELSTEP	.
.	.
.	.
.	.
.	.
.	.
10 CONTINUE	10 EL=EL + ELSTEP

17. SUBROUTINE PEAK (FRR, MRR, GPP, IGOBAK)

17.1 Argument List

FRR - $f_o F_2$ correction quantity (INPUT)
MRR - $M(3000)F_2$ correction quantity (INPUT)
GPP - Predicted peak group path (OUTPUT)
IGOBAK - Error condition returned (OUTPUT)

17.2 Common Blocks

/PERT C/ linked to PERT F, the routine that calculates F_2 -layer correction factors from parameters scaled from the oblique ionogram.
/REMWEN/ linked from TRISL. Contains reflection layer information.
/FIDDLE/ linked from OBLFACT. Contains the "peak frequency" FP scaled from the oblique ionogram, transmitter location, and take-off azimuth.

17.3 Function

Computes the "predicted peak group path" corresponding to oblique ionogram correction factors FRR and MRR, and "peak frequency" FP.

17.4 Algorithm

The input parameters FRR and MRR are stored in elements 3 and 5 of /PERT C/ for use by PERT F for calculating correction factors to $f_o F_2$ and $M(3000)F_2$.

An elevation is selected from the following critical table according to the peak frequency, element 1 of /FIDDLE/:

Table 4. Elevation Determination

FP less than	Elevation	FP less than	Elevation
5.74	Undefined	16.74	5.2
6.74	11.9	17.74	4.8
7.74	10.3	18.74	4.5
8.74	8.9	19.74	4.2
9.74	7.7	20.74	4.0
10.74	6.7	21.74	3.8
11.74	5.9	23.74	3.7
12.74	5.2	25.74	3.6
13.74	4.6	28.74	3.5
14.74	4.1	30.74	3.4
15.74	3.9	≥ 30.74	Undefined

The calling program is required to insure that $5.74 < FP < 30.74$.

The ray-tracing program TRISL is called to compute the predicted peak group path GPP.

Elements of /REMWEN/ are checked to insure reflection consistency occurs in the F2 layer. Furthermore, the geocentric distance of the ray endpoint is checked that it is less than 6378.85 km. If these tests are passed, the error condition flag IGOBAK is set to zero; otherwise, an error condition is noted by setting IGOBAK to unity.

18. SUBROUTINE SKIP (FRR, MRR, GPS, IOPT, IGOBAK)

18.1 Argument List

FRR	- $f_0 F_2$ correction quantity (INPUT)
MRR	- $M(3000)F_2$ correction quantity (INPUT)
GPS	- Predicted minimum group path (OUTPUT)
IOPT	- Correction control parameter (INPUT)
IGOBAK	- Error condition returned (OUTPUT)

18.2 Common Blocks

/PERT C/	linked to PERT F
/REMWEN/	linked from TRISL
/FIDDLE/	linked from calling program (OBLFACT)

18.3 Function

Computes the predicted minimum group path corresponding to the oblique ionogram correction terms FRR and MRR, and "skip frequency" FS (element 2 of /FIDDLE/).

18.4 Algorithm

SKIP transfers FRR and MRR of the argument list to elements 3 and 5 of /PERT C/ respectively, to be used in PERT F to calculate F_2 correction factors.

A sequence of elevations between 0° and 20° is selected for ray tracing via calls to TRISL. The elevation step is contained in element 8 of /FIDDLE/ and a sufficient number of elevations are selected to include the entire domain (0° , $20^\circ+$). Provision is made for up to 41 ray traces; thus, the user must insure that the elevation step size is no greater than 0.5° . The elevation scan is terminated at the first occurrence of a penetration through the ionosphere if such occurs before the normal loop termination.

The rays traced in this elevation scan are partitioned into three sets:

- (a) Rays not reflecting from the F_2 layer. These are excluded from further consideration in (b) and (c).
- (b) Rays with end point at geocentric distance no greater than 6378.85 km.
- (c) Rays with end point at geocentric distance greater than 6378.85 km.

If set (b) is empty, the error flag IGOBAK is set to unity and control is returned to the calling program. Otherwise, the element of (b) with the smallest group path is determined. This least group path is established as the predicted minimum group path GPS unless the following conditions obtain:

- (a) SKIP had been called with IOPT not zero, and
- (b) The ray with next higher elevation belongs to set (c) and has a smaller group path length.

In the latter case, the minimum group path returned as GPS is given by:

$$GPS = G_b + \left\{ (G_c - G_b) / (R_c - R_b) \right\} (6378.85 - R_b),$$

where the G's and R's refer to group paths and end point geocentric distance, and the subscripts b and c refer to the above selected elements of set (b) and (c).

Should calls be issued to SKIP more than 100 times in any run of OBLFACT, the error flag is set to two and the task immediately aborted.

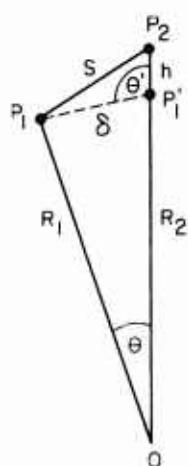
19. REMARKS ON THE USE OF DOUBLE PRECISION ARITHMETIC

The version of the program that the present author has studied has been modified from CDC 6600 machines for use on UNIVAC machines. The essence of this modification is to assign the double precision attribute to every real variable. In the opinion of the present author, wholesale use of double precision arithmetic is not justified, reduction notwithstanding.

In the first place, double precision arithmetic is expensive. Analysis of double precision arithmetic reveals that (1) twice the core storage is required for the variables involved in the calculation, (2) the coding requires, in general, three times the number of instructions, and (3) the execution time increases by approximately a factor of four.

In the second place, increasing the precision of a calculation does not increase the accuracy of the computed result. For example, the geomagnetic field employed in conjunction with the ITS parameter prediction model is a sixth order spherical harmonic expansion. The expansion coefficients are given to one part per million or less. An eight significant digit machine in single precision can calculate the geomagnetic field at a point to the accuracy of the model. The ionospheric parameter model is essentially a one percent model; double precision arithmetic will not improve this situation.

On the other hand, there are situations where single precision arithmetic may produce inaccurate results; for example, in the solution of plane triangles in certain situations.



Consider the situation depicted here. The distances R_1 and R_2 and the angle θ are known and the distance S between P_1 and P_2 is required. The law of cosines applies and

$$S^2 = R_1^2 + R_2^2 - 2R_1 R_2 \cos \theta. \quad (30)$$

Typically, the distances R_1 and R_2 are of the order of 6000 km, the arc $P_1 P_1'$ might be 60 km ($\theta = 0.01$ rad), and the altitude difference $P_1' P_2$ might also be of the order of 60 km. Thus, take R_2 and $\cos \theta$ to be given exactly by

$$R_2 = R_1(1 + 0.01),$$

$$\cos \theta = 1 - \frac{1}{2} \times 10^{-4}.$$

With single precision of 8 significant digits,

$$S^2 = R_1^2 - 1 + (1 + 2 \times 10^{-2} + 10^{-4} \pm 10^{-9}) - (2 + 2 \times 10^{-2} - 10^{-4} - 10^{-6} \pm 10^{-8})$$
$$S^2 = R_1^2 - 2 \times 10^{-4} + 10^{-6} \pm 10^{-8}.$$

In this case, the truncation error has resulted in reduction of precision to one part in 10^{-4} .

This loss of precision may or may not be tolerable; in either case it is not necessary, for the law of cosines may be reformulated to solve the triangle $P_1 P_2 P_1'$ for S , retaining full single precision results. The length δ of the cord of the angle θ is given by

$$\delta = 2R_1 \sin \frac{1}{2} \theta.$$

Furthermore,

$$\cos \theta' = -\sin \frac{1}{2} \theta = -\delta / 2R_1,$$

$$R_2 = R_1 + h.$$

Then,

$$S^2 = h^2 + \delta^2 + h\delta^2/R_1. \quad (31)$$

This form of the law of cosines will retain single precision results, and should be used wherever possible. To implement this recommendation in SUBROUTINE TRISL, however, would require considerable effort and analysis; a totally new program may be required.

20. MODEL COMPARISON

For purposes of comparison, the WIMP program modelling subroutines were used to generate ionospheric models for various combinations of parameters (Sunspot Number, Season, Universal Time) for a midlatitude location. These were compared with similar models derived from a program in use at RADC.⁴ These comparisons are shown in Figures 3 through 13.

4. Rush, C. M., Miller, D., and Gibbs, J. (1974) The relative daily variability of $F_0 F_2$ and $h_m F_2$ and their implications for HF radio propagation, Radio Science, 9:749-756.

Both models use the same formulation for $f_o F_2$, the maximum plasma frequency of the F-layer (the ITS-78 model). Figures 3 through 5 show the Universal Time variation of the height of maximum electron density ($h_m F_2$) for three seasons and two sunspot numbers [W(XX) and R(XX) refer to the WIMP and RADC models for SSN = XX]. Similarly, Figures 6 through 8 show the comparison of parabolic semithickness ($y_m F_2$); WIMP uses a semithickness value which is time independent. The WIMP model contains a discontinuity at the lower side of the F layer, which results in the most significant departures from the RADC model in the vertical profile. In order to illustrate these departures, the difference between the plasma frequency was calculated by the two models at the altitude of the F_1 -layer maximum used in WIMP. These results are shown for four seasons in Figures 9 through 12, where the times of sunrise and sunset are also indicated. Figure 13 shows a comparison of the two models for given time (χ is the solar zenith angle). The relevant ionospheric model parameters are indicated in the figure.

The results of ray tracing obliquely through the 3-D ionosphere of which Figure 13 represents a single vertical profile are shown in Figure 14. The ray-trace program used was the standard RADC program, known as ARCON II, ITS. As expected, the greatest discrepancies between the oblique group path for the WIMP and RADC models are to be found corresponding to the profile discontinuity at the F_1 layer (compare Figures 9 through 12). In order to examine the differences in computed leading edge of a backscatter ionogram, due to the different models, a one-dimensional ionospheric model was generated, having the vertical profile given by the RADC and WIMP models in Figure 13, (that is, having no horizontal gradients). Leading edges were then computed for simulated backscatter ionograms, using the ARCON II ray-trace program, and the results shown in Figure 15.

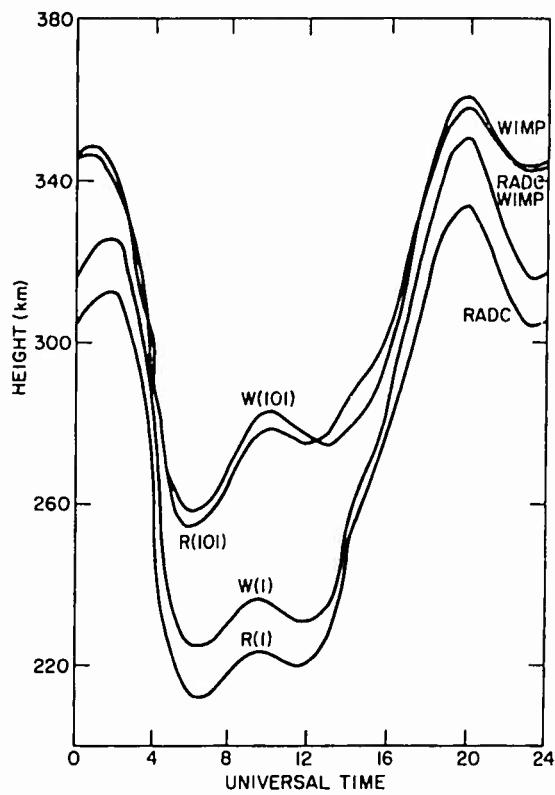


Figure 3. RADC and WIMP Model
 $h_m F_2$, Winter Solstice

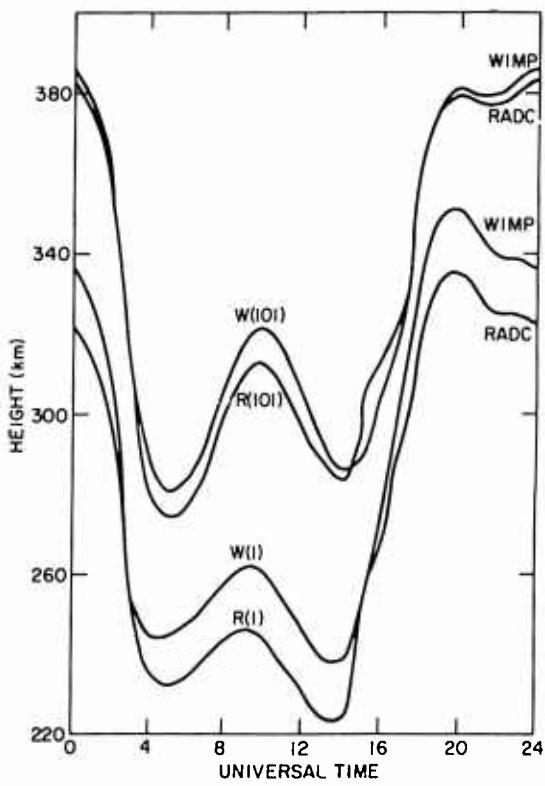


Figure 4. RADC and WIMP Model
 $h_m F_2$, Vernal Equinox

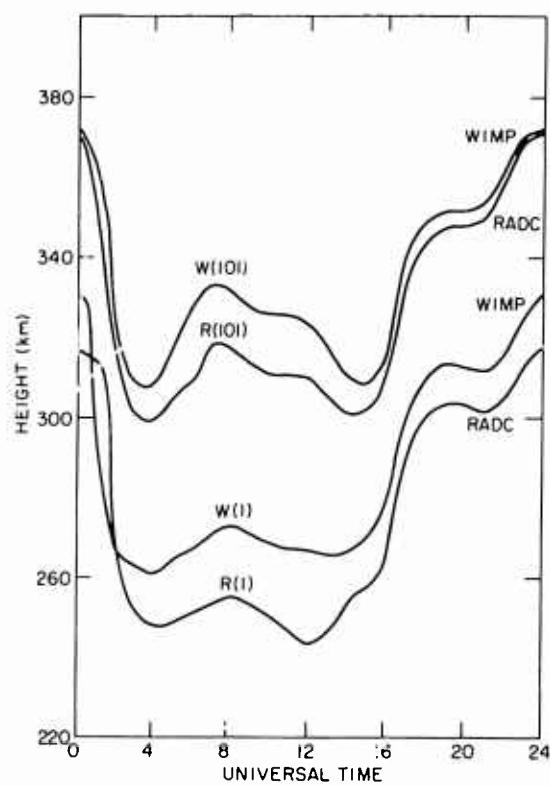


Figure 5. RADC and WIMP Model
 $h_m F_2$, Summer Solstice

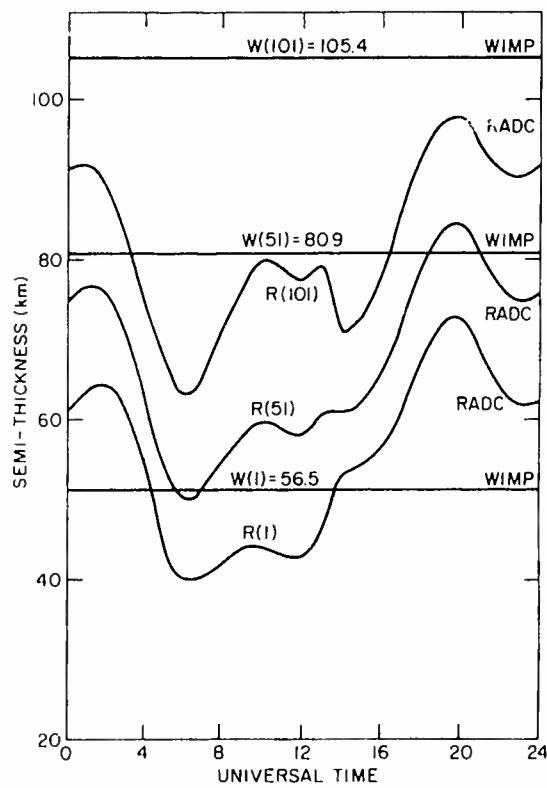


Figure 6. RADC and WIMP Model
 $y_m F_2$, Winter Solstice

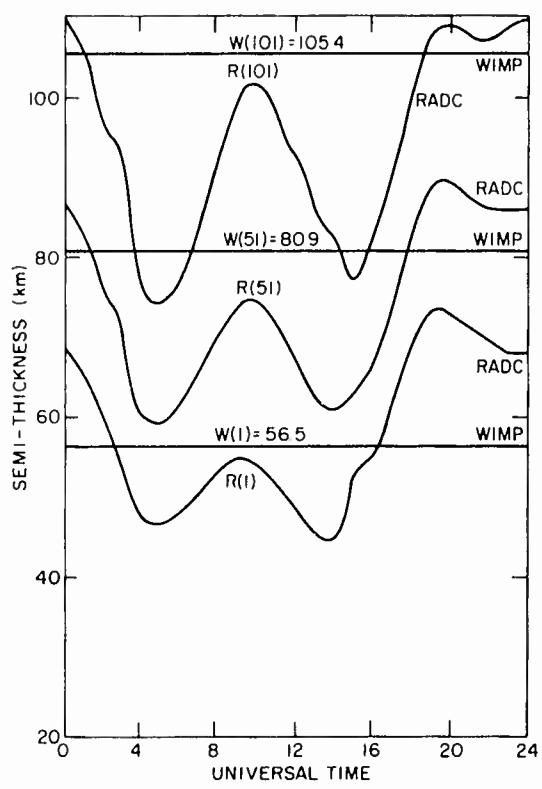


Figure 7. RADC and WIMP Model
 $y_m F_2$, Vernal Equation

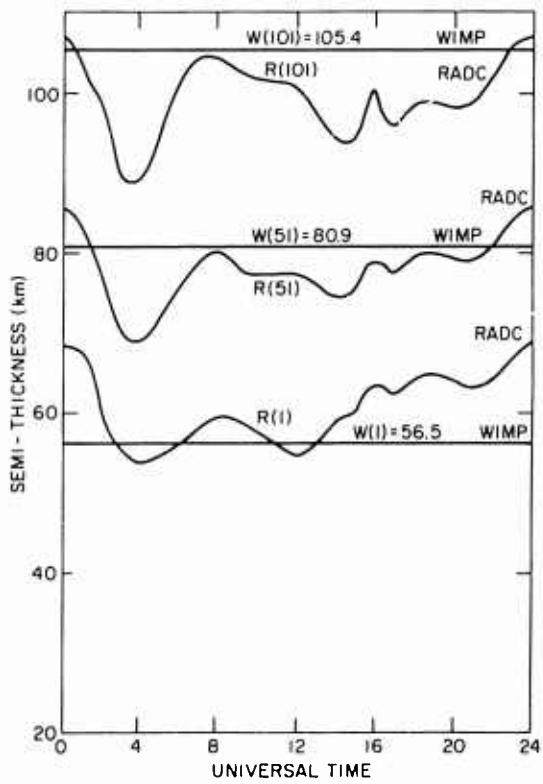


Figure 8. RADC and WIMP Model
 $y_m F_2$, Summer Solstice

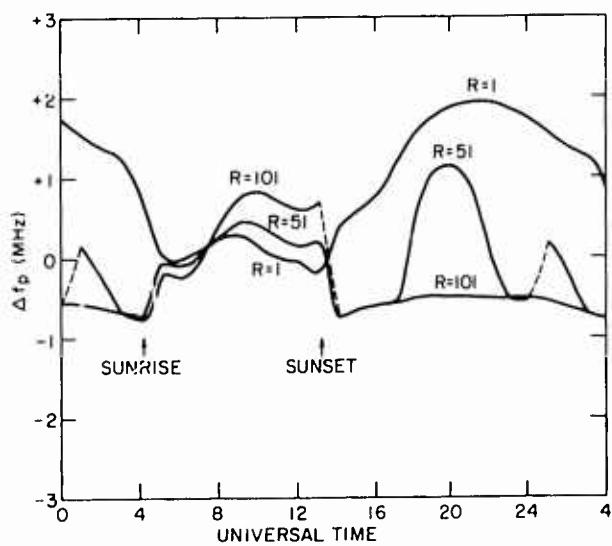


Figure 9. RADC Plasma Frequency at WIMP $h_m F_1$ Minus WIMP $f_o F_1$, Winter Solstice

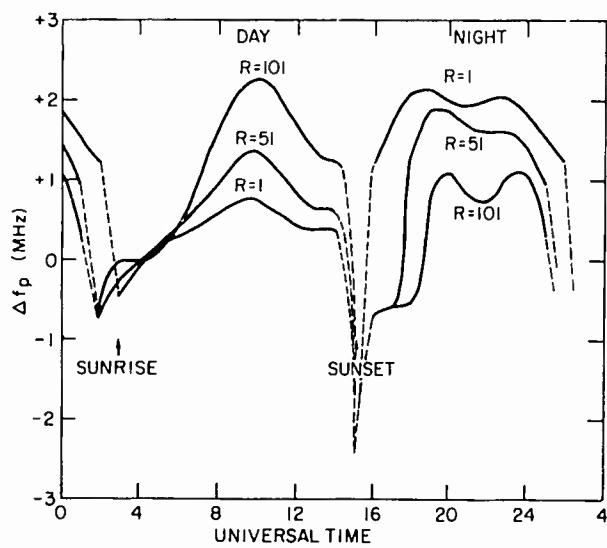


Figure 10. RADC Plasma Frequency at WIMP $h_m F_1$ Minus WIMP $f_o F_1$, Vernal Equinox

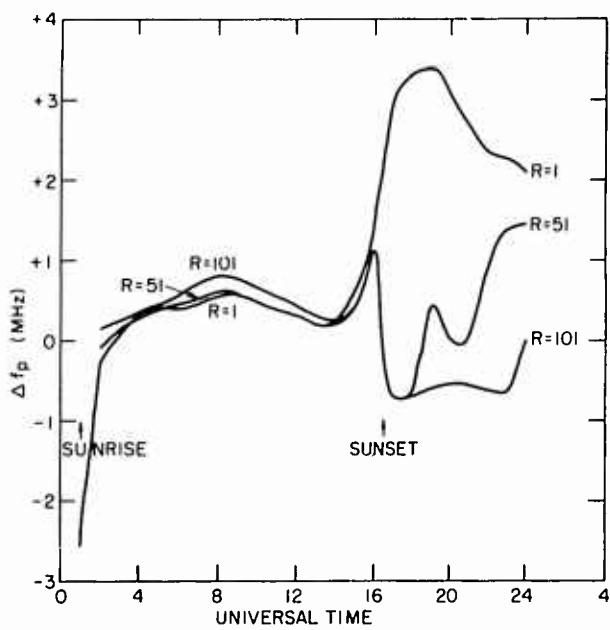


Figure 11. RADC Plasma Frequency at WIMP $h_m F_1$ Minus WIMP $f_o F_1$, Summer Solstice

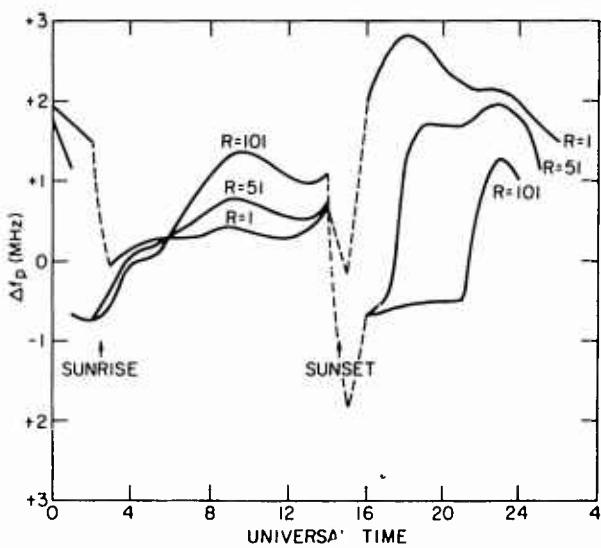


Figure 12. RADC Plasma Frequency at WIMP $h_m F_1$ Minus WIMP $f_o F_1$, Autumnal Equinox

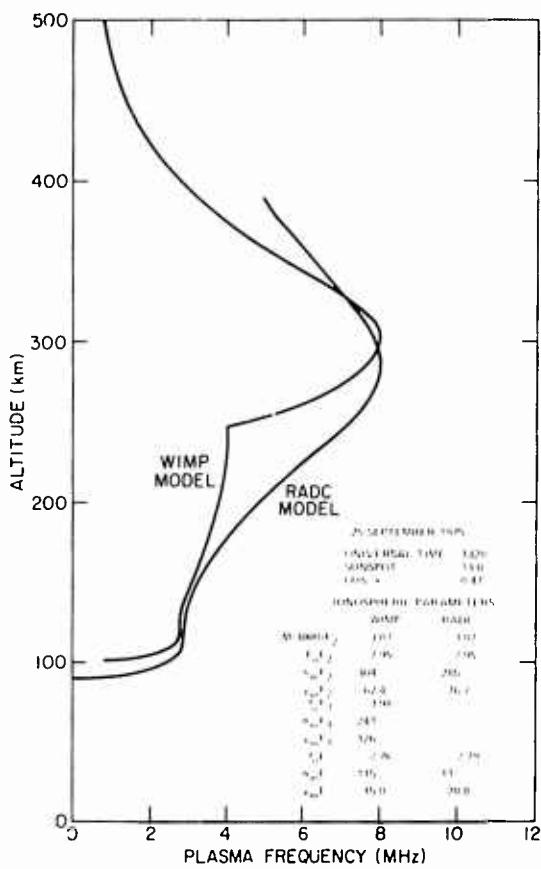


Figure 13. RADC and WIMP Plasma Frequency Profiles

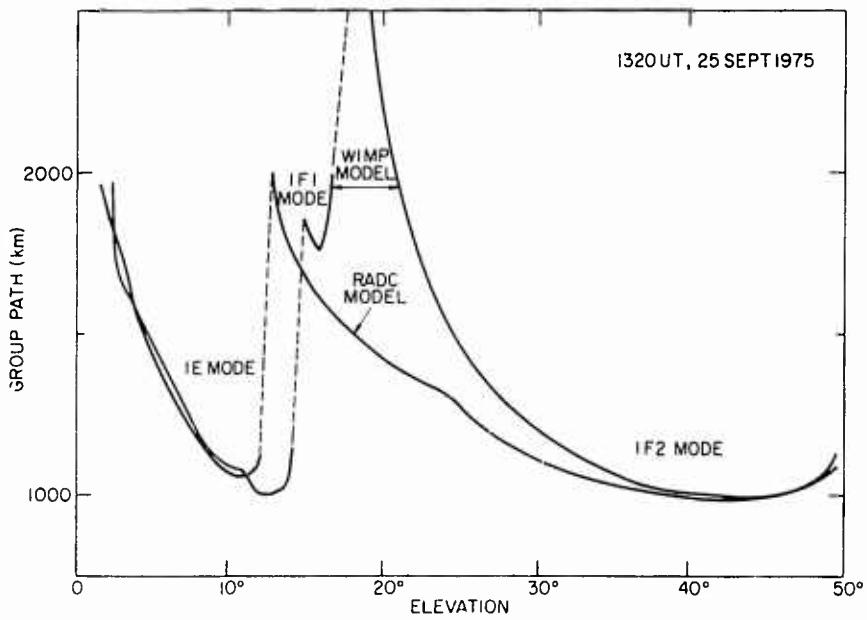


Figure 14. ALCON II 10-MHz Ray Traces, RADC and WIMP Profiles

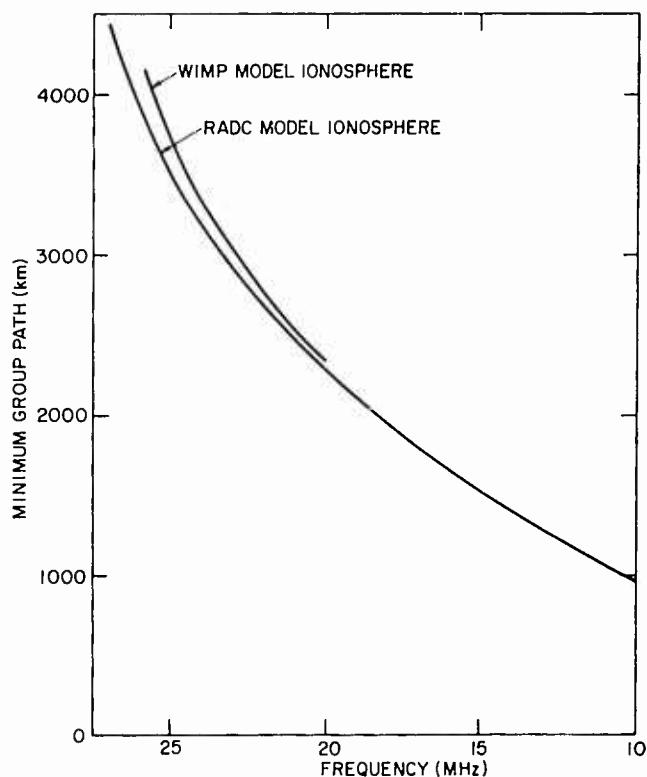


Figure 15. ARCON II
Predicted Leading Edges,
RADC and WIMP Profiles

21. COORDINATE CONVERSION

The conversion from apparent radar range (that is, group path (P) to true range (R) can be accomplished if the ionospheric structure is known, by using the procedures described earlier. The RADC model for 1320 UT on 25 September 1975 was used, together with the ARCON II ray-trace program, to compute $(P-R)$ as a function of P for frequencies in the range 18 to 26 MHz, as shown in Figure 16. The locus of the backscatter leading edge is indicated by the curve labelled P_{\min} , corresponding to the minimum group path at each frequency.

Figure 17 shows the comparison of the actual leading edge of a backscatter ionogram measured at 1320 UT (Curve 2) with the simulated leading edge (Curve 6). Curve 1 shows a leading edge measured at 1340 UT, indicating that the ionosphere is moderately unstable, since Curves 1 and 2 are noticeably different. Curve 3 indicates a secondary leading edge appearing in the ionograms, perhaps a result of azimuthal gradients in the ionosphere. The ionospheric model was then updated by modifying it on the basis of the measured vertical ionogram and allowing for a linear gradient, such that

$$N_e = BN_{eo} (1 + A R_+) ,$$

where N_e is the modelled electron density at any location.

N_{eo} is the modelled electron density (from the RADC program)

$$B = \frac{(f_o F_2) \text{ measured}}{(f_o F_2) \text{ model}},$$

$A = \text{constant}$,

R_+ = boresight range (in radians).

It should be noted that the range is here measured in terms of the angle subtended at the earth's center by the arc on the earth's surface which is the ground range. Curve 5 in Figure 17 shows the computed leading edge for $A = 2.0$ and Curve 4 shows the best fit ($A = 1.61$) with the measured data. By repeating the procedure illustrated in Figure 16, the best estimated conversion from radar range to true range can be determined for any operating frequency. Although azimuthal radar information is not available, it is possible to ray trace at various azimuths to establish a locus on the ground of possible ranges for a target having any given radar range.

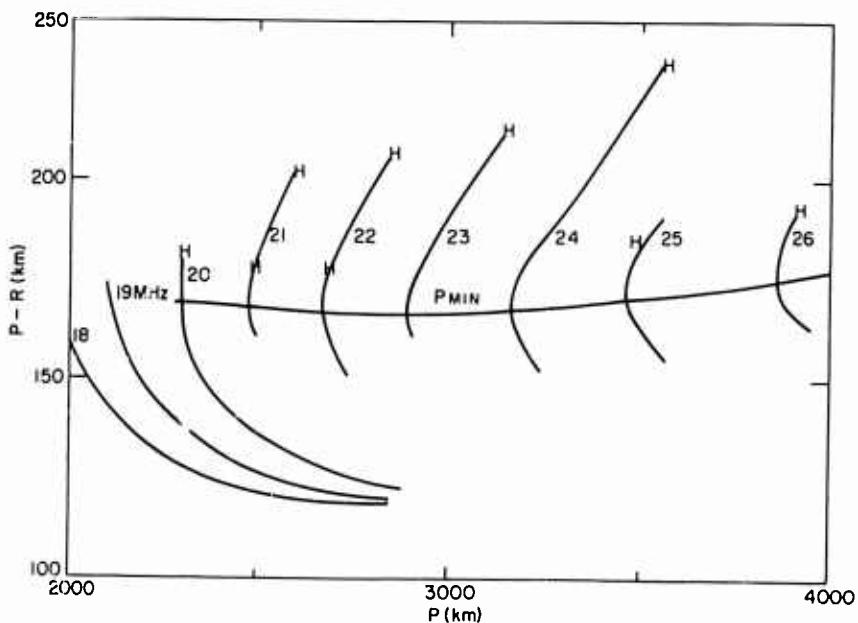


Figure 16. Illustrating Range Conversion

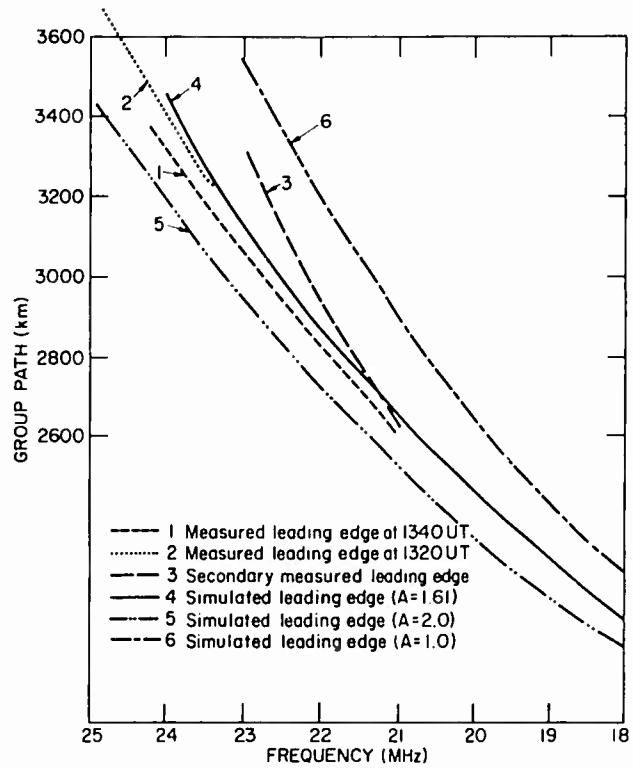


Figure 17. Backscatter Leading Edge Comparison

Appendix A

Program Listings for the WIMP Model Ionosphere

Program listings are included for the WIMP model ionosphere; each subroutine is briefly described as follows:

1. RIIP - Calling control program for layer parameters and electron density.
2. CRPL2 - Generates $f_0 F_2$ and $M(3000)F_2$.
3. MMDIP - Geomagnetic Field Model.
4. PERT F - $f_0 F_2$ and $M(3000)F_2$ gradient factors.
5. DFP3 - Great Circle Range/Azimuth Calculations.
6. DFP - Great Circle Range Calculation.
7. PTHP - E , F_1 , $Y_m F_2$, and $h_m F_2$ calculations.
8. NFROMR - Electron Density Profile.



ROUTINE RIIP

74/74 OPT=1

FTN 4.5+414

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SUBROUTINE RIIP(RFEC,BNLATA,BWLONA,PLASD) RII
C RII
C PROGRAMMED FOR 0.ODOM BY COMPUTATIONS,INC. -OCTOBER,1967 RII
C RII
C RII
C RII
IMPLICIT DOUBLE PRECISION (A-H,O-Z) RII
DOUBLE PRECISION M3000,NLATA RII
DOUBLE PRECISION MFAC RII
LOGICAL SMOOTH,TILT,NIP,FAST RII
COMMON/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAE,HME,HAF1,HMF1,HAF2,HMF2, RII
1SN,ZT,YR,D,HAESET,MFAC,F2FAC,F1FAC,EFAC,H2FAC,SNSQRT,QRAD,CQ,IDL,I RII
2A,SMOOTH RII
COMMON/RPERT/RRFEC,ITIP/NIPRIP/NIP/TILTC/TILT,FAST RII
COMMON/RIIFWA/IX(4) RI2
REAL IX RI2

DATA NLATA,WLONGA RI2
DATA SN,ZT,YR,D/13.00,13.00,7509.00,269.00/ RI2
DATA M3000,FCF2,FCF1,FCE/3.0500,8.00,4.0800,2.7900/ RI2
DATA HBE,HME,HMF1,HMF2/90.00,110.00,180.00,288.00/ RI2
DATA HAE,HAF1,HAF2/20.00,70.00,108.00/ RI2
DATA MFAC,F2FAC,F1FAC,EFAC,H2FAC/5*1.00/ RI2
DATA HAESET/15.00/ RI2

NLATA=BNLATA*57.29577951308232D0 RII
WLONGA=BWLONA *57.29577951308232D0 RII
RRFEC=RFEC RII
NLATA=DMOD(NLATA,90.00) RII
WLONGA=DMOD(WLONGA,360.00)+180.00-DSIGN(180.00,WLONGA) RII
1004 CALL CRPL2(NLATA,WLONGA) RII
M3000=M3000*MFAC RI2
FCF2 = FCF2*F2FAC RI2
C PREDICTED BOTTOM OF E LAYER RII
1005 BA=100.00 RII
AA=BA+HAESET RII
IF(IDL*IA.EQ.0) GO TO 1006 RII
CALL DFP(NLATA,WLONGA,76.00,102.00,DIST) RII
BA=100.00-4.00*DMAX1((1.00-DABS(DIST-3.03)/3.03)**2,0.000)*DMAX1( RII
1 DCOS((DABS(15.00*DABS(ZT-12.00)-WLONGA)-90.00)/(2.00* RII
2 57.29577951308232D0)),u,0.00) RII
C PREDICTED TRUE HEIGHT PROFILE RII
1006 CALL PTHP(NLATA,WLONGA,AA,BA) RII
C GET ELECTRON DENSITY AT REF. POINT RII
C GET N FROM R RII
IF(RFEC.LE.6370.00) RETURN RII
CALL NFROMR(RFEC,PLASD) RII
RETURN RII
END RII

```

OUTINE CRPL2

74/74 OPT=1

FTN 4.5+414

04/27/

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SUBROUTINE CRPL2(NLAT,WLONG) CRP
C ...TO FIND CRITICAL FREQUENCY AS A FUNCTION OF THETA AND PHI CRP
C FROM NEW NBS IONOSPHERIC PREDICTIONS FOR A PARTICULAR TIME... CRP
C IMPLICIT DOUBLE PRECISION (A-H,O-Z) CRP
C DOUBLE PRECISION NLAT,M3000,MFAC CRP
C DIMENSION SINTO(11),COSTO(11),G(76),GAMMA(2),DKTO(76,2) CRP
C DIMENSION CT(8),ST(8) CRP
C COMMON/RIIPAR/M3000,FCF20,DUM(9),SN,ZT,YR,DAY,HAESET,MFAC, FFAC, CRP
C 1DUM1(6),ID(3) CRP
* /LABCRP/NHARM(2),KI(2),KII(2),KIII(2),KIV(2),KV(2),KVI(2),KVII(2), CRP
* KVIII(2),KIX(2),D(13,76,2) CRP
DATA RAD/.0174532925199433D0/ CRP
G(1)=1.000 CRP
CALL MHODIP(NLAT,WLONG,SSMX) CRP
THERAD=(360.00-WLONG)*RAD CRP
COSLAM=DCOS(NLAT*RAD) CRP
CT(1)=COSLAM*DCOS(THERAD) CRP
ST(1)=COSLAM*DSIN(THERAD) CRP
DO 63047 IJK=2,8 CRP
CT(IJK)=CT(1)*CT(IJK-1)-ST(1)*ST(IJK-1) CRP
63047 ST(IJK)=CT(1)*ST(IJK-1)+ST(1)*CT(IJK-1) CRP
IF(DABS(ZT-ZTP).LT.1.0-3.AND.DABS(YR-YRP).LT.1.0-1)GO TO 20 CRP
ZTP=ZT CRP
YRP=YR CRP
T0=15.000*ZT-180.000 CRP
TORAD=T0*RAO CRP
ARG=0.000 CRP
NHARML=MAX0(NHARM(1),NHARM(2)) CRP
DO 1 J=1,NHARML CRP
ARG=TORAD+ARG CRP
SINTO(J)=DSIN(ARG) CRP
1 COSTO(J)=DCOS(ARG) CRP
DO 2 L=1,2 CRP
NHARML=NHARM(L) CRP
K9=KIX(L)+1 CRP
DO 2 K=1,K9 CRP
DKTO(K,L)=D(1,K,L) CRP
DO 3 J=1,NHARML CRP
3 DKTO(K,L)=DKTO(K,L)+D(2*J+1,K,L)*COSTO(J)+D(2*J,K,L)*SINTO(J) CRP
2 CONTINUE CRP
20 DO 100 L=1,2 CRP
NHARML=NHARM(L) CRP
K1=KI(L)+1 CRP
K2=KII(L)+1 CRP
K3=KIII(L)+1 CRP
K4=KIV(L)+1 CRP
K5=KV(L)+1 CRP
K6=KVI(L)+1 CRP
K7=KVII(L)+1 CRP
K8=KVIII(L)+1 CRP
K9=KIX(L)+1 CRP
K1P1=K1+1 CRP
K1P2=K1+2 CRP
K1P3=K1+3 CRP
K2P1=K2+1 CRP
K2P2=K2+2 CRP
K2P3=K2+3 CRP

```

ROUTINE CRPL 2

74/74 7PT=1

FTN 4.5+414

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      K3P1=K3+1          CRP
      K3P2=K3+2          CRP
      K3P3=K3+3          CRP
      K4P1=K4+1          CRP
      K4P2=K4+2          CRP
      K4P3=K4+3          CRP
      K5P1=K5+1          CRP
      K6P1=K6+1          CRP
      K7P1=K7+1          CRP
      K8P1=K8+1          CRP
      DO 4 K=2,K1        CRP
4      G(K)=G(K-1)*SSMX CRP
      IF(K1.EQ.K2) GO TO 9 CRP
      G(K1P1)=CT(1)      CRP
      G(K1P2)=ST(1)      CRP
      DO 5 K=K1P3,K2,2  CRP
      G(K)=G(K-2)*SSMX CRP
5      G(K+1)=G(K-1)*SSMX CRP
      IF(K2.EQ.K3) GO TO 9 CRP
      G(K2P1)=CT(2)      CRP
      G(K2P2)=ST(2)      CRP
      DO 6 K=K2P3,K3,2  CRP
      G(K)=G(K-2)*SSMX CRP
6      G(K+1)=G(K-1)*SSMX CRP
      IF(K3.EQ.K4) GO TO 9 CRP
      G(K3P1)=CT(3)      CRP
      G(K3P2)=ST(3)      CRP
      DO 7 K=K3P3,K4,2  CRP
      G(K)=G(K-2)*SSMX CRP
7      G(K+1)=G(K-1)*SSMX CRP
      IF(K4.EQ.K5) GO TO 9 CRP
      G(K4P1)=CT(4)      CRP
      G(K4P2)=ST(4)      CRP
      DO 8 K=K4P3,K5,2  CRP
      G(K)=G(K-2)*SSMX CRP
8      G(K+1)=G(K-1)*SSMX CRP
      IF(K5.EQ.K6) GO TO 9 CRP
      G(K5P1)=CT(5)      CRP
      G(K6)=ST(5)        CRP
      IF(K6.EQ.K7) GO TO 9 CRP
      G(K6P1)=CT(6)      CRP
      G(K7)=ST(6)        CRP
      IF(K7.EQ.K8) GO TO 9 CRP
      G(K7P1)=CT(7)      CRP
      G(K8)=ST(7)        CRP
      IF(K8.EQ.K9) GO TO 9 CRP
      G(K8P1)=CT(8)      CRP
      G(K9)=ST(8)        CRP
9      GAMMA(L)=0.0D0    CRP
      DO 10 K=1,K9       CRP
10     GAMMA(L)=GAMMA(L)+DKTO(K,L)*G(K)    CRP
100    CONTINUE          CRP
      FCF20=GAMMA(1)*DABS(FFAC) CRP
      M3000=GAMMA(2)*DABS(MFAC) CRP
      IF(FFAC.LT.0.0D0)CALL PERTF(ZT,NLAT,WLONG,FCF20) CRP
      IF(MFAC.LT.0.0D0)CALL PERTM(ZT,NLAT,WLONG,M3000) CRP
      RETURN             CRP

```

ROUTINE PTHP

74/74 OPT=1

FTN 4.5+414

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      SUBROUTINE PTHP(NLAT,WLONG,A,B) PTH
C   PREDICTED TRUE HEIGHT PROFILE PTH
C   PROGRAMMED FOR 0.000M BY I.STUHLER PTH
C   IMPLICIT DOUBLE PRECISION (A-H,O-Z) PTH
C   DOUBLE PRECISION NLAT,M3000,M,J,KK PTH
C   LOGICAL SMOOTH PTH
C   COMMON/FACCOM/FM,ZZ,KK,P3000 PTH
C   COMMON/RIIPAR/M3000,FCF20,FCF10,FCEO,HBEP,HPE,HMEP,`F1,HMF1P,HPF2 PTH
1,HMF2P,SN,ZT,YR,D,OM(3),F1FAC,EFAC,H2FAC, PTH
2 SNSQRT,QRAD,CQ,IO(2),SMOOTH PTH
   DATA RAD/57.2957795130823200/ PTH
C   SOLVE FOR ZENITH CORR. ANGLE FOR DAY OF YEAR PTH
   M=23.4500*DSIN(180.00*(D-82.500)/(182.00*RAD)) PTH
C   GET F3000 PROPAGATION FREQ FOR F2 LAYER PTH
   F3000=FCF20*M3000 PTH
C   CHECK FOR INCORRECT DAY(NEG) PTH
   IF(D.LT.0.000) GO TO 2000 PTH
C   IS DAY PAST SPRING PTH
   IF(D.GE.162.500) GO TO 1000 PTH
   X=D+365.500 PTH
   Y=1.000 PTH
   GO TO 1001 PTH
C   IS DAY PAST FALL PTH
1000 IF(D.GE.344.500) GO TO 1002 PTH
   X=0 PTH
   Y=-1.000 PTH
   GO TO 1001 PTH
C   CHECK FOR INCORRECT DAY (TOO LARGE) PTH
1002 IF(D.GE.366.500) GO TO 2001 PTH
   X=0 PTH
   Y=1.00 PTH
C   SOLVE FOR SOLAR ZENITH ANGLE IN RAD PTH
1001 J=Y*.023500*(64.00/(4.00+DABS((X-344.500)/45.00)**3)-240.00/(15.00 PTH
   1+DABS(X-344.500))) PTH
   IF(ZT.LT.12.00) ZT=-ZT PTH
   Z=DABS(15.00*DABS(ZT-12.00)-J*15.00-WLONG) PTH
   IF(Z.GE.180.00) Z=360.00-Z PTH
   ZSQ=Z*Z PTH
   QSQ=ZSQ*(DCOS(0.600*(NLAT+M)/RAD)**2)+(NLAT-M)**2 PTH
1005 Q=DSQRT(QSQ) PTH
   QRAD=Q/RAD PTH
   CQ=DCOS(.93200*QRAD) PTH
C   FUNCTION FOR E-LAYER NIGHT TIME FORMATION PTH
   CCQ=((CQ+1.00)**.500)**2 PTH
   SNSQRT=DSQRT(1.00+.004D0*SN) PTH
   IF(CQ.LE.0.00) GO TO 1101 PTH
C   SOLVE FOR PRED E-LAYER CRITICAL FREQ PTH
C   10.0489=3.17*3.17, .5625=.75*.75 PTH
   FCEO=SNSQRT*DSQRT(10.0489D0*CQ**2*(2.00/3.77500)+.5625D0*CCQ**2) PTH
   IF(FCEO.GE.FCF20) FCEO=.7500*SNSQRT*CCQ PTH
   GO TO 1102 PTH
1101 FCEO=.7500*SNSQRT*CCQ PTH
C   SOLVE FOR PRED F1-LAYER CRITICAL FREQ PTH
1102 FCF10=1.26D0*FCEO+.500 PTH
   IF(FCF10.LT.FCF20+.99D0) GO TO 9982 PTH
   FCF10=.99D0*FCF20 PTH
   FCEO=DMAX1((FCF10-.500)/1.26D0,1.0-5) PTH

```

ROUTINE PTHP

74/74 OPT=1

FTM 4.5+414

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C   SOLVE FOR REF. FREQ. NO. 1
9982  FK1=FCF20-(FCF20-FCF10)/4.00          PTH
C   CALCULATE PRED. SEMITHICKNESS OF F2 LAYER
      HPF2=(0.48900*SH+56.000)*H2FAC          PTH
C   SOVE FOR REF FREQ. NO. 2
      FK2=FCF20*(1.00-(DSQRT(HPF2)/100.000))  PTH
C   SET FM TO GREATER OF TWO REF. FREQ.
      IF(FK1.GT.FK2) GO TO 1003                PTH
      FM=FK2
      GO TO 1004
1003 FM=FK1
C   SOLVE FOR VIRTUAL HT. OF F3000
1004 XX=FM/F3000
      H3000=3100.00*XX**2+70.000          PTH
      FC=4.00*FM-3.00*FCF10                PTH
      P3000=((FC+3.78D0*FCEO+1.5D0)/(1.26D0*FCEO+.5D0))*DLOG((FC+8.82D0
      1 *FCEO+3.5D0)/(FC-1.26D0*FCEO-0.5D0))  PTH
      ZZ=(A-B)*(FC+3.78D0*FCEO+1.5D0)/(8.00*FCEO)*DLOG((FC+7.78D0
      * *FCEO+1.5D0)/(FC-.22D0*FCEO+1.5D0))  PTH
      FF=FM/FCF20
      KK=HPF2*FF*DLOG((1.00+FF)/(1.00-FF))/2.000  PTH
C   CALCULATE PRED. HT. OF F2 LAYER MAX.
      HMF2P=8.00*(H3000-ZZ-B-KK)/P3000+HPF2+A  PTH
C   CALC. HTS. OF OTHER LAYERS
      HMF1P=HMF2P-HPF2
      HMEP=A
      HBEP=B
      HPF1=HMF1P-HMEP
      HPE=A-B
      ZT=DABS(ZT)
      FCEO=DMIN1(FCEO*EFAC,(.99D0*FCF20-.5D0)/1.26D0)  PTH
      IF(F1FAC) 1014,1014,1015
1014 FCF10=1.26D0*FCEO+.5D0
      GO TO 1016
1015 FCF10=FCF10*F1FAC
1016 IF(SMOOTH)FCF10=FCF10/.866025403784439D0
      FCF10=DMIN1(FCF10,.99D0*FCF20)
      RETURN
2000 WRITE(6,4)D
4  FORMAT(4H D =D13.5,12H IS NEGATIVE)
      STOP
2001 WRITE(6,5)D
5  FORMAT(4H D =D13.5,22H IS GREATER THAN 366.5)
      STOP
      END

```

```

      SUBROUTINE NFROMR(RFEC,PLASD)          NFR
C
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)      NFR
      DOUBLE PRECISION K,J,M3000              NFR
      LOGICAL SMOOTH                         NFR
      COMMON/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAE,HME,HAF1,HMF1,HAF2,HMF2,  NFR
      1DUM(10),SNSQRT,QRAD,CQ,1D,IA ,SMOOTH  NFR
C HEIGHT ABOVE GROUND OF REF. PT.          NFR
      OH=RFEC-6370.00                         NFR
C NO - IS POINT OF INTEREST ABOVE E LAYER MAX NFR
      IF(OH.GT.HME) GO TO 201                 NFR
      IF(ID.EQ.1) GO TO 2001                 NFR
C IS PT. OF INTEREST BELOW E LAYER          NFR
      IF((HME-OH).GE.HAE) GO TO 300           NFR
C NO - SOLVE FOR E LAYER PLASMA DENSITY    NFR
      F02=FCE*FCE*(1.00-((HME-OH)/HAE)**2)  NFR
      GO TO 202                               NFR
C E LAYER WITH D LAYER TAIL                NFR
2001  ZP=2.00*(HME-OH)/HAE                 NFR
      K=1.500*DSQRT(1.700/(1.700+ZP))       NFR
      J=1.00+(ZP-1.00)*DABS(ZP-1.00)/10.00  NFR
      J=J/(1.00-.100/(1.00+ZP)**2)           NFR
      ZPP=2.00                                NFR
      IF(ZP.GT.0.00) ZPP=2.00-0.5LOG(1.00+1.7200*ZP**K)  NFR
      IF(ZPP.LE.0.00) GO TO 300               NFR
      ZPP=2.00-ZPP**J                         NFR
      F02=FCE*FCE*(1.00-ZPP*ZPP/4.00)        NFR
      GO TO 202                               NFR
C SOLVE FOR REF. HTS. 1 THRU 3            NFR
201   HS2=HMF2-HAF2*DSQRT(1.00-(FCF1/FCF2)**2)  NFR
      HS1=HMF1-HAF1*DSQRT(1.00-(FCE/FCF1)**2)  NFR
      HT2=(HS2+HMF1)/2.00                     NFR
C IS PT. OF INTEREST ABOVE REF PT 3        NFR
      IF(OH.GT.HT2) GO TO 203                 NFR
C NO- SOLVE FOR F1 LAYER PLASMA DENSITY   NFR
      BIGK1=(HS1-HME+HS2-HMF1)/(2.00*(FCF1-FCE))  NFR
      BIGK3=HAF1/FCF1                         NFR
      BIGK2=HMF1-(FCF1*(HS1-HME)+FCE*(HS2-HMF1))/(2.00*(FCF1-FCE))  NFR
      BIGA=BIGK1**2+BIGK3**2                  NFR
      BIGB=2.00*BIGK1*(BIGK2-OH)               NFR
      BIGC=OH**2-2.00*OH*BIGK2+BIGK2**2-HAF1**2  NFR
      F0=(-BIGB+DSQRT(BIGB**2-4.00*BIGA*BIGC))/(2.00*BIGA)  NFR
      IF(F0.LT.FCE) F0=FCE                   NFR
      F02=F0*F0                               NFR
      GO TO 202                               NFR
C SOLVE FOR DENSITY ABOVE F2 LAYER MAX    NFR
211   OHH=(OH-HMF2)/OH                     NFR
      Z=(OH-HMF2)/HAF2**2.00                 NFR
      F02=FCF2**2*DEXP(1.00-Z-DEXP(-Z))+(0.500+FCF2/10.000)*OH*HMF2/OH  NFR
      F02=DMIN1(F02,FCF2**2)                 NFR
      GO TO 202                               NFR
C IS POINT OF INTEREST ABOVE F2-LAYER MAX  NFR
203   IF(OH.GT.HMF2) GO TO 211             NFR
C NO-SOLVE FOR F2-LAYER PLASMA DENSITY    NFR
      BIGK1=(HS2-HMF1)/(2.00*(FCF2-FCF1))  NFR
      BIGK3=HAF2/FCF2                         NFR
      BIGK2=HMF2-FCF2*BIGK1                  NFR

```

ROUTINE NFROMR 74/74 OPT=1

FTN 4.5+414

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```
BIGA=BIGK1**2+BIGK3**2 NFR
BIGB=2.00*BIGK1*(BIGK2-OH) NFR
BIGC=OH**2-2.00*OH*BIGK2+BIGK2**2-HAF2**2 NFR
FO=(-BIGB+DSQRT(BIGB**2-4.00*BIGA*BIGC))/(2.00*BIGA) NFR
FO2=FO*FO NFR
202 PLASD=FO2*12400.00 NFR
IF(ID.EQ.1) GO TO 301 NFR
RETURN NFR
300 PLASD=0.00 NFR
IF(ID.EQ.0)RETURN NFR
301 CQ=DCOS(QRAD*.85D0) NFR
IF(CQ.GT.0.0D0) GO TO 302 NFR
CQ=0.00 NFR
RETURN NFR
302 CQ=CQ**(.25D0) NFR
303 PLASD=PLASD+SNSQRT*SNSQRT*CQ*1.02/(1.00+81.00*((65.00-OH)/HAE)**4) NFR
RETURN NFR
END NFR
```

ROUTINE DFP

74/74 OPT=1

FTN 4.5+414

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```

SUBROUTINE DFP(NLATA,WLONGA,NLATB,WLONGB,DIST)          DFP
IMPLICIT DOUBLE PRECISION (A-H,O-Z)                    DFP
DOUBLE PRECISION NLATA,NLATB                          DFP
DATA RAD/57.29577951308232D0/                      DFP
Dacos(DUMMY)=DATAN2(DSQRT(1.000-DUMMY*DUMMY),DUMMY)  DFP
C   SHIFT INPUT LAT. BY ONE QUADRANT                   DFP
PPA=90.000-NLATA                                      DFP
PPB=90.000-NLATB                                      DFP
GGH=WLONGA                                         DFP
GGK=WLONGB                                         DFP
C   FIND SMALLEST ANGULAR DIFF. BETWEEN A AND B       DFP
HHGK=GGH+GGK                                         DFP
ABHHGK=DABS(HHGK)                                    DFP
HHK=ABHHGK                                         DFP
IF(HHK.GT.180.00)HHK=360.00-HHK                      DFP
C   SOLVE FOR BEARING FROM A TO B                     DFP
RAAPB=HHK/RAD                                         DFP
CSAAPB=DCOS(RAAPB)                                    DFP
RPPA=PPA/RAD                                         DFP
SINPPA=DSIN(RPPA)                                    DFP
COSPPA=DCOS(RPPA)                                    DFP
RPPB=PPB/RAD                                         DFP
SINPPB=DSIN(RPPB)                                    DFP
COSPPB=DCOS(RPPB)                                    DFP
COSAAB=COSPPA*COSPPB+SINPPA*SINPPB*CSAAPB        DFP
RAAB=Dacos(COSAAB)                                    DFP
C   SOLVE FOR GREAT CIRCLE DISTANCE BETWEEN A AND B  DFP
DIST=6370.000*RAAB                                     DFP
RETURN                                              DFP
END                                                 DFP

```

ROUTINE MMDIP 74/74 OPT=1

FTN 4.5+414

04/27/

```

SUBROUTINE MMDIP(NLAT,WLONG,SSMX) DMM
  IMPLICIT DOUBLE PRECISION (A-H,O-Z) DMM
C COMPUTE MAGNETIC FIELD COMPONENTS MAGNETIC DIP AND MODIFIED MAGNETIC DMM
C DIP DMM
  DOUBLE PRECISION NLAT DMM
  DIMENSION P(7,7),DP(7,7),CP(7),AOR(7),SP(7) DMM
  DIMENSION CT(7,7),H(7,7),G(7,7) DMM
  DATA P,DP,SP/1.000,104*0.000/,CP/1.000,6*0.000/ DMM
  DATA RD/57.29577951308232D0 /,HC/6371.203/ DMM
  DATA CT/2*0.00,.33333333D0,.26666667D0,.25714286D0, DMM
1  .25396825D0,.25252525D0,3*0.00,.200,.22857142D0,.23809523D0, DMM
2  .24242424D0,4*0.00,.14285714D0,.19047619D0,.21212121D0, DMM
3  5*0.00,.11111111D0,.16161616D0,6*0.00,.09090909D0,14*0.00/ DMM
  DATA G/0.00,.304112D0,.024035D0,-.031518D0,-.041794D0, DMM
1  .016256D0,-.019523D0,0.00,.021474D0,-.051253D0, DMM
2  .062130D0,-.045298D0,-.034407D0,..004853D0,2*0.00, DMM
3  -.013381D0,-.024898D0,-.021795D0,-.019447D0,.003212D0, DMM
4  3*0.00,-.006496D0,.007008D0,-.006060D0,.021413D0, DMM
5  4*0.00,-.002044D0,.002775D0,.001051D0,5*0.00,.000697D0, DMM
6  .000227D0,6*0.00,.001115D0/ DMM
  DATA H/8*0.00,-.057989D0,.033124D0,.014870D0,-.011825D0, DMM
1  -.000796D0,-.005758D0,2*0.00,-.001579D0,-.004075D0, DMM
2  .010006D0,-.002D0,-.008735D0,3*0.00,.00021D0,.00043D0, DMM
3  .004597D0,-.003406D0,4*0.00,.001385D0,.002421D0, DMM
4  -.000118D0,5*0.00,-.001218D0,-.001116D0,6*0.00, DMM
5  -.000325D0/ DMM
  P1=NLAT DMM
  P2=360.000-(WLONG) DMM
  IF(P1-89.9D0)2,4,1 DMM
1  P1=89.9D0 DMM
  P2=0.00 DMM
  GO TO 4 DMM
2  IF(P1+89.9D0)3,4,4 DMM
3  P1=-89.9D0 DMM
  P2=0.00 DMM
4  PHI=P2/RD DMM
  AR=HC/(HC+3.D5) DMM
  C=DSIN(P1/RD) DMM
  S=DSQRT(1.-C**2) DMM
  SP(2)=DSIN(PHI) DMM
  CP(2)=DCOS(PHI) DMM
  AOR(1)=AR**2 DMM
  AOR(2)=AR**3 DMM
  DO 5 M=3,7 DMM
  SP(M)=SP(2)*CP(M-1)+CP(2)*SP(M-1) DMM
  CP(M)=CP(2)*CP(M-1)-SP(2)*SP(M-1) DMM
5  AOR(M)=AR*AOR(M-1) DMM
  BV=0.00 DMM
  BN=0.00 DMM
  BPHI=0.00 DMM
  DO 6 N=2,7 DMM
  FN=DBLE(FLOAT(N)) DMM
  SUMR=0.00 DMM
  SUMT=0.00 DMM
  SUMP=0.00 DMM
  DO 7 M=1,N DMM
  IF(N-M)8,9,8 DMM

```

ROUTINE MMDIP 74/74 OPT=1

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9   P(N,N)=S*P(N-1,N-1)          DMM
    DP(N,N)=S*DP(N-1,N-1)+C*P(N-1,N-1)  DMM
    GO TO 10                      DMM
8   P(N,M)=C*P(N-1,M)-CT(N,M)*P(N-2,M)  DMM
    DP(N,M)=C*DP(N-1,M)-S*P(N-1,M)-CT(N,M)*DP(N-2,M)  DMM
10  FM=DBLE(FLOAT(M-1))          DMM
    TS=G(N,M)*CP(M)+H(N,M)*SP(M)  DMM
    SUMR=SUMP+P(N,M)*TS          DMM
    SUMT=SUMT+DP(N,M)*TS          DMM
7   SUMP=SUMP+FM*P(N,M)*(-G(N,M)*SP(M)+H(N,M)*CP(M))  DMM
    BV=BV+AOR(N)*FN*SUMR          DMM
    BN=BN-AOR(N)*SUMT          DMM
6   BPHI=BPHI-AOR(N)*SUMP          DMM
    COSLAM=DCOS((NLAT)/RD)          DMM
    COM1=-BV                      DMM
    COM2=BN                      DMM
    COM3=-BPHI/S          DMM
    TMP=COM2**2+COM3**2          DMM
    BIGI=DATAN(-COM1/DSQRT(TMP))  DMM
    SSMX=(BIGI/DSQRT(BIGI**2+COSLAM))  DMM
C   NEXT CARD DELETED DSINCE SMX NOT USED BY CRPL2  DMM
C   SMX=DASIN(SSMX)          DMM
    RETURN                      DMM
    ENO                         DMM

```

ROUTINE PEP.F

74/74 OPT=1

FTN 4.5+414

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```

SUBROUTINE PERTF(T,NL,HL,FCF20)
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
DOUBLE PRECISION NLREF,MR,MZ,MD,NL
COMMON/PERTC/NLREF,HLREF,FR,FD,MR,MD,FZ,MZ,DUT,DW,X,GAMMA,AZM
1 DFAC,DMAC,AZREF
RTD=57.29577951308232D0
CALL DFP3(NLREF,HLREF,NL,HL,DIST,AZ)
AZ=AZ-AZREF
STHINV=1.0D0/DABS(DSIN((AZM-(90.0D0+GAMMA))/RTD))
Y=DUT*360.0D0*X*STHINV
W=DW*STHINV
SD=DSIN((DIST+Y)/W*360.0D0/RTD)
FCF20=FCF20*(1.0D0+FZ*SD)*(1.0D0+FR*DIST/FD)*(1.0D0+AZ*DFAC)
FCF20=AMAX1(.51D0,FCF20)
RETURN
ENTRY PERTM(T,NL,HL,FCF20)
FCF20=FCF20*(1.0D0+MZ*SD)*(1.0D0+MR*DIST/MD)*(1.0D0+AZ*DMAC)
FCF20=AMAX1(1.0D0,FCF20)
RETURN
END

```

ROUTINE FACTO 74/74 OPT=1

FTN 4.5+414

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```
SUBROUTINE FACTO(NLREF, WLREF, FCF2R, HMINR, ZTREF)          FAC
IMPLICIT DOUBLE PRECISION(A-H,0-Z)                          FAC
DOUBLE PRECISION KK, M3000P, M3000R, MFAC, MM, NLREF, K1    FAC
COMMON/FACCOM/F1, ZZ, KK, P3000                          FAC
COMMON/RIIPAR/M3000P, FCF2, FCF1, FCE, HBE, HAE, HME, HAF1, HMF1, HPF2,  FAC
1 HMF2, SNS(5), MFAC, F2FAC, DUM(6), IDUM(3)             FAC
DATA RTD/57.2957795130823200/                           FAC
F2FAC=1.00                                              FAC
MFAC=1.00                                              FAC
IF(FCF2R.EQ.0.00) RETURN                                FAC
ZTS=SNS(2)                                              FAC
SNS(2)=ZTREF                                         FAC
CALL CRPL2(NLREF, WLREF)                                FAC
F2FAC=DABS(FCF2R/FCF2)                                FAC
IF(HMINR.EQ.0.00) GO TO 10                            FAC
CALL RIIP(6370.00, NLREF/RTD, WLREF/RTD, PLASD)        FAC
P1=(FCF2+3.78D0*FCE+1.500)/FCF1*DLOG((FCF2+8.82D0*FCE+3.500) /  FAC
1 (FCF2-FCF1))                                         FAC
MM=HAE/8.00                                              FAC
Z1=MM*(FCF2+3.7800*FCE+1.500)/FCE*DLOG((FCF2+7.7800*FCE+1.500) /  FAC
1 (FCF2-.22D0*FCE+1.500))                            FAC
FFM=FCF1+(FCF2-FCF1)/4.00                            FAC
FF1=FFM/FCF2                                         FAC
K1=50.D0*DLOG((1.00+FF1)/(1.00-FF1))                FAC
H3000=P3000/P1*(DABS(HMINR)-Z1-HBE-HPF2*K1/100.00)+ZZ+HBE+KK  FAC
M3000R=(FM/FCF2)*DSQRT(3100.00/(H3000-70.00))        FAC
MFAC=DSIGN(M3000R/M3000P, HMINR)                      FAC
10 F2FAC=DSIGN(F2FAC, FCF2R)                           FAC
SNS(2)=ZTS                                         FAC
RETURN                                              FAC
END                                              FAC
```

Appendix B

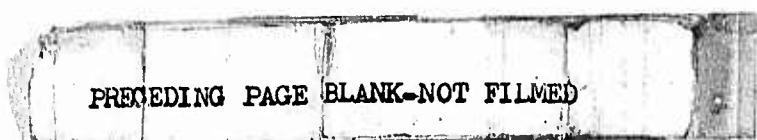
Block Diagram and Flow Chart for WIMP Ray-Tracing Program TRISL

Explanation:

BI. TRISL BLOCK DIAGRAM

This presentation shows the general communication network among the various functional processes of TRISL, and illustrates the iterative complications inherent in the program. The function of the various blocks is generally described as follows:

- BLOCK I: Initialization Procedures.
- BLOCK II: E-layer refraction upwards.
- BLOCK III: F_1 -layer refraction upwards.
- BLOCK IV: Reflection layer initialization.
- BLOCK V: Tilt calculation and consistency checks.
- BLOCK VI: F_1 -layer refraction downwards.
- BLOCK VII: E-layer refraction downwards.
- BLOCK VIII: Error checks.
- BLOCK IX: Iterate reflection and tilt.
- BLOCK X: Traffic control.
- BLOCK XI: Normal Terminal calculations.
- BLOCK XII: ERROR exits.



B2. DETAILED FLOW CHARTS

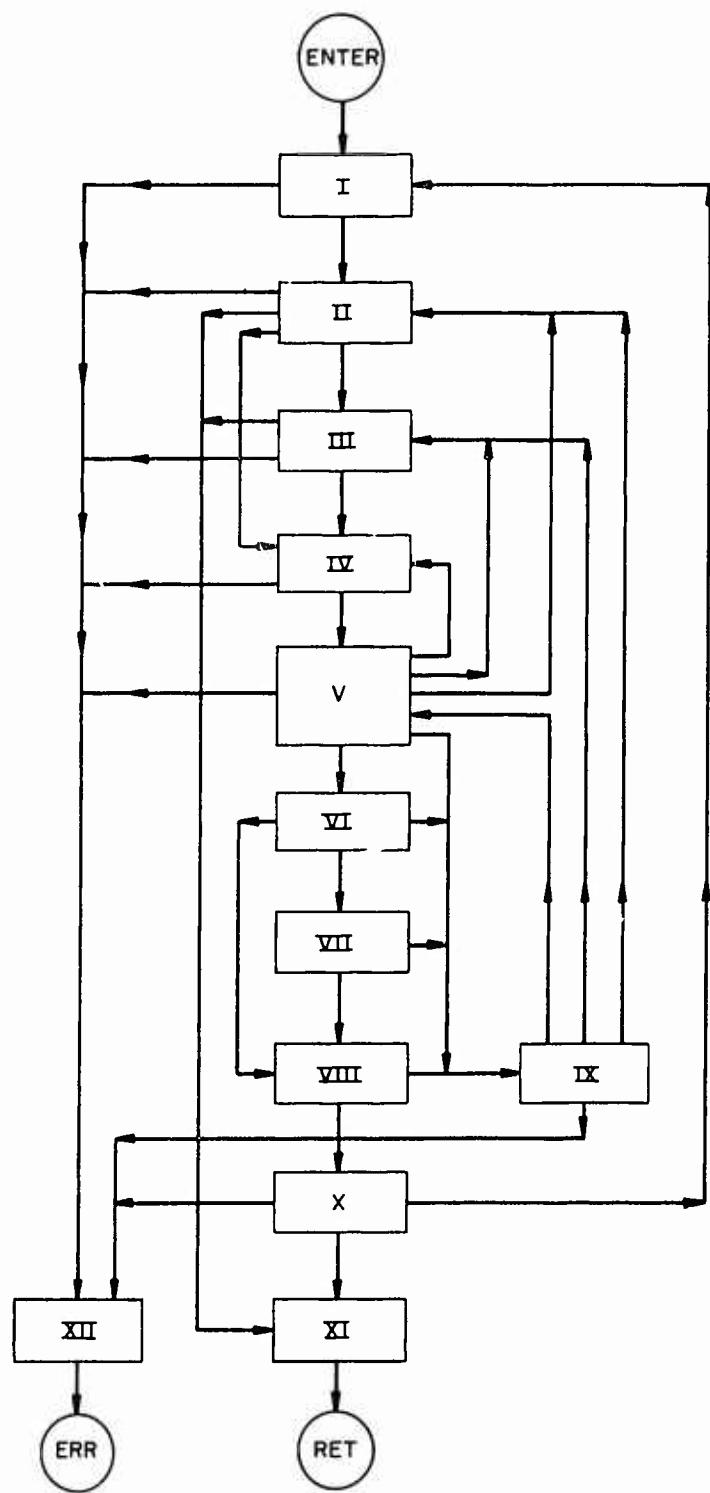
Detailed flow charts are presented for each block. Most line members of TRISL are accounted for except when so doing unduly complicates comprehension of the process.

B3. FLOW CHART SYMBOLS AND CONVENTIONS

- (a) Process entry/exit point.
- (b) Processing statements.
- (c) Decision trees, two or three way branches.
- (d) External procedures.
- (e) Numbers in the form Snnn refer to statement numbers in the program.
- (f) Numbers in the form nnn refer to line numbers of the program listing.
- (g) Entry points to a block are labelled generally with block designation statement number and line number specifying the source.
- (h) Exit points from a block are generally labelled by block designation, statement number, and line number specifying the destination.
- (i) Error exits are labelled by an error number and the error condition detected.
- (j) Exits from the bottom generally enter the next block at the top.
- (k) External call names and calling line numbers are contained within the external procedure symbols.

B4. PROGRAM LISTING

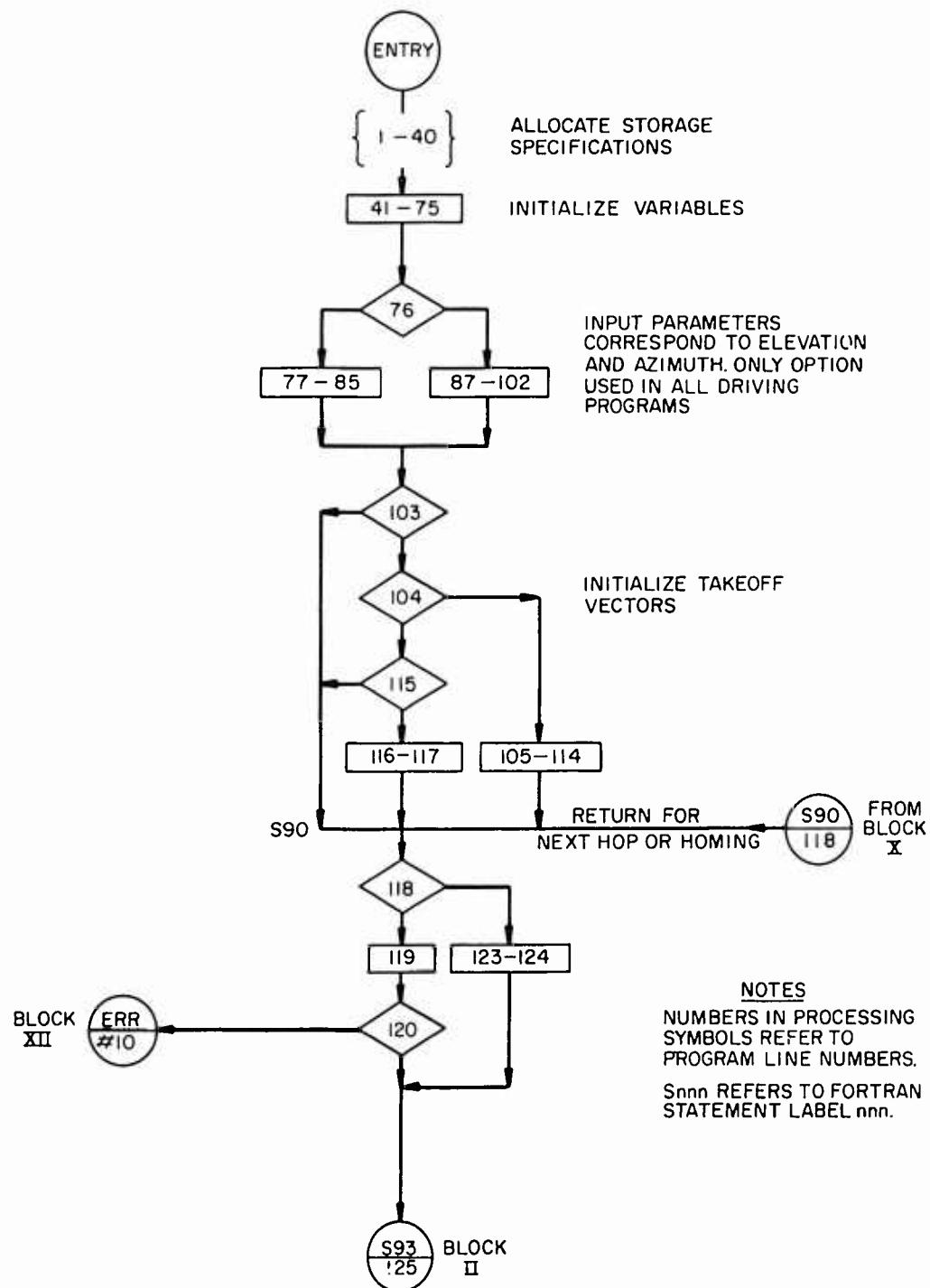
Listings are included for TRISL together with its externals.



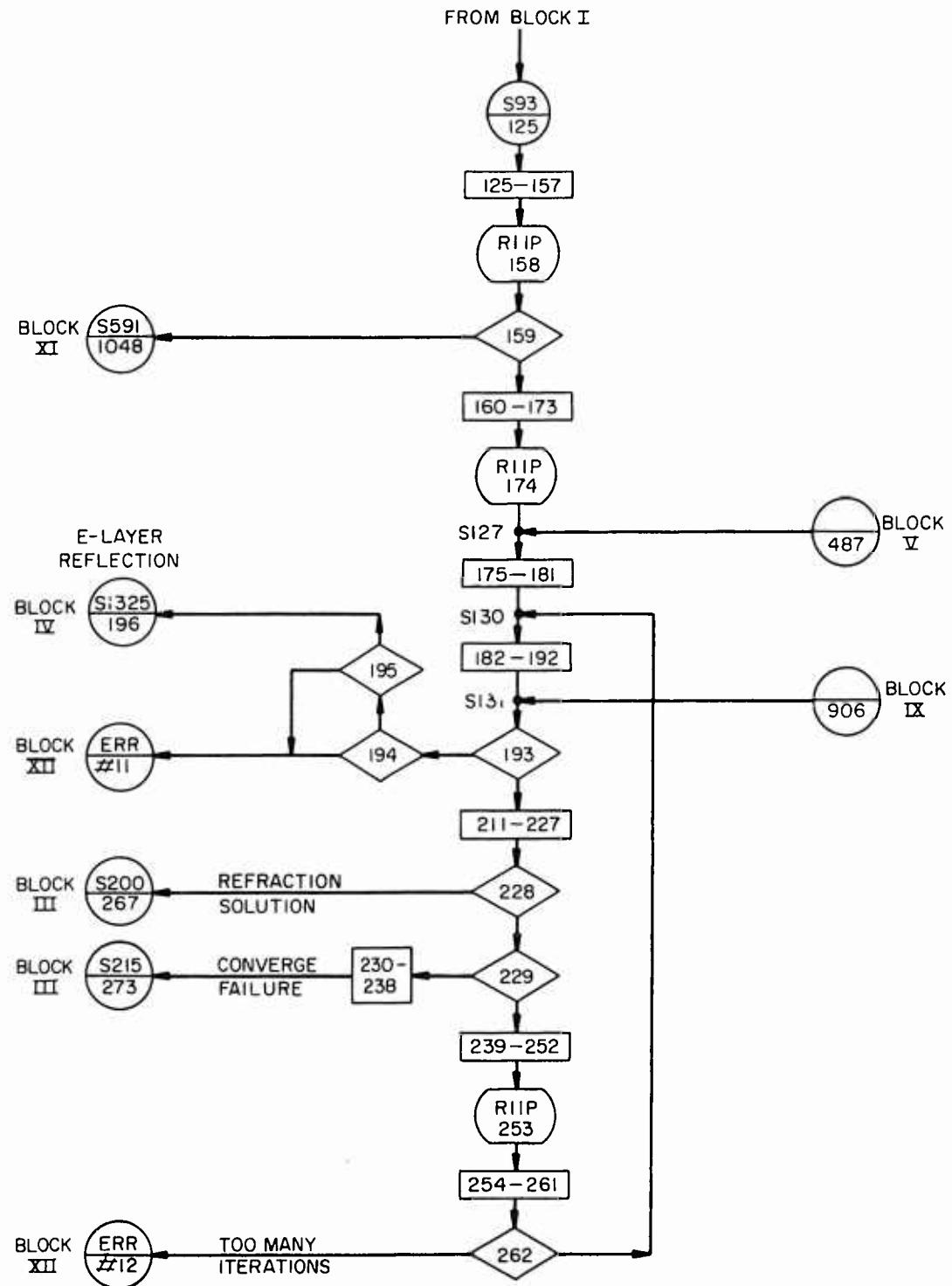
TRISL Block Diagram

TRISL: Block I, Argument List

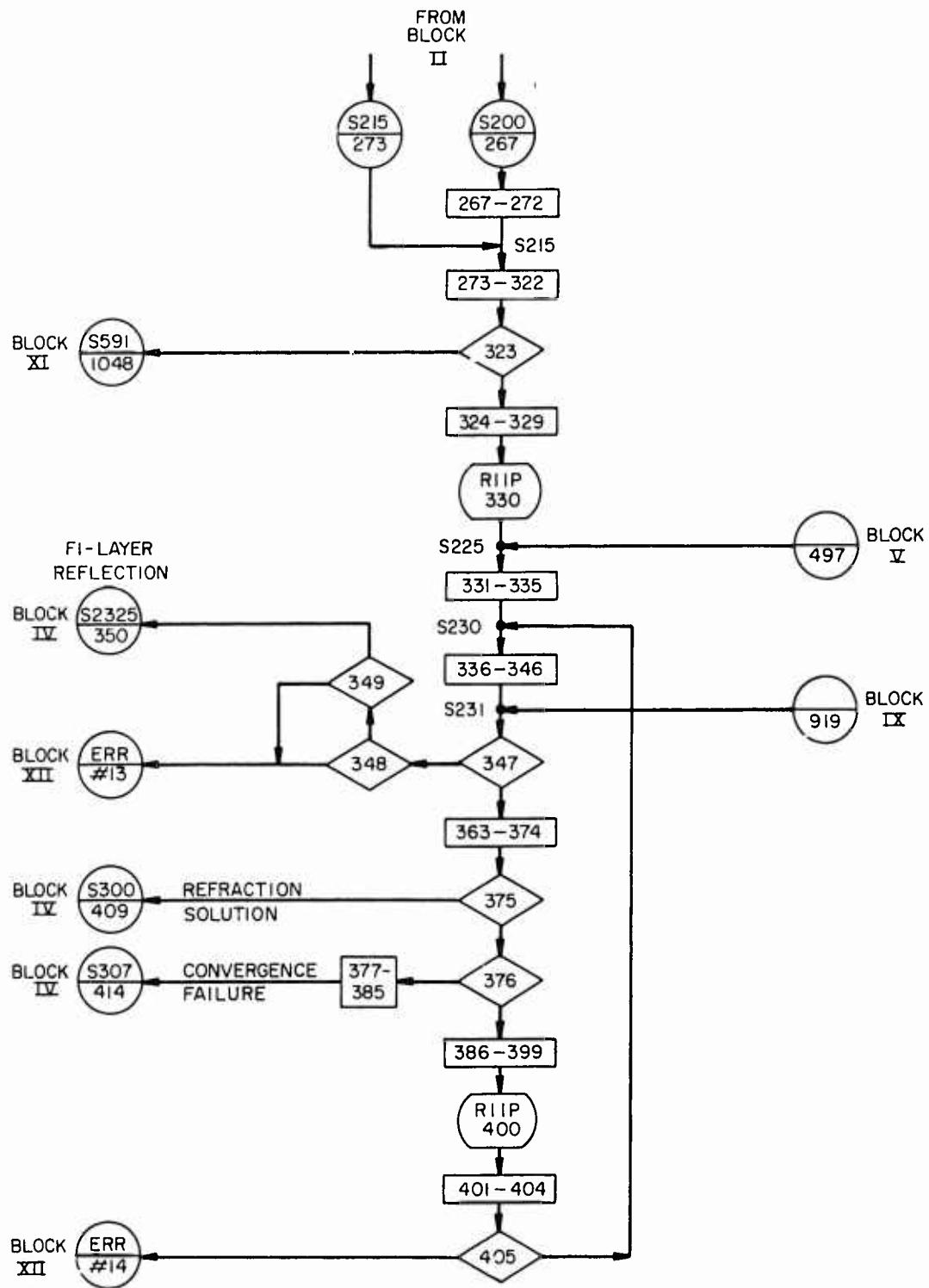
Element	I/D	Mnemonic	Type	Definition
1	I	MAI	Double	Geocentric Distance, Initial Point
2	I	NLAI	Double	North Latitude, Initial Point
3	I	WLAI	Double	West Longitude, Initial Point
4	I	NLAZ	Double	Takeoff Bearing (all calls) or Target North Latitude
5	I	WLAZ	Double	Takeoff Elevation (all calls) or Target West Longitude
6	I	MAZ	Double	Less than 6000 km (all calls) or Target Geocentric Distance
7	I	FREQ	Double	Frequency
8	I	MODE	Integer	MODE = Number of hops = 6370 km, (all calls)
9	I	RTARG	Double	
10	O	RS 2	Double	Geocentric Distance, End Point
11	O	NLTARG	Double	North Latitude, End Point
12	O	WLTARG	Double	West Longitude, End Point
13	O	PPTOT	Double	Phase Path Length
14	O	GPTOT	Double	Group Path Length
15	O	AZF	Double	Final to Initial Azimuth
16	O	ELF	Double	End Point Elevation
17	O	SRANGE	Double	Final-Initial Straight Line Distance
18	O	ELSR	Double	Takeoff Elevation
19	O	DIST	Double	Final-Initial Great Circle Ground Range
20	O	BEAR	Double	Initial to Final Azimuth
21	O	IGOBAK	Integer	Error Flag 8 = 0 No Error = 1 Fatal Error = 2 Penetrate



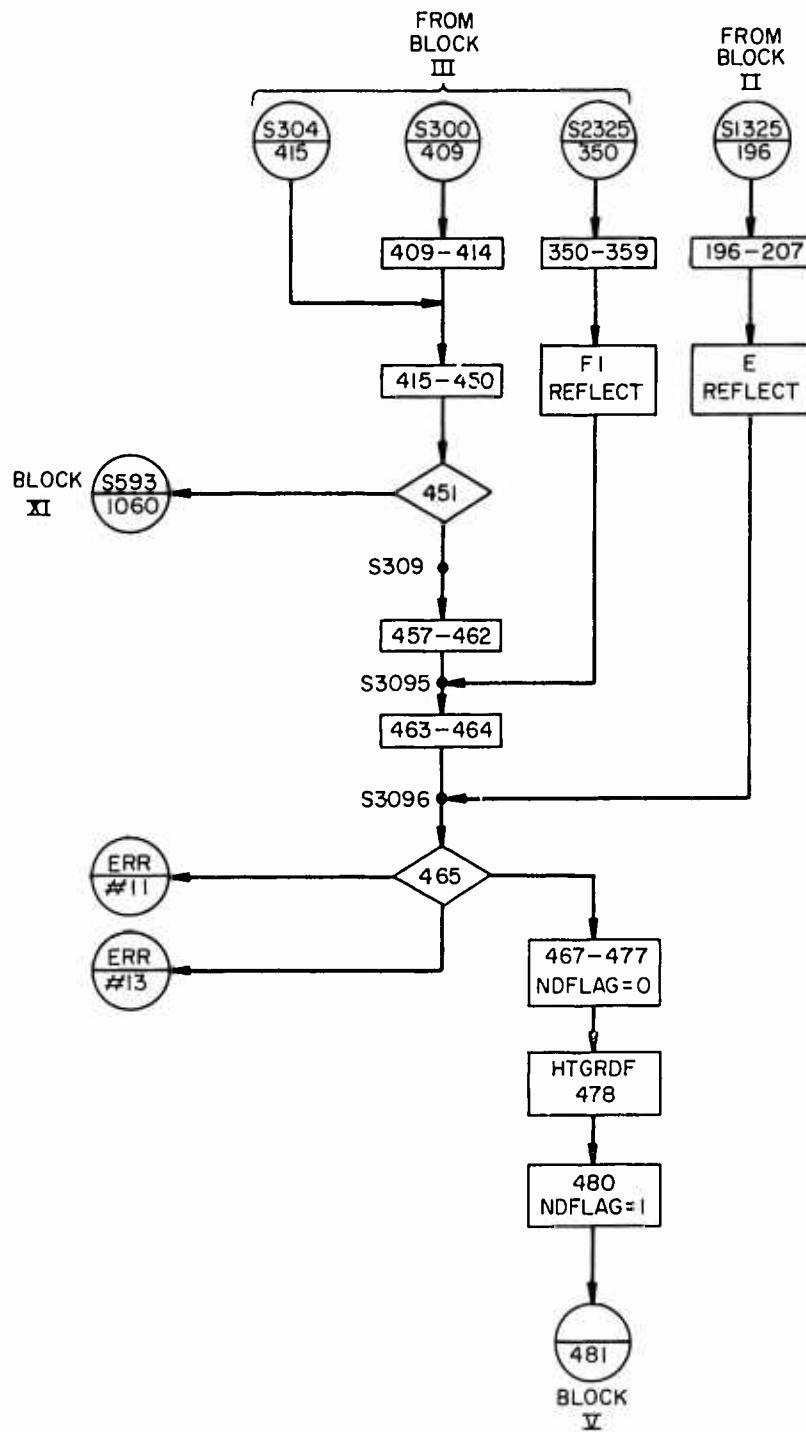
Block I, Initialization Procedures



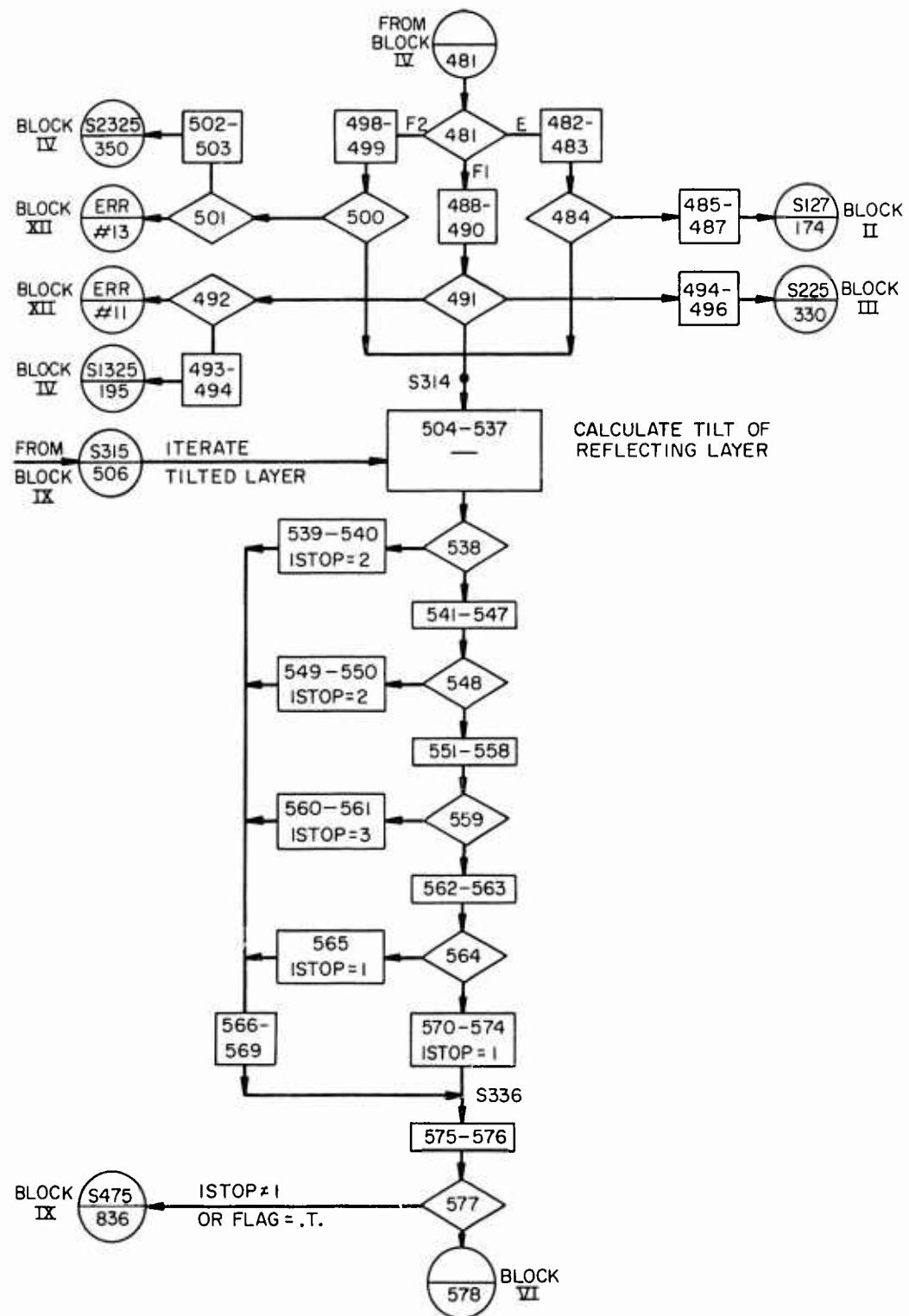
Block II, E-Layer Refraction Upwards



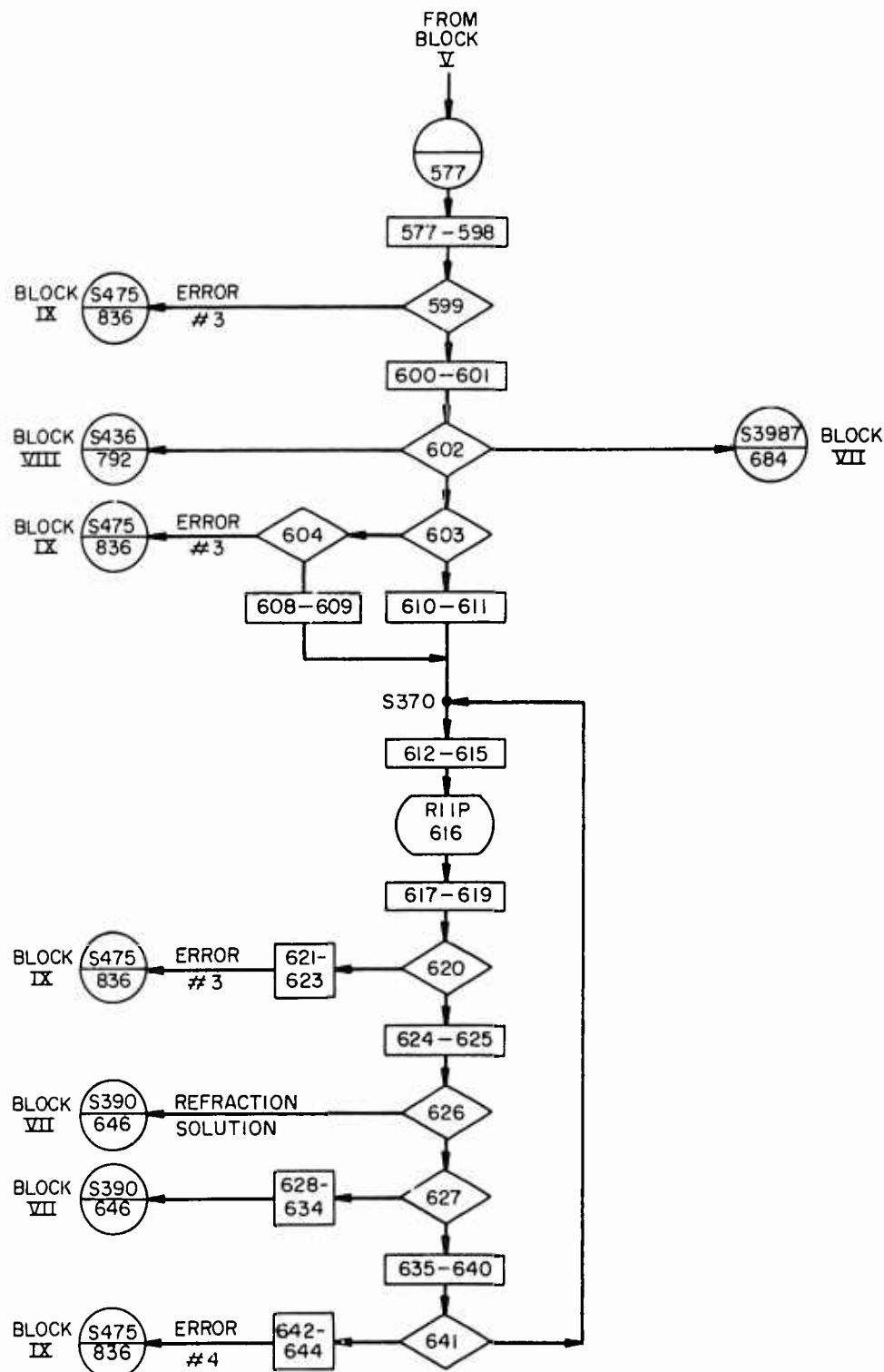
Block III, F_1 -Layer Refraction Upwards



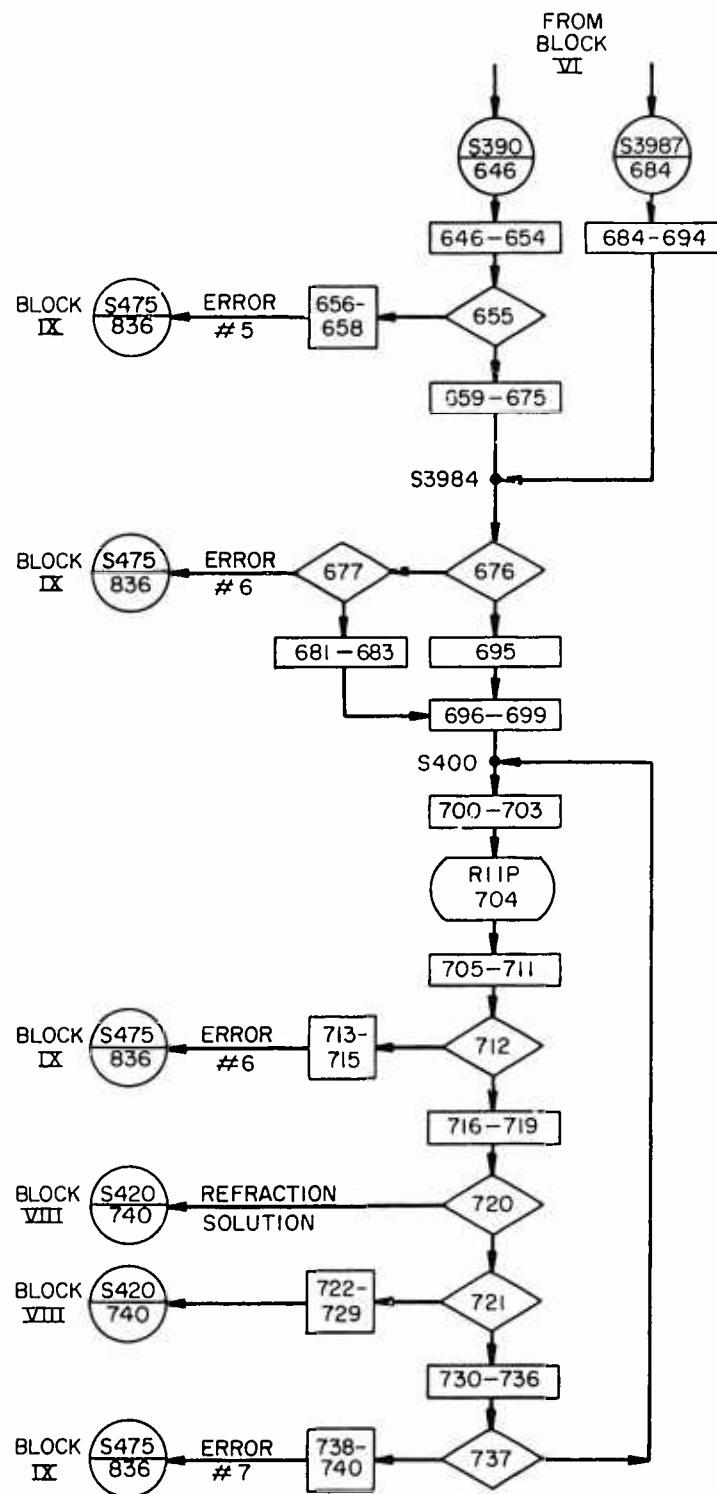
Block IV, Reflection Layer Initialization



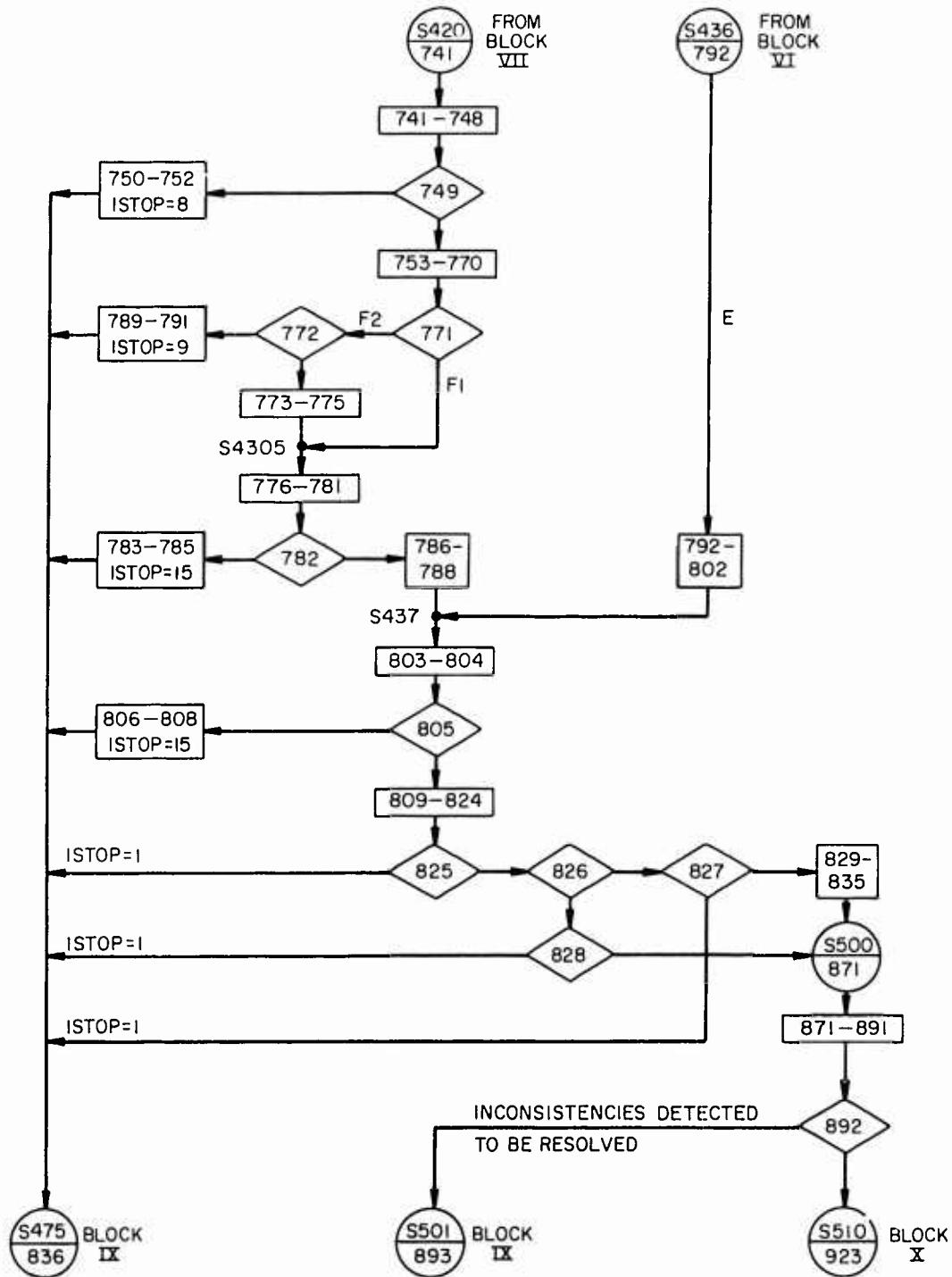
Block V, Tilt Calculation and Consistency Checks



Block VI, F_1 -Layer Refraction Downwards



Block VII, E-Layer Refraction Downwards

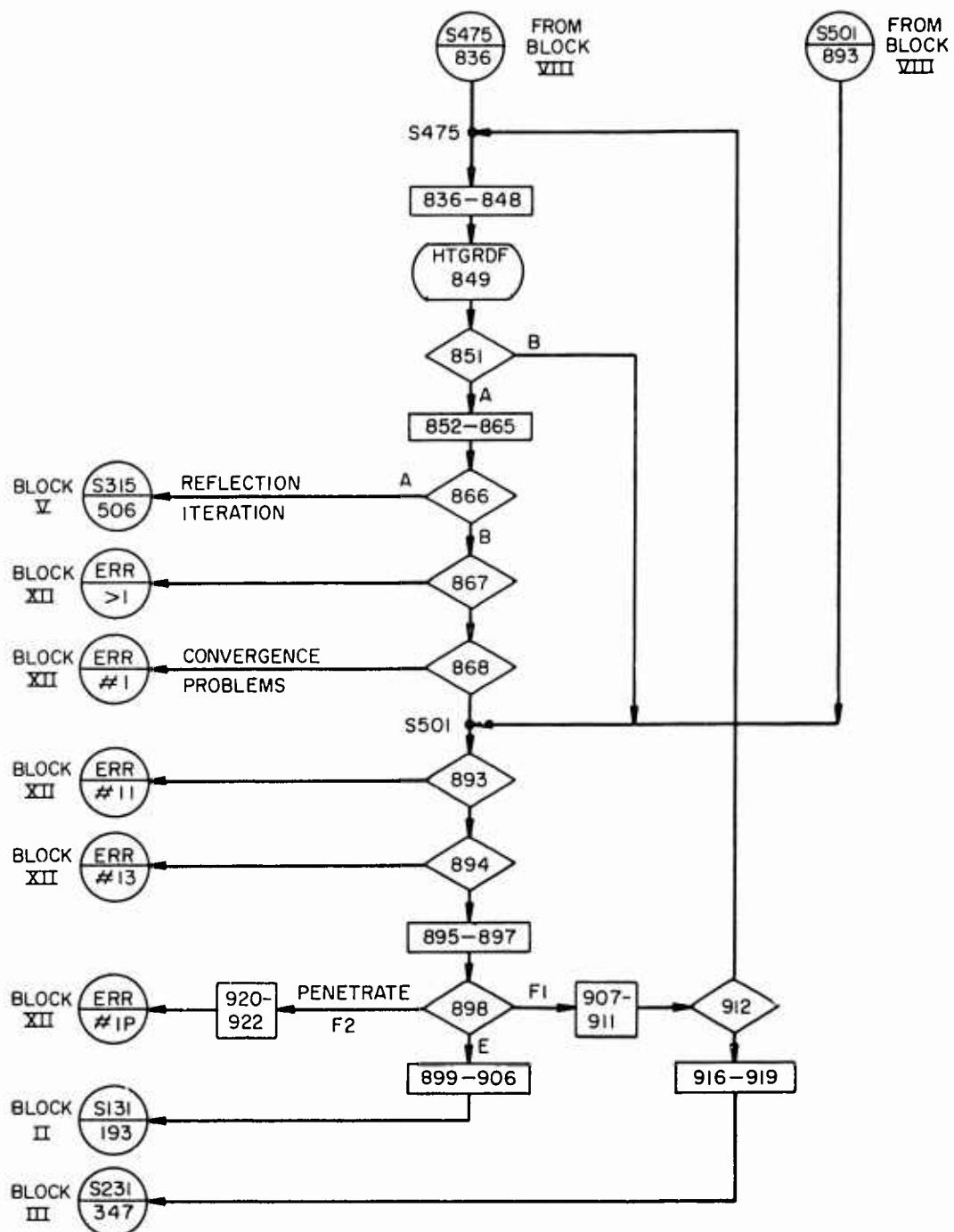


NOTES

BLOCK X EXIT IS DESIRED CONVERGENT SOLUTION TO
TILTED LAYER ITERATION

THE ISTOP=1 EXITS TO S475 ARE NORMAL. THE OTHER
ERROR CONDITIONS MAY BE CORRECTED IN SUCCEEDING
ITERATIONS

Block VIII, Error Checks



-851-

BRANCH B-INCONSISTENCY
BETWEEN HTGRDF AND
REST OF PROGRAM A PRO
PO REFLECTION LAYER

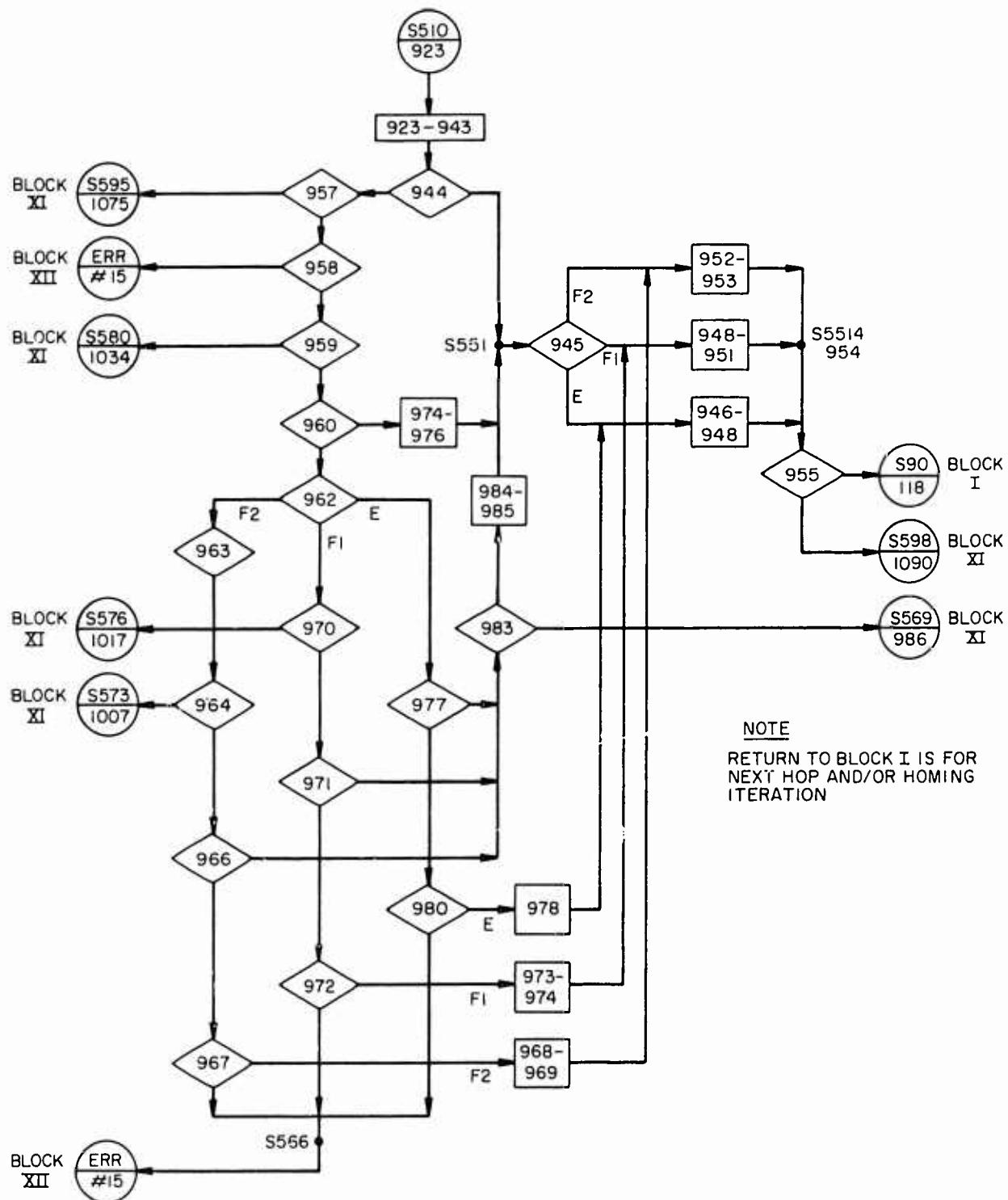
-866-

BRANCH B-
ITERATION LIMIT
EXCEEDED

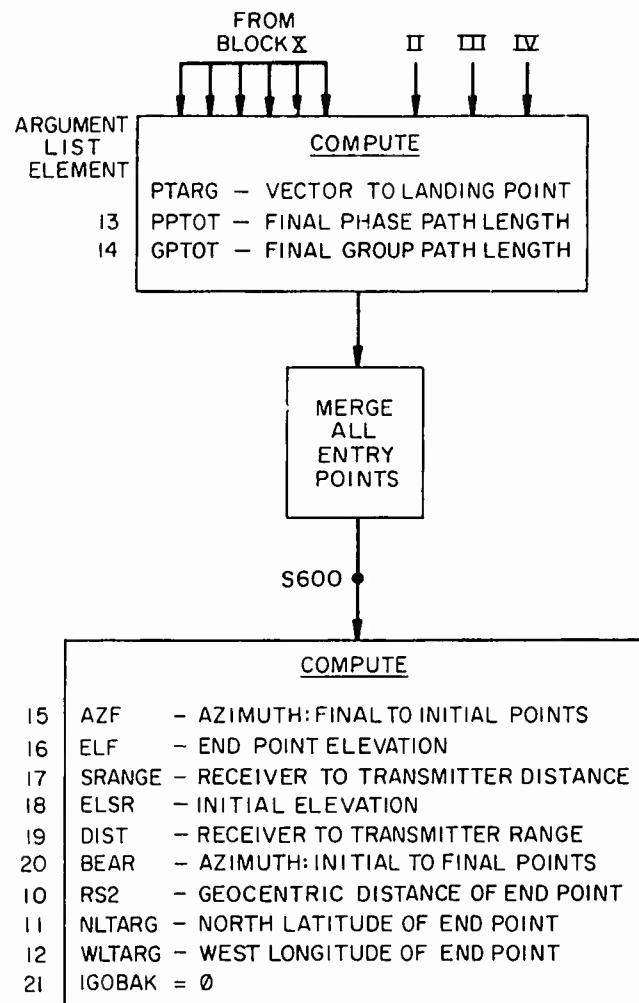
-898-

E-E LAYER REFLECTION
F1-F1 LAYER REFLECTION
RETURNS TO BLOCK II OR
III TO RESOLVE INCON-
SISTENCIES DETECTED IN 851

Block IX, Iterate Reflection and Tilt



Block X, Traffic Control



Block XI, Normal Terminal Calculations

OUTINE TRISL

74/74 OPT=1

FTN 4.5+414

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```

SUBROUTINE TRISL(MA1,NLA1,WLA1,NLA2,WLA2,MA2,FREQ,MODE,RTARG,RS2, TR2
*NLTARG,WLTARG,PPTOT,GPTOT,AZF,ELF,S RANGE,ELSR,DIST,BEAR,IG0BAK) TR2
IMPLICIT DOUBLE PRECISION (A-H,O-Z) TR2
LOGICAL HITS,FLAG,SEARCH,ASC,FLAG2,FLAG3,NOELAY,INCHOP,LP(6),NIP TR2
LOGICAL GPONLY TR2
DOUBLE PRECISION MESSPR TR2
DOUBLE PRECISION NLA1,MA1,NLA2,MA2,NLTARG,MAG,MA1B1,MB1,NLC1,NL4, TR2
1MRX1SQ,NLC2,MR3,NL8,NLC3,MN1,MA2C2,MC2,MA3C3,MC3,NLD,MRM1,MRM2, TR2
2MRY1SQ,MC4SQ,NLE,MRM3,MRM4,MC5SQ,NLW2,KP,L,N1,M,KPPP,LOC, TR2
3MAGVEC,NORTH(3),ME,MN,NORTH1(3),EAST1(3),MR2,MC1PSQ,M3000 TR2
REAL OUT2 TR2
DIMENSION S1(3),A1(3),B1(3),A11(3),EAST(3),MESSPR(15), TR2
* XI(3),KP(3),L(3,3),P1P(3),PC2(3),P8(3),R3(3),PC3(3),P10(3),C TR2
*2(3),PR1(3),N1(3),P0(3),A2(3),M(3,3),C3(3),A3(3),PHI(3),KPPP(3),P( TR2
*3,3),PD(3),PE(3),PQ(3),PH2(3),H2(3),PTARG(3), RN1(3),R2(3) TR2
*),PC1(3),P4(3) TR2
COMMON/FLIMSY/DIST1,ICNPRB /GPFLAG/GPONLY,IWRITE TR2
COMMON/CPREV/PQ,P,RT1,C52PPP,C53PPP,MRM1,CBETM1,MRM4,RY, TR2
2 DPP1P,HC5SQ,RM1,YY2PPP,ZY2PPP,H1,MC4SQ,MRY1SQ,YY1PPP, TR2
2 ZY1PPP,C42PPP,C43PPP,YS3PPP,ZS3PPP,C32PPP,RTM1,DNDR,DNDNL, TR2
3 DNDWL,D,GNU,PP2,PPEF1D,CBETM2,HE,PPF2,RV,HF1,PP2A,DPP2P, TR2
4 MB1,SBET1,GPF2,GPEF1D,DPGP2P,DPGP1P, TR2
5 F1,PREV(56),HITS,INCHOP,FLAG,FLAG2,FLAG3,NOELAY,LP TR2
COMMON/VECTRS/LOC(3,8),VEC(3,6),IREFL TR2
COMMON/NIPRIP/NIP TR2
*/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAE,HME,HAF1,HMF1,HAF2,HMF2,DUM(13 TR2
*),ID(3)/RTCOM/COSBO,NUSE TR2
COMMON/REMHEN/INUSE,NNUSE(20),FCREF(20) TR2
DATA R,EPS1,EPS2,EPS3,EPS4,EPS5/6670.00,5*1.00/ TR2
DATA PI,RTD,DTR,R0/3.141592653589793D0,57.29577951308232D0, TR2
*.0174532925199433D0,6370.00/ TR2
DATA LIMEA,LIMF1A,LIMF1D,LIMED,LIMF2/5*15/ TR2
DATA MESSPR/7HF2 ITER,8HBIG TILT,8HBIG TILT,9HF1-D ITER, TR2
1 9HF1-D REFL,7HF1 MISS,8HE-D ITER,8HE-D REFL,6HE MISS, TR2
2 8HI-I REFL,9HE-F1 DUCT,8HE-A ITER,10HF1-F2 DUCT, TR2
3 9HF1-A ITER,9HMISS TARG/ TR2
WLON(ARG1,ARG2)=DSIGN(PI,ARG1)+PI-DATAN2(ARG1,ARG2) TR2
DACOS(ARG1)=DATAN2(DSQRT(1.00-ARG1**2),ARG1) TR2
DASIN(ARG1)=DATAN2(ARG1,DSQRT(1.00-ARG1**2)) TR2
INCHOP=.TRUE. TR2
HITS=.TRUE. TR2
ASC=MODE.EQ.0 TR2
SEARCH=ASC TR2
PP0=0.00 TR2
PPEF1A=0.00 TR2
DPP1=0.00 TR2
PP2A=0.00 TR2
PPF2=0.00 TR2
PP2=0.00 TR2
PPEF1D=0.00 TR2
DPP2P=0.00 TR2
PP0P=0.00 TR2
PPTOT=0.00 TR2
GPTOT=0.00 TR2
GPEF1A=0.00 TR2
DGP1=0.00 TR2
DGP2=0.00 TR2

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GPEF1A=0.00          TR2
GPF2=0.00          TR2
GPEF1D=0.00          TR2
DGP2P=0.00          TR2
DGP1P=0.00          TR2
ICNPRB=0          TR2
INUSE=0          TR2
IGOBANK=0          TR2
IHOPS=0          TR2
RS2=RTARG          TR2
CN=DCOS(NLA1*DTR)          TR2
SN=DSIN(NLA1*DTR)          TR2
CW=DCOS(WLA1*DTR)          TR2
SH=DSIN(WLA1*DTR)          TR2
A1(1)=CN*CW          TR2
A1(2)=-CN*SH          TR2
A1(3)=SN          TR2
IF(MA2.LT.6000.00) GO TO 50          TR2
CN=DCOS(NLA2*DTR)          TR2
DO 45 I=1,3          TR2
A11(I)=MA1*A1(I)          TR2
A1(I)=A11(I)          TR2
45 B1(1)=MA2*DCOS(WLA2*DTR)*CN-A1(1)          TR2
B1(2)=-MA2*DSIN(WLA2*DTR)*CN-A1(2)          TR2
B1(3)=MA2*DSIN(NLA2*DTR)-A1(3)          TR2
MB1=MAG(B1)          TR2
DTA1B1=DOT(A1,B1)          TR2
GO TO 60          TR2
C WHEN MA2 IS INPUTTED AS A NUMBER LESS THAN 6000, NLA2 IS ASSUMED          TR2
C TO BE THE BEARING, AND WLA2 IS ASSUMED TO BE THE TAKE-OFF ANGLE          TR2
50 EAST1(1)=SN          TR2
EAST1(2)=CW          TR2
EAST1(3)=0.00          TR2
CALL CROSS(A1,EAST1,NORTH1)          TR2
CAZ=DCOS(NLA2*DTR)          TR2
SAZ=DSIN(NLA2*DTR)          TR2
CEL=DCOS(WLA2*DTR)          TR2
SEL=DSIN(WLA2*DTR)          TR2
DO 55 I=1,3          TR2
B1(I)=CEL*(CAZ*NORTH1(I)+SAZ*EAST1(I))+SEL*A1(I)          TR2
A11(I)=MA1*A1(I)          TR2
55 A1(I)=A11(I)          TR2
MB1=1.00          TR2
DTA1B1=SEL*MA1          TR2
60 IF(DABS(MA1-R0).LE.1.0-5) GO TO 90          TR2
IF(DASIN(R0/MA1)-DACOS(-DTA1B1/(MA1*MB1))88,88,80          TR2
80 T1=(-DTA1B1-0SQRT(DTA1B1**2-DOT(B1,B1)*(DOT(A1,A1)-R0**2)))          TR2
*/DOT(B1,B1)          TR2
DO 85 J=1,3          TR2
85 A1(J)=B1(J)*T1+A1(J)          TR2
A=-2.00*DOT(A1,B1)/DOT(A1,A1)          TR2
DO 87 J=1,3          TR2
87 B1(J)=B1(J)+A*A1(J)          TR2
PPTOT=T1*MB1          TR2
GPTOT=PPTOT          TR2
GO TO 90          TR2
88 IF(DTA1B1.GE.0.00) GO TO 90          TR2

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PPTOT=-2.00*DTA1B1/MB1          TR2
GPTOT=PPTOT                      TR2
90   IF(INCHOP) GO TO 92          TR2
IONREF=IONREF+1                  TR2
IF(IONREF.LT.40) GO TO 93          TR2
ISTOP=10                          TR2
GO TO 7310                        TR2
92   IONREF=0                      TR2
IHOPS=IHOPS+1                      TR2
93   PREV(13)=0.00                  TR2
C   START OF E LAYER REFRACTION   TR2
NIP=.FALSE.                        TR2
INT=0                             TR2
INUSE=INUSE+1                      TR2
FLAG=.FALSE.                        TR2
FLAG2=.FALSE.                       TR2
CALL  CROSS(A1,B1,XI)              TR2
CALL  CROSS(XI,B1,KP)              TR2
MA1B1=MAG(XI)                      TR2
MB1=MAG(B1)                        TR2
A1MAG=MAG(A1)                      TR2
C   EQN(2)                         TR2
DO 100 J=1,3                      TR2
L(1,J)=XI(J)/MA1B1                TR2
L(2,J)=B1(J)/MB1                  TR2
100  L(3,J)=KP(J)/(MA1B1*MB1)      TR2
Y5P=0.00                           TR2
Z5P=0.00                           TR2
C   EQN(9)                          TR2
P1P(1)=0.00                        TR2
DO 110 I=2,3                      TR2
110  P1P(I)=L(I,1)*A1(1)+L(I,2)*A1(2)+L(I,3)*A1(3)  TR2
YC1P=DSQRT(B**2-P1P(3)**2)        TR2
C   EQN(12)                         TR2
DO 120 J=1,3                      TR2
120  PC1(J)=L(2,J)*YC1P+L(3,J)*P1P(3)      TR2
C   EQN(14,15)                      TR2
NLC1=DASIN(PC1(3)/B)              TR2
HLC1=WLON(PC1(2),PC1(1))          TR2
C   EQN(17)                          TR2
BETAC1=DASIN(DOT(PC1,B1)/(MB1*B)) TR2
BCBC1=B*DCOS(BETAC1)              TR2
125  CALL  RIIP(R0,NLC1,HLC1,PLASD)      TR2
IF(SEARCH.AND.ASC.AND.RTARG.GT.BCBC1.AND.RTARG.LE.R0+HBE)GOTO 591 TR2
NIP=.TRUE.                          TR2
NOELAY=.FALSE.                      TR2
IF(FCE.GT.0.00)GO TO 126          TR2
FCE=1.0-2                          TR2
NOELAY=.TRUE.                      TR2
126  RM=R0+HBE+HAE                  TR2
H=HAE                             TR2
F=FREQ/FCE                         TR2
Y3P=DSQRT(RM**2-P1P(3)**2)        TR2
Y8EP=DSQRT((R0+HBE)**2-P1P(3)**2) TR2
DO 1265 J=1,3                      TR2
1265 PC1(J)=L(2,J)*Y3P+L(3,J)*P1P(3)      TR2
NLC1= DASIN(PC1(3)/RM)             TR2

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        WLC1=WLC1(PC1(2),PC1(1))
        CALL RIIP(R0,WLC1,WLC1,PLASD)          TR2
        RM=HBE+HAE+R0                          TR2
127    H=HAE                                TR2
        NOELAY=.FALSE.                         TR2
        IF(FCE.GT.0.00) GO TO 129              TR2
        FCE=1.0-2                            TR2
        NOELAY=.TRUE.                          TR2
129    F=FREQ0/FCE                          TR2
130    IF(.NOT.FLAG) GO TO 1305             TR2
        CBET1=DA8S(Z10PP)/RM                TR2
        SBET1=DSQRT(1.00-CBET1**2)          TR2
        Y3P=RM*SBET1                         TR2
        YBEP=(R0+HBE)*SBET1                 TR2
        GO TO 131                           TR2
1305   Y3P=DSQRT(RM**2-P1P(3)**2)        TR2
        YBEP=DSQRT((R0+HBE)**2-P1P(3)**2)  TR2
C     EQN(10)
        CBET1=BCBC1/RM                      TR2
        SBET1=DSQRT(1.00-CBET1*CBET1)       TR2
131    IF(F*SBET1.GT.1.00) GO TO 135      TR2
        IF(FLAG) GO TO 134                  TR2
132    IF(FLAG2) GO TO 134                  TR2
1325   IREFL=1                            TR2
        RM=R0+HBE+HAE                      TR2
        MR3=A1MAG                           TR2
        SIN02=DOT(A1,B1)/(MB1*A1MAG)       TR2
        COS02=DSQRT(1.00-SIN02**2)          TR2
        Y9P=P1P(2)                          TR2
        Z9P=P1P(3)                          TR2
        C22P=L(2,1)*B1(1)+L(2,2)*B1(2)+L(2,3)*B1(3)  TR2
        C23P=L(3,1)*B1(1)+L(3,2)*B1(2)+L(3,3)*B1(3)  TR2
        Y10P=COS02*(Y9P*COS02+Z9P*SIN02)      TR2
        Z10P=COS02*(Z9P*COS02-Y9P*SIN02)      TR2
        GO TO 3096                           TR2
134    FLAG=.FALSE.                         TR2
        ISTOP=11                            TR2
        GO TO 7310                           TR2
135    IF(.NOT.NOELAY) GO TO 137          TR2
        Y4P=Y3P                            TR2
        DGP1=0.00                           TR2
        Z4P=P1P(3)                          TR2
        GO TO 139                           TR2
137    DGP1=-H/SBET1+H*F/2.00* ALOG((F*SBET1+1.00)/(F*SBET1-1.00))  TR2
        GAM1=CBET1*DGP1/RM                TR2
        Y4P=Y3P*DCOS(GAM1)-P1P(3)*DSIN(GAM1)  TR2
        Z4P=P1P(3)*DCOS(GAM1)+Y3P*DSIN(GAM1)  TR2
C     DIST BETWEEN SUCCESSIVE R<S
139    DISTB=DSQRT((Y4P-Y5P)**2+(Z4P-Z5P)**2)  TR2
        IF(FLAG) GO TO 141                  TR2
        DO 140 J=1,3                      TR2
140    P4(J)=L(2,J)*Y4P+L(3,J)*Z4P      TR2
        GO TO 1418                         TR2
141    DO 1413 J=1,3                      TR2
1413   P4(J)=M(2,J)*Y4P+M(3,J)*Z4P+P0(J)  TR2
1418   IF(DISTB.LE.EPS1) GO TO 200        TR2
        IF(INT.LE.1.OR.DISTB.LT.DISTA) GO TO 145  TR2

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        OUT2=DISTA                                TR2
        IF(IWRITE.EQ.1) WRITE(6,142) OUT2,IHOPS      TR2
142      FORMAT(24H E-LAYER CONV. PROBLEMS,,F6.1,17H KM USED, HOP NO.,I3) TR2
        H=HP                                      TR2
        Y3P=Y3PP                                    TR2
        RM=RMP                                      TR2
        DGP1=GPP                                    TR2
        F=FP                                       TR2
        GO TO 215                                  TR2
145      NL4=DASIN(P4(3)/MAG(P4))                TR2
        WL4=WLON(P4(2),P4(1))                      TR2
        DISTA=DISTB                                TR2
        GPP=DGP1                                    TR2
        Y5P=Y4P                                      TR2
        Z5P=Z4P                                      TR2
        HP=H                                       TR2
        FP=F                                       TR2
        Y3PP=Y3P                                    TR2
        RMP=RM                                      TR2
        SIN01=SBET1                                TR2
        COS01=CBET1                                TR2
        DO 148 J=1,3                                TR2
148      R2(J)=P4(J)                                TR2
        CALL RIIP(R0,NL4,WL4,PLASD)                TR2
        NOELAY=.FALSE.                            TR2
        IF(FCE.GT.0.00) GO TO 149                  TR2
        FCE=1.0-2                                  TR2
        NOELAY=.TRUE.                            TR2
149      RM=HBE+HAE+R0                            TR2
        H=HAE                                      TR2
        F=FRE0/FCE                                TR2
        INT=INT+1                                  TR2
        IF(INT.LE.LIMEA) GO TO 130                  TR2
        ISTOP=12                                  TR2
        GO TO 7310                                 TR2
C      END OF E LAYER REFRACTION                TR2
C      START OF F1 LAYER REFRACTION              TR2
200      Y5P=Y4P                                  TR2
        Z5P=Z4P                                      TR2
        SIN01=SBET1                                TR2
        COS01=CBET1                                TR2
        DO 210 J=1,3                                TR2
210      R2(J)=P4(J)                                TR2
        MR2=RM                                      TR2
        RR1=HR2-H                                  TR2
        SIN01P=SIN01                                TR2
        COS01P=COS01                                TR2
        Y6P=COS01*(Y5P*COS01+Z5P*SIN01)          TR2
        Z6P=COS01*(Z5P*COS01-Y5P*SIN01)          TR2
        IF(.NOT.FLAG) GO TO 2155                  TR2
        DO 2151 J=1,3                                TR2
2151    P4(J)=M(2,J)*Y3P+M(3,J)*Z10PP        TR2
        RR1=-H/MAG(P4)                            TR2
        DO 2152 J=1,3                                TR2
2152    P4(J)=R2(J)+RR1*P4(J)                  TR2
        RR1=MAG(P4)                                TR2
        MR2=MAG(R2)                                TR2

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COS01P=BCBC1/MR2          TR2
SIN01P=DSQRT(1.00-COS01P**2) TR2
DO 2153 J=1,3             TR2
P4(J)=M(2,J)*Y6P+M(3,J)*Z6P+P0(J) TR2
2153 P8(J)=R2(J)-P4(J)     TR2
CALL CROSS(R2,P8,XI)      TR2
CALL CROSS(XI,P8,KP)      TR2
CNST=MAG(XI)              TR2
FLOG=MAG(P8)              TR2
DO 2154 J=1,3             TR2
L(1,J)=XI(J)/CNST        TR2
L(2,J)=P8(J)/FLOG        TR2
2154 L(3,J)=KP(J)/(CNST*FLOG) TR2
Y5P=L(2,1)*R2(1)+L(2,2)*R2(2)+L(2,3)*R2(3) TR2
Z5P=L(3,1)*R2(1)+L(3,2)*R2(2)+L(3,3)*R2(3) TR2
Y6P=L(2,1)*P4(1)+L(2,2)*P4(2)+L(2,3)*P4(3) TR2
Z6P=L(3,1)*P4(1)+L(3,2)*P4(2)+L(3,3)*P4(3) TR2
FLAG=.FALSE.                TR2
2155 INT=0                 TR2
FLAG3=.FALSE.              TR2
HEA=H                      TR2
HEZ=H                      TR2
PPEF1A=0.00                 TR2
IF(.NOT.NOELAY)PPEF1A=H*(.500*SIN01-1.00/SIN01+F/4.00*(1.00-F**(-2
*)+COS01**2)*DL0G((F*SIN01+1.00)/(F*SIN01-1.00))) TR2
DPP1A=PPEF1A                TR2
*P0=RR1*DSQRT(1.00-(COS01P*MR2/RR1)**2) TR2
1AU1EA=MR2*SIN01P-PP0       TR2
IF(.NOT.HITS.OR.COS01P*MR2/A1MAG.GE.1.00) GO TO 217 TR2
PP0=PP0-A1MAG*DSQRT(1.00-(COS01P*MR2/A1MAG)**2) TR2
217 C12P=Y5P-Y6P             TR2
C13P=Z5P-Z6P                TR2
MC1PSQ=C12P**2+C13P**2      TR2
MRX1SQ=BCBC1**2              TR2
218 RM=R0+HBE+HAE+HAF1       TR2
TC2=DSQRT((RM**2-MRX1SQ)/MC1PSQ) TR2
IF(SEARCH.AND.RTARG.GT.DSQRT(MRX1SQ).AND.RTARG.LE.RR1) GO TO 591 TR2
YC2P=C12P*TC2+Y6P            TR2
ZC2P=C13P*TC2+Z6P            TR2
DO 220 J=1,3                 TR2
220 PC2(J)=L(2,J)*YC2P+L(3,J)*ZC2P      TR2
NLC2= DASIN(PC2(3)/RM)        TR2
HLC2=WLON(PC2(2),PC2(1))     TR2
CALL PIIF(R0,NLC2,HLC2,PLASD) TR2
225 RM=R0+HBE+HAE+HAF1       TR2
H=HAF1                      TR2
F=FREQ/FCF1                 TR2
Y9P=0.00                     TR2
Z9P=0.00                     TR2
230 IF(.NOT.FLAG) GO TO 2305 TR2
CBET4= DABS(Z10PP)/RM        TR2
SBET4=DSQRT(1.00-CBET4**2)   TR2
Y7P=RM*SBET4                 TR2
GO TO 231                   TR2
2305 TDEL3=DSQRT((RM**2-MRX1SQ)/MC1PSQ) TR2
Y7P=C12P*TDEL3+Y6P           TR2
Z7P=C13P*TDEL3+Z6P           TR2

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MR3=RM          TR2
CBET4=BCBC1/MR3 TR2
SBET4=DSQRT(1.D0-CBET4*CBET4) TR2
231 IF(F*SBET4.GT.1.D0) GO TO 235 TR2
IF(FLAG) GO TO 234 TR2
232 IF(FLAG3) GO TO 234 TR2
2325 IREFL=2 TR2
RM=R0+HAE+HAE+HAF1 TR2
Y9P=Y5P TR2
Z9P=Z5P TR2
MR3=MR2 TR2
COS02=COS01 TR2
SIN02=SIN01 TR2
Y10P=COS02*(Y9P*COS02+Z9P*SIN02) TR2
Z10P=COS02*(Z9P*COS02-Y9P*SIN02) TR2
GO TO 3095 TR2
234 FLAG=.FALSE. TR2
ISTOP=13 TR2
GO TO 7310 TR2
235 DGP2=H*(F/2.00*DLOG((F*SBET4+1.D0)/(F*SBET4-1.D0))-1.D0/SBET4) TR2
GAM2=CBET4*DGP2/RM TR2
Y8P=Y7P*DCOS(GAM2)-Z7P*DSIN(GAM2) TR2
Z8P=Z7P*DCOS(GAM2)+Y7P*DSIN(GAM2) TR2
C DIST BETWEEN SUCCESSIVE R<s TR2
DISTB=DSQRT((Y8P-Y9P)**2+(Z8P-Z9P)**2) TR2
IF(FLAG) GO TO 241 TR2
DO 240 J=1,3 TR2
240 P8(J)=L(2,J)*Y8P+L(3,J)*Z8P TR2
GO TO 2425 TR2
241 DO 242 J=1,3 TR2
242 P8(J)=M(2,J)*Y8P+M(3,J)*Z8P+P0(J) TR2
2425 IF(DISTB.LE.EPS2) GO TO 300 TR2
IF(INT.LE.1.OR.DISTB.LT.DISTA)GO TO 245 TR2
OUT2=DISTA TR2
IF(IWRITE.EQ.1) WRITE(6,243) OUT2,IHOPS TR2
243 FORMAT(25H F1-LAYER CONV. PROBLEMS,,F6.1,17H KM USED, HOP NO.,I3) TR2
H=HP TR2
F=FP TR2
Y7P=Y7PP TR2
RM=RMP TR2
DGP2=GPP TR2
GO TO 307 TR2
245 NL8=DASIN(P8(3)/MAG(P8)) TR2
WL8=WLON(P8(2),P8(1)) TR2
Y9P=Y8P TR2
Z9P=Z8P TR2
HP=H TR2
FP=F TR2
Y7PP=Y7P TR2
RMP=RM TR2
GPP=DGP2 TR2
COS02=CBET4 TR2
SIN02=SIN01 TR2
DO 247 J=1,3 TR2
247 R3(J)=P8(J) TR2
DISTA=DISTB TR2
CALL RIIP(R0,NL8,WL8,PLASD) TR2

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RM=R0+H8E+HAE+HAF1          TR2
H=HAF1                      TR2
F=FREQ/FCF1                  TR2
INT=INT+1                     TR2
IF(INT.LE.LIMF1A) GO TO 230  TR2
ISTOP=14                      TR2
GO TO 7310                     TR2
C   END OF F1 LAYER REFRACTION
300  Y9P=Y8P                  TR2
Z9P=Z8P                      TR2
SIN02=SBET4                  TR2
COS02=CBET4                  TR2
DO 305 J=1,3                  TR2
305  R3(J)=P8(J)              TR2
307  MR3=RM                  TR2
IREFL=3                      TR2
RM=R0+HMF2                  TR2
RR2=MR3-H                     TR2
Y10P=COS02*(Y9P*COS02+Z9P*SIN02)  TR2
Z10P=COS02*(Z9P*COS02-Y9P*SIN02)  TR2
COS02P=COS02                 TR2
SIN02P=SIN02                 TR2
IF(.NOT.FLAG) GO TO 3075      TR2
DO 3071 J=1,3                  TR2
3071 P8(J)=M(2,J)*Y7P+M(3,J)*Z10P+P0(J)  TR2
RR2=-H/MAG(P8)                TR2
DO 3072 J=1,3                  TR2
3072 P8(J)=R3(J)+RR2*P8(J)    TR2
RR2=MAG(P8)                  TR2
MR3=MAG(R3)                  TR2
COS02P=BCRC1/MR3              TR2
SIN02P=DSQRT(1.00-COS02P**2)  TR2
DO 3073 J=1,3                  TR2
3073 P8(J)=M(2,J)*Y10P+M(3,J)*Z10P+P0(J)  TR2
P4(J)=R3(J)-P8(J)              TR2
CALL CROSS(R3,P4,XI)          TR2
CALL CROSS(XI,P4,KP)          TR2
CNST=MAG(XI)                  TR2
FLOG=MAG(P4)                  TR2
DO 3074 J=1,3                  TR2
L(1,J)=XI(J)/CNST             TR2
L(2,J)=P4(J)/FLOG             TR2
3074 L(3,J)=KP(J)/(CNST*FLOG)  TR2
Y9P=L(2,1)*R3(1)+L(2,2)*R3(2)+L(2,3)*R3(3)  TR2
Z9P=L(3,1)*R3(1)+L(3,2)*R3(2)+L(3,3)*R3(3)  TR2
Y10P=L(2,1)*P8(1)+L(2,2)*P8(2)+L(2,3)*P8(3)  TR2
Z10P=L(3,1)*P8(1)+L(3,2)*P8(2)+L(3,3)*P8(3)  TR2
FLAG=.FALSE.                   TR2
3075 DO 308 J=1,3              TR2
308  PREV(J)=0.D0               TR2
IF(.NOT.SEARCH) GO TO 309      TR2
IF(RTARG.GT.RR1.AND.RTARG.LE.MR2) GO TO 593  TR2
IF(IREFL.EQ.1) GO TO 309      TR2
IF(MR2.LE.RR2.AND.RTARG.LE.RR2.AND.RTARG.GT.MR2) GO TO 593  TR2
IF(RR1.GT.MR3.AND.RTARG.LE.RR1.AND.RTARG.GT.MR3) GO TO 593  TR2
C   TILTED F2 LAYER
309  HF1A=H                      TR2

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HF1=H
TAU=MR3*SINO2P-RR2*DSQRT(1.00-(MR3/RR2*COS02P)**2)+TAU1EA TR2
PPEF1A=PPEF1A+H*(.500*SINO2+F/4.00*(1.00-F**(-2)+COS02**2)*DLOG((F TR2
**SINO2+1.00)/(F*SINO2-1.00))-1.00/SINO2)+TAU TR2
GPEF1A=DGP1+DGP2+TAU TR2
3095 C22P=Y9P-Y10P TR2
C23P=Z9P-Z10P TR2
3096 TC3=(RM**2-Y10P**2-Z10P**2)/(C22P**2+C23P**2) TR2
IF(TC3.LT.0.00) GO TO (134,134,234),IREFL TR2
TC3=DSQRT(TC3) TR2
YC3P=C22P*TC3+Y10P TR2
ZC3P=C23P*TC3+Z10P TR2
DO 310 J=1,3 TR2
PC3(J)=L(2,J)*YC3P+L(3,J)*ZC3P TR2
P10(J)=L(2,J)*Y10P+L(3,J)*Z10P TR2
310 C2(J)=L(2,J)*C22P+L(3,J)*C23P TR2
BETA22=0.00 TR2
NLC3=DASIN(PC3(3)/RM) TR2
WLC3=WLON(PC3(2),PC3(1)) TR2
NOFLAG=0 TR2
CALL HTGRDF(NDFLAG,FREQ,RTD*NLC3,RTD*WLC3,RTD*DACOS(BCB1/RM),0, TR2
*00,RM,RM1,RT1,RTM1,DNDR,DNDNL,DNDWL,PNTFLG) TR2
NOFLAG=1 TR2
GO TO (311,312,313),IREFL TR2
311 F1=FREQ/FCE TR2
H1=HAF1 TR2
IF(NUSE.EQ.1) GO TO 314 TR2
FLAG2=.TRUE. TR2
INT=0 TR2
GO TO 127 TR2
312 F1=FREQ/FCF1*.866025403784439D0 TR2
RM1=RM1+HAF1 TR2
H1=HAF1*2.00 TR2
GO TO (3123,314,3125),NUSE TR2
3123 IF(FLAG2) GO TO 134 TR2
FLAG2=.TRUE. TR2
GO TO 1325 TR2
3125 FLAG3=.TRUE. TR2
INT=0 TR2
GO TO 225 TR2
313 F1=FREQ/FCF2 TR2
H1=HAF2 TR2
IF(NUSE.EQ.3) GO TO 314 TR2
IF(FLAG3) GO TO 234 TR2
FLAG3=.TRUE. TR2
GO TO 2325 TR2
314 INTF2=0 TR2
IRCYCL=0 TR2
315 COPHC3=PC3(3)/RM TR2
SIPHC3=DSQRT(1.00-COPHC3**2) TR2
NNUSE(INUSE)=NUSE TR2
FCREF(INUSE)=FREQ/F1 TR2
C CORRECTION IN F1 CRITICAL PRINT OUT TR2
IF(NUSE.EQ.2) FCREF(INUSE)=FCF1 TR2
COTHC3=PC3(1)/DSQRT(PC3(1)**2+PC3(2)**2) TR2
SITHC3=PC3(2)/DSQRT(PC3(1)**2+PC3(2)**2) TR2
PR1(1)=RTM1*COTHC3*SIPHC3 TR2

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        PR1(2)=RTM1*SITHC3*SIPHC3          TR2
        PR1(3)=RTM1*COPHC3                TR2
        N1(1)=COTHC3*SIPHC3*DNDR-COTHC3*COPHC3*DNDNL/RTM1+SITHC3*DNDNL/(RT TR2
        *M1*SIPHC3)                      TR2
        N1(2)=SITHC3*SIPHC3*DNDR-SITHC3*COPHC3*DNDNL/RTM1-COTHC3*DNDNL/(RT TR2
        *M1*SIPHC3)                      TR2
        N1(3)=COPHC3*DNDR+SIPHC3*DNDNL/RTM1          TR2
        MN1=MAG(N1)                      TR2
        T0=-RTM1/MN1                      TR2
        ISTOP=1                           TR2
        DO 320 J=1,3                      TR2
        P0(J)=N1(J)*T0+PR1(J)            TR2
320      A2(J)=P10(J)-P0(J)            TR2
        CALL CROSS(A2,C2,XI)            TR2
        CALL CROSS(XI,C2,KP)            TR2
        MA2C2=MAG(XI)                  TR2
        MC2=MAG(C2)                    TR2
        DO 330 J=1,3                      TR2
        M(1,J)=XI(J)/MA2C2            TR2
        M(2,J)=C2(J)/MC2              TR2
330      M(3,J)=KP(J)/(MA2C2*MC2)      TR2
        Z10PP=M(3,1)*A2(1)+M(3,2)*A2(2)+M(3,3)*A2(3)      TR2
        RB=RM1-H1                      TR2
        IF(PB.GE. DABS(Z10PP)) GO TO 332      TR2
        ISTOP=2                           TR2
        GO TO 3345                      TR2
332      COBETB= DABS(Z10PP)/RB          TR2
        SIBETB=DSQRT(1.00-COBETB**2)      TR2
        YS1PP=RB*SIBETB                TR2
        DO 333 J=1,3                      TR2
333      S1(J)=M(2,J)*YS1PP+M(3,J)*Z10PP+P0(J)      TR2
        R4=MAG(S1)                      TR2
        PP2=1.00-(MR3/R4*COS02)**2      TR2
        IF(PP2.GE.0.00) GO TO 3331      TR2
        ISTOP=2                           TR2
        GO TO 3345                      TR2
3331    PP2=R4*DSQRT(PP2)-MR3*SIN02      TR2
        PP2A=PP2                         TR2
        IF(IREFL.GT.1) GO TO 3336      TR2
        IF(HITS) GO TO 3334            TR2
        PP0=R4*DSQRT(1.00-(MR3/R4*COS02)**2)      TR2
        GO TO 3336                      TR2
3334    PP0=PP2                         TR2
3336    CBTM1=RB*COBETB/RTM1          TR2
        IF(CBTM1.LE.1.00) GO TO 334      TR2
        ISTOP=3                           TR2
        GO TO 3345                      TR2
334      SBTTM1=DSQRT(1.00-CBTM1**2)      TR2
        FLAG=.FALSE.                    TR2
        IF(1.00-F1*SBTTM1.GT.0.00) GO TO 335      TR2
        FLAG=.TRUE.                     TR2
3345    THETA=1.00/RTM1                TR2
        DIST1=1.010                      TR2
        IRCYCL=0                         TR2
        GO TO 336                      TR2
335      FLOG=H1*F1*DLOG((1.00+F1*SBTTM1)/(1.00-F1*SBTTM1))/2.00      TR2
        GPF2=FLOG*2.00                  TR2

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THETA=CBTTM1*FLOG/RTM1
PPF2=H1*SBTTM1+(1.00-F1**(-2)+CBTTM1**2)*FLOG
IRCYCL=IRCYCL+1
336 YS2PP=YS1PP*DCOS(THETA)-Z10PP*DSIN(THETA)
ZS2PP=Z10PP*DCOS(THETA)+YS1PP*DSIN(THETA)
IF(FLAG.OR.ISTOP.GT.1) GO TO 475
YS3PP=YS1PP*DCOS(2.00*THETA)-Z10PP*DSIN(2.00*THETA)
ZS3PP=Z10PP*DCOS(2.00*THETA)+YS1PP*DSIN(2.00*THETA)
ALPHAV=PI/2.00-THETA-DASIN(SIBETB)
RV=RB*COBETB/OSIN(ALPHAV)
YVPP=YS2PP*RV/RB
C32PP=YS3PP-YVPP
C33PP=ZS3PP-Z10PP
DO 340 J=1,3
C3(J)=M(2,J)*C32PP+M(3,J)*C33PP
340 A3(J)=M(2,J)*YS3PP+M(3,J)*ZS3PP+P0(J)
CALL CROSS(A3,C3,PHI)
CALL CROSS(PHI,C3,KPPP)
MA3C3=MAG(PHI)
MC3=MAG(C3)
C32PPP=MC3
DO 350 J=1,3
P(1,J)=PHI(J)/MA3C3
P(2,J)=C3(J)/MC3
P(3,J)=KPPP(J)/(MA3C3*MC3)
350 C F1 LAYER DOWNWARD
YS3PPP=P(2,1)*A3(1)+P(2,2)*A3(2)+P(2,3)*A3(3)
IF(YS3PPP.GE.0.00) GO TO 3555
ZS3PPP=P(3,1)*A3(1)+P(3,2)*A3(2)+P(3,3)*A3(3)
INT=0
GO TO (436,3987,353),IREFL
353 IF(MR3.GE.DABS(ZS3PPP)) GO TO 360
IF(B.GE. DABS(ZS3PPP)) GO TO 356
3555 ISTOP=3
IRCYCL=0
GO TO 475
356 YDPPP=-DSQRT(B**2-ZS3PPP**2)
GO TO 370
360 YDPPP=-DSQRT(MR3**2-ZS3PPP**2)
C F1 LAYER ITERATION 370 TO 390
370 DO 380 J=1,3
380 PD(J)=P(2,J)*YDPPP+P(3,J)*ZS3PPP
NLD=DASIN(PD(3)/MAG(PD))
WLD=WLON(PD(2),PD(1))
CALL RIIP(R0,NLD,WLD,PLASD)
RM=HBE+HAE+HAF1+R0
H=HAF1
F=FREQ/FCF1
IF(RM.GE.DABS(ZS3PPP)) GO TO 382
ISTOP=3
IRCYCL=0
GO TO 475
382 YDPPP2=-DSQRT(RM**2-ZS3PPP**2)
DISTB=DABS(YDPPP2-YDPPP)
IF(DISTB.LE.EPS3) GO TO 390
IF(INT.LE.1.OR.DISTB.LT.DISTA) GO TO 384
H=HP

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F=FP          TR2
RM=RMP        TR2
YDPPP2=YDPPP TR2
OUT2=DISTA   TR2
IF(IHRITE.EQ.1) WRITE(6,243) OUT2,IHOPS  TR2
GO TO 390    TR2
384  YDPPP=YDPPP2 TR2
DISTA=DISTB  TR2
RMP=RM       TR2
FP=F         TR2
HP=H         TR2
INT=INT+1    TR2
IF(INT.LE.LIMF1D) GO TO 370  TR2
ISTOP=4      TR2
IRCYCL=0    TR2
GO TO 475    TR2
C   E LAYER DOWNWARD TR2
390  YM1PPP=YDPPP2 TR2
HF1=H         TR2
MRM1=DSQRT(YM1PPP**2+ZS3PPP**2) TR2
DO 395 J=1,3 TR2
395  RN1(J)=P(2,J)*YM1PPP+P(3,J)*ZS3PPP TR2
SBETM1=DABS(DOT(RN1,C3)/(MRM1*MC3)) TR2
CBETM1=DSQRT(1.00-SBETM1*SBETM1) TR2
R4=MAG(A3)   TR2
PP2=PP2+R4*DSQRT(1.00-(MRM1/R4*CBETM1)**2)-MRM1*SBETM1 TR2
IF(F*SBETM1.GT.1.00)GO TO 398  TR2
ISTOP=5      TR2
IRCYCL=0    TR2
GO TO 475    TR2
398  FLOG=DL0G((F*SBETM1+1.00)/(F*SBETM1-1.00)) TR2
DGP2P=H*(F/2.00*FLOG-1.00/SBETM1) TR2
TH12=CBETM1*DGP2P/RM   TR2
PPEF1D=H*(.500*SBETM1+F/4.00*(1.00-F**(-2)+CBETM1**2)*FLOG-1.00/SBETM1) TR2
OPP2P=PPEF1D TR2
RR2=MRM1*SBETM1   TR2
RR2C=MRM1*CBETM1   TR2
YM2PPP=YM1PPP*DCOS(TH12)-ZS3PPP*DSIN(TH12) TR2
ZM2PPP=ZS3PPP*DCOS(TH12)+YM1PPP*DSIN(TH12) TR2
MRM2=DSQRT(YM2PPP**2+ZM2PPP**2) TR2
YY1PPP=CBETM1*(YM2PPP*CBETM1-ZM2PPP*SBETM1) TR2
ZM2PPP=CBETM1*(ZM2PPP*CBETM1+YM2PPP*SBETM1) TR2
C42PPP=YY1PPP-YM2PPP   TR2
C43PPP=ZM2PPP   TR2
MRY1SQ=YY1PPP**2+ZM2PPP**2   TR2
MC4SQ=C42PPP**2+C43PPP**2   TR2
3984  IF(MR2**2.GE.MRY1SQ)GO TO 399  TR2
IF(B**2.GE.MRY1SQ) GO TO 3986  TR2
ISTOP=6      TR2
IRCYCL=0    TR2
GO TO 475    TR2
3986  TE=-DSQRT((B**2-MRY1SQ)/MC4SQ) TR2
RM=B         TR2
GO TO 3995   TR2
3987  CNST=-DOT(A3,C3)/MC3**2   TR2
C42PPP=P(2,1)*C3(1)+P(2,2)*C3(2)+P(2,3)*C3(3)   TR2

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C43PPP=P(3,1)*C3(1)+P(3,2)*C3(2)+P(3,3)*C3(3)          TR2
YY1PPP=YS3PPP+CNST*C42PPP                                TR2
ZY1PPP=ZS3PPP+CNST*C43PPP                                TR2
MRY1SQ=YY1PPP**2+ZY1PPP**2                                TR2
MC4SQ=MC3**2                                              TR2
MRM1=DSQRT(YS3PPP**2+ZS3PPP**2)                            TR2
CBETH1=DSQRT(MRY1SQ)/MRM1                                  TR2
SBETH1=DSQRT(1.00-CBETH1**2)                                TR2
GO TO 3984                                                 TR2
399  TE=-DSQRT((MR2**2-MRY1SQ)/MC4SQ)                      TR2
3995  YEPPIP=C42PPP*TE+YY1PPP                                TR2
      ZEPPIP=C43PPP*TE+ZY1PPP                                TR2
C   E LAYER ITERATION 400 TO 420                            TR2
      INT=0                                                 TR2
400  DO 410 J=1,3                                         TR2
410  PE(J)=P(2,J)*YEPPIP+P(3,J)*ZEPPIP                  TR2
      NLE=DASIN(PE(3)/MAG(PE))                            TR2
      WLE=WLON(PE(2),PE(1))                                TR2
      CALL RIIP(R0,NLE,WLE,PLASD)                          TR2
      NOELAY=.FALSE.                                       TR2
      IF(FCE.GT.0.00) GO TO 4105                          TR2
      FCE=1.0-2                                           TR2
      NOELAY=.TRUE.                                       TR2
4105  RM=HBE+HAE+R0                                         TR2
      H=HAE                                              TR2
      F=FREQ/FCE                                         TR2
      IF(RM**2.GE.MRY1SQ) GO TO 411                      TR2
      ISTOP=6                                            TR2
      IRCYCL=0                                           TR2
      GO TO 475                                           TR2
411  TE=-DSQRT((RM**2-MRY1SQ)/MC4SQ)                      TR2
      YEPPIP2=C42PPP*TE+YY1PPP                                TR2
      ZEPPIP2=C43PPP*TE+ZY1PPP                                TR2
      DISTB=DSQRT((YEPPIP-YEPPIP2)**2+(ZEPPIP-ZEPPIP2)**2) TR2
      IF(DISTB.LE.EPS4) GO TO 420                          TR2
      IF(INT.LE.1.0R.DISTB.LT.DISTA) GO TO 414            TR2
      H=HP                                              TR2
      F=FP                                              T92
      RM=RMP                                           TR2
      YEPPIP2=YEPPIP                                TR2
      ZEPPIP2=ZEPPIP                                TR2
      OUT2=DISTA                                         TR2
      IF(IWRITE.EQ.1) WRITE(6,142) OUT2,1HOPS            TR2
      GO TO 420                                           TR2
414  YEPPIP=YEPPIP2                                         TR2
      ZEPPIP=ZEPPIP2                                     TR2
      RMP=RM                                           TR2
      FP=F                                              TR2
      HP=H                                              TR2
      DISTA=DISTB                                         TR2
      INT=INT+1                                         TR2
      IF(INT.LE.LIMED) GO TO 400                        TR2
      ISTOP=7                                           TR2
      IRCYCL=0                                           TR2
      GO TO 475                                           TR2
420  YM3PPP=YEPPIP2                                         TR2
      ZM3PPP=ZEPPIP2                                     TR2

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        HE=H                         TR2
C   END OF E LAYER               TR2
      MRM3=DSQRT(YM3PPP**2+ZM3PPP**2) TR2
      CBETM2=MRM1*CBETM1/MRM3          TR2
      SBETM2=DSQRT(1.00-CBETM2*CBETM2) TR2
      IF(IREFL.EQ.2) PP2=PP2+MRM1*SBETM1-MRM3*SBETM2 TR2
      IF(F*SBETM2.GT.1.00) GO TO 430 TR2
      ISTOP=8                         TR2
      IRCYCL=0                         TR2
      GO TO 475                         TR2
430   IF(.NOT.NOELAY) GO TO 4302   TR2
      FLOG=0.00                         TR2
      DPP1P=0.00                         TR2
      TH34=0.00                         TR2
      DGP1P=0.00                         TR2
      YM4PPP=YM3PPP                      TR2
      ZM4PPP=ZM3PPP                      TR2
      MRM4=MRM3                         TR2
      GO TO 4304                         TR2
4302  FLOG=DLOG((F*SBETM2+1.00)/(F*SBETM2-1.00)) TR2
      DGP1P=H*(F/2.00*FLOG-1.00/SBETM2) TR2
      TH34=CBETM2*DGP1P/RM              TR2
      YM4PPP=YM3PPP*DCOS(TH34)-ZM3PPP*DSIN(TH34) TR2
      ZM4PPP=ZM3PPP*DCOS(TH34)+YM3PPP*DSIN(TH34) TR2
      MRM4=DSQRT(YM4PPP**2+ZM4PPP**2) TR2
      DPP1P=H* (.500*SBETM2+F/4.00*(1.00-F**(-2)+CBETM2**2)*FLOG-1.00/SBETM2) TR2
      *TM2)                         TR2
4304  RR1=MRM4-H                     TR2
      IF(IREFL.LT.3) GO TO 4305         TR2
      IF(DABS(RR2C).GT.RR1) GO TO 431  TR2
      TAU=RR2-RR1*DSQRT(1.00-(RR2C/RR1)**2) TR2
      PPEF1D=PPEF1D+DPP1P+TAU           TR2
      GPEF1D=DGP1P+DGP2P+TAU           TR2
4305  YY2PPP=CBETM2*(YM4PPP*CBETM2-ZM4PPP*SBETM2) TR2
      ZY2PPP=CBETM2*(ZM4PPP*CBETM2+YM4PPP*SBETM2) TR2
      C52PPP=YY2PPP-YM4PPP              TR2
      C53PPP=ZY2PPP-ZM4PPP              TR2
      MC5SQ=C52PPP**2+C53PPP**2        TR2
      SBM4H2=1.00-(CBETM2/(1.00-HE/MRM4))**2 TR2
      IF(SBM4H2.GT.0.00) GO TO 4307   TR2
      ISTOP=15                         TR2
      IRCYCL=0                         TR2
      GO TO 475                         TR2
4307  TAU1ED=MRM4*SBETM2-(MRM4-HE)*DSQRT(SBM4H2) TR2
      RY=DSQRT(MRY1SQ)                 TR2
      GO TO 437                         TR2
431   ISTOP=9                         TR2
      IRCYCL=0                         TR2
      GO TO 475                         TR2
436   MB1=MAG(A3)                     TR2
      SBET1=-DOT(A3,C3)/(MB1*MC3)       TR2
      CBET1=DSQRT(1.00-SBET1**2)         TR2
      RY=MB1*CBET1                      TR2
      MRY1SQ=RY**2                      TR2
      CNST=MB1/MC3*SBET1                TR2
      C52PPP=P(2,1)*C3(1)+P(2,2)*C3(2)+P(2,3)*C3(3) TR2
      C53PPP=P(3,1)*C3(1)+P(3,2)*C3(2)+P(3,3)*C3(3) TR2

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      YY2PPP=YS3PPP+CNST*C52PPP          TR
      ZY2PPP=ZS3PPP+CNST*C53PPP          TR
      MC5SQ=MC3**2                         TR
437   HITS=R0.GT.RY                      TR
      INCHOP=(R0+50.00).GE.RY             TR
      IF(R0+HBE.GT.RY) GO TO 438         TR
      ISTOP=15                            TR
      IRCYCL=0                            TR
      GO TO 475                           TR
438   TQ=-DSQRT(((R0+HBE)**2-MRY1SQ)/MC5SQ) TR
      YBEPBP=C52PPP*T0+YY2PPP            TR
      ZBEPBP=C53PPP*T0+ZY2PPP            TR
      IF(.NOT.HITS) GO TO 450             TR
      TQ=-DSQRT((R0**2-MRY1SQ)/MC5SQ)   TR
      YQPPP=C52PPP*T0+YY2PPP            TR
      ZQPPP=C53PPP*TQ+ZY2PPP            TR
      DO 440 J=1,3                      TR2
      PQ(J)=P(2,J)*YQPPP+P(3,J)*ZQPPP  TR2
      GO TO 461                           TR2
440   DO 460 J=1,3                      TR2
      PQ(J)=P(2,J)*YY2PPP+P(3,J)*ZY2PPP TR2
C     STARTS TO ITERATE TILTED F2      TR2
461   DIST2=DSQRT((PQ(1)-PREV(1))**2+(PQ(2)-PREV(2))**2+(PQ(3)-PREV
      *(3))**2)                         TR2
      RTDIF=DABS(RT1-PREV(13))          TR2
      IF(IRCYCL.LE.2) GO TO 475          TR2
      IF(DIST2-EPS5) 463,463,462        TR2
462   IF(DIST1-DIST2) 470,475,475      TR2
463   IF(RTDIF-EPS5) 500,500,475        TR2
470   CALL PRVGET                      TR2
      ICNPRB=1                           TR2
      IF(IWRITE.EQ.1) WRITE(6,473) IHOPS,EPS5,DIST1,RTDIF      TR2
473   FORMAT(48H TILTED LAYER CONVERGENCE PROBLEMS ON HOP NUMBER,I3,
      1 1H,,F6.1,29H KM. CRITERIA NOT MET, DIST1=,F8.2,8H, RTDIF=,
      2 F8.2)                           TR2
      GO TO 500                           TR2
475   YH2PP=RTM1*YS2PP/RB               TR2
      ZH2PP=RTM1*ZS2PP/RB               TR2
      DO 480 J=1,3                      TR2
480   PW2(J)=M(2,J)*YH2PP+M(3,J)*ZH2PP+P0(J)             TR2
      NLH2=DASIN(PW2(3)/MAG(PH2))       TR2
      WLH2=WLON(PW2(2),PW2(1))         TR2
      DO 490 J=1,3                      TR2
490   H2(J)=PW2(J)-P0(J)              TR2
      BETA22=0ACOS(DOT(PH2,H2)/(MAG(H2)*MAG(PH2)))        TR2
      BETTM1=DASIN(SBTTM1)              TR2
      CALL PRVST0                      TR2
      DIST1=DIST2                      TR2
      BP=RTM1                           TR2
      CALL HTGRDF(NDFLAG,FREQ,RTD*NLH2,RTD*WLH2,RTD*BETTM1,RTD*BETA22,B
      *P,RM1,RT1,RTM1,DNDR,DNDNL,DNDWL,%NTFLG)           TR2
      IF(IREFL.NE.NUSE) GO TO 501        TR2
      GO TO (4916,4917,4918),IREFL      TR2
4916  F1=FREQ/FCE                    TR2
      H1=HAE                            TR2
      GO TO 4919                         TR2
4917  F1=FREQ/FCF1*.86602540378443900 TR2

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RM1=RM1+HAF1          TR2
H1=HAF1*2.00          TR2
GO TO 4919          TR2
4918 F1=FREQ/FCF2      TR2
H1=HAF2          TR2
4919 INTF2=INTF2+1      TR2
RM=MAG(PW2)          TR2
DO 492 J=1,3          TR2
492 PC3(J)=PH2(J)      TR2
IF(INTF2.LE.LIMF2) GO TO 315  TR2
IF(ISTOP.GT.1) GO TO 7310  TR2
494 IF(FLAG.OR.PNTFLG.GT.500) GO TO 501  TR2
GO TO 7310          TR2
C ITERATION FINISHED  TR2
500 DO 5003 J=1,3      TR2
VEC(J,1)=L(2,J)      TR2
LOC(J,1)=L(2,J)*YBEP+L(3,J)*P1P(3)  TR2
VEC(J,2)=L(2,J)*C12P+L(3,J)*C13P  TR2
LOC(J,2)=R2(J)      TR2
VEC(J,3)=M(2,J)      TR2
LOC(J,3)=L(2,J)*Y9P+L(3,J)*Z9P  TR2
VEC(J,4)=P(2,J)      TR2
LOC(J,4)=H(2,J)*YS1PP+H(3,J)*Z10PP+P0(J)  TR2
LOC(J,5)=A3(J)      TR2
LOC(J,6)=P(2,J)*YM1PPP+P(3,J)*ZS3PPP  TR2
"EC(J,5)=P(2,J)*C42PPP+P(3,J)*C43PPP  TR2
LOC(J,7)=P(2,J)*YM3PPP+P(3,J)*ZM3PPP  TR2
VEC(J,6)=P(2,J)*C52PPP+P(3,J)*C53PPP  TR2
5003 LOC(J,8)=P(2,J)*YBEP+P(3,J)*ZBEP    TR2
DO 5008 K=1,6      TR2
MAGVEC=MAG(VEC(1,K))  TR2
IF(MAGVEC.EQ.0.0D0) GO TO 5008  TR2
DO 5007 J=1,3      TR2
5007 VEC(J,K)=VFC(J,K)/MAGVEC  TR2
5008 CONTINUE      TR2
IF(PNTFLG.LT..5) GO TO 510  TR2
501 IF(FLAG2) GO TO 134  TR2
IF(FLAG3) GO TO 234  TR2
RM=RM1          TR2
INT=0          TR2
FLAG=.TRUE.      TR2
GO TO (502,503,504),IREFL  TR2
502 CBET1=COBETB*RB/RM  TR2
FLAG2=.TRUE.      TR2
SBET1=DSQRT(1.00-CBET1**2)  TR2
Y3P=DSQRT(RM**2-Z10PP**2)  TR2
P1P(3)=Z10PP  TR2
F=FREQ/FCF1      TR2
H=HAF1          TR2
MR3=RM          TR2
CBET4=COBETB*RB/RM  TR2
IF(DABS(CBET4).LT.1.00.AND.DABS(RM).GT.DABS(Z10PP)) GO TO 5035  TR2
ISTOP=6          TR2

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```

      IRCYCL=0          TR
      GO TO 475          TR
5035  SBET4=DSQRT(1.00-CBET4**2)          TR
      Y7P=DSQRT(RM**2-Z10PP**2)          TR
      Z7P=Z10PP          TR
      GO TO 231          TR
504   IF(IWRITE.EQ.1) WRITE(6,505)IHOPS      TR
505   FORMAT(23H PENETRATION ON HOP NO.,I3,1H.)  TR
      GO TO 7311         TR
510   IF(HITS) GO TO 530         TR
      GO TO (512,514,514),IREFL        TR
512   PP0P=MB1*SBET1          TR
      GO TO 516          TR
514   PP0P=(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)  TR
516   DO 520 J=1,3          TR
      B1(J)=P(2,J)*C52PPP+P(3,J)*C53PPP  TR
520   A1(J)=PQ(J)          TR
      GO TO 550          TR
530   GO TO (531,532,532),IREFL        TR
531   ALPHAQ=DASIN(MB1/R0*C BET1)        TR
      PP0P=MB1*SBET1-R0*DSQRT(1.00-(RY/R0)**2)  TR
      GO TO 533          TR
532   ALPHAQ=DASIN(MRM1*CBETM1/R0)        TR
      PP0P=(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)-R0*DSQRT(1.00-(MRM4/R0*C BETM2)**2)  TR
533   B22PPP=-C52PPP*DCOS(2.00*ALPHAQ)+C53PPP*DSIN(2.00*ALPHAQ)  TR
      B23PPP=-C53PPP*DCOS(2.00*ALPHAQ)-C52PPP*DSIN(2.00*ALPHAQ)  TR
      DO 540 J=1,3          TR
      A1(J)=P0(J)          TR
540   B1(J)=P(2,J)*B22PPP+P(3,J)*B23PPP  TR
550   IF(IHOPS.GE.IABS(MODE))GO TO 552      TR
551   GO TO (5511,5512,5513),IREFL        TR
5511  PPTOT=PPTOT+PP0+PPF2+PP0P          TR
      GPTOT=GPTOT+PP0+GPF2+PP0P          TR
      GO TO 5514          TR
5512  PPTOT=PPTOT+PP0+DPP1+PPF2+PP2+DPP1P+PP0P+TAU1EA+TAU1ED  TR
      GPTOT=GPTOT+PP0+DGP1+GPF2+PP2+DGP1P+PP0P+TAU1EA+TAU1ED  TR
      GO TO 5514          TR
5513  PPTOT=PPTOT+PP0+PPEF1A+PPF2+PP2+PPEF1D+PP0P          TR
      GPTOT=GPTOT+PP0+GPEF1A+GPF2+PP2+GPEF1D+PP0P          TR
5514  MB1=MAG(A1)          TR
      IF(.NOT.HITS.AND.IHOPS.GE.IABS(MODE).AND.MB1.GE.RTARG) GO TO 598  TR
      GO TO 90            TR
552   IF(SEARCH.AN0.RTARG.GT.MR3-HF1A.AND.RTARG.LE.DMAX1(RV,MR3))GOT0595  TR
      IF(ASC) GO TO 566          TR
      IF(DABS(RTARG-R0).LE.1.0-5.AND.HITS) GO TO 580          TR
      IF(MODE.GT.0) GO TO 563          TR
C     DESCENDING MODE          TR
      GO TO (564,562,560),IREFL        TR
560   IF(RTARG.LE.DMAX1(RV,MRM1).AND.RTARG.GT.MRM1-HF1) GO TO 576        TR
      IF(DMIN1(MRM4-HE,MRM1).LT.RTARG.AND.RTARG.LE.DMAX1(MRM4,MRM1-HF1))  TR
      * GO TO 573          TR
      IF(RTARG.LE.MRM4-HE) GO TO 568          TR
      IF(INCHOP) GO TO 566          TR
      SEARCH=.TRUE.          TR
      GO TO 5513          TR
562   IF(RTARG.LE.RV.AND.RTARG.GT.MRM4) GO TO 576          TR

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IF(RTARG.LE.MRM4) GO TO 568          TR2
IF(INCHOP) GO TO 566                TR2
SEARCH=.TRUE.                         TR2
GO TO 5512                           TR2
563  SEARCH=.TRUE.                   TR2
ASC=.TRUE.                           TR2
GO TO 551                           TR2
564  IF(RTARG.LE.RV) GO TO 568          TR2
SEARCH=.TRUE.                         TR2
IF(.NOT.INCHOP) GO TO 5511           TR2
566  ISTOP=15                         TR2
GO TO 7310                           TR2
568  IF(RTARG.GE.RY.OR.INCHOP) GO TO 569          TR2
SEARCH=.TRUE.                         TR2
GO TO 551                           TR2
569  TTARG=0.00                         TR2
IF(RTARG.GT.RY) TTARG=-DSQRT((RTARG**2-MRY1SQ)/MC5SQ) TR2
YTARGP=C52PPP*TTARG+YY2PPP           TR2
ZTARGP=C53PPP*TTARG+ZY2PPP           TR2
DO 570 J=1,3                          TR2
B1(J)=C52PPP*P(2,J)+C53PPP*P(3,J) TR2
570  PTARG(J)=P(2,J)*YTARGP+P(3,J)*ZTARGP          TR2
PP0P=0.00                            TR2
IF(RTARG.GT.RY) PP0P=-RTARG*DSQRT(1.00-(RY/RTARG)**2) TR2
GO TO (571,5715,5715),IREFL          TR2
571  PP0P=MB1*SBET1+PP0P               TR2
PPTOT=PPTOT+PP0+PPF2+PP0P           TR2
GPTOT=GPTOT+PP0+GPF1+GPF2+PP0P     TR2
GO TO 600                            TR2
5715 PP0P=(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)+PP0P TR2
GO TO (5720,5720,5725),IREFL          TR2
5720 PPTOT=PPTOT+PP0+DPP1+PPF2+PP2+DPP1P+PP0P+TAU1EA+TAU1EO TR2
GPTOT=GPTOT+PP0+DGP1+GPF2+PP2+DGP1P+PP0P+TAU1EA+TAU1EO TR2
GO TO 600                            TR2
5725 PPTOT=PPTOT+PP0+PPEF1A+PPF2+PP2+PPEF1D+PP0P           TR2
GPTOT=GPTOT+PP0+GPEF1A+GPF2+PP2+GPEF1D+PP0P           TR2
GO TO 600                            TR2
573  TTARG=-DSQRT((RTARG**2-MRY1SQ)/MC4SQ)          TR2
YTARGP=C42PPP*TTARG+YY1PPP           TR2
ZTARGP=C43PPP*TTARG+ZY1PPP           TR2
DO 575 J=1,3                          TR2
B1(J)=C42PPP*P(2,J)+C43PPP*P(3,J) TR2
575  PTARG(J)=P(2,J)*YTARGP+P(3,J)*ZTARGP          TR2
PPTOT=PPTOT+PPEF1A+PPF2+PP2+PP0+PPEF1D           TR2
GPTOT=GPTOT+GPEF1A+GPF2+PP2+PP0+GPEF1D           TR2
GO TO 600                            TR2
576  YTARGP=-DSQRT(RTARG**2-ZS3PPP**2)          TR2
ZTARGP=ZS3PPP                         TR2
DO 579 J=1,3                          TR2
B1(J)=C32PPP*P(2,J)                  TR2
579  PTARG(J)=P(2,J)*YTARGP+P(3,J)*ZTARGP          TR2
GO TO (5793,5793,5797),IREFL          TR2
5793 TAU=MRM4*SBETM2-(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)+P*P0+PP2 TR2
PPTOT=PPTOT+TAU+DPP1+PPF2+TAU1EA          TR2
GPTOT=GPTOT+TAU+DGP1+GPF2+TAU1EA          TR2
GO TO 600                            TR2

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5797 TAU=MRM1*SBEHM1-(MRM1-HF1)*DSQRT(1.00-(CBETM1/(1.00-HF1/MRM4))**2) TR
  *PP0+PP2 TR
  PPTOT=PPTOT+TAU+PPEF1A+PPF2+DPP2P TR
  GPTOT=GPTOT+TAU+GPEF1A+GPF2+DGP2P TR
  GO TO 600 TR
C   TARGET ON GROUND TR
580  DO 590 J=1,3 TR
  B1(J)=C52PPP*P(2,J)+C53PPP*P(3,J) TR
590  PTARG(J)=A1(J) TR
  GO TO(5902,5904,5906),IREFL TR
5902 PPTOT=PPTOT+PP0+PPF2+PP0P TR
  GPTOT=GPTOT+PP0+GPF2+PP0P TR
  GO TO 600 TR
5904 PPTOT=PPTOT+PP0+PPF1+PPF2+PP2+DPP1P+PP0P+TAU1EA+TAU1ED TR
  GPTOT=GPTOT+PP0+DGP1+GPF2+PP2+DGP1P+PP0P+TAU1EA+TAU1ED TR
  GO TO 600 TR
5906 PPTOT=PPTOT+PP0+PPEF1A+PP2+PPF2+PPEF1D+PP0P TR
  GPTOT=GPTOT+PP0+GPEF1A+PP2+GPF2+GPEF1D+PP0P TR
  GO TO 600 TR
C   ASCENDING MODE TR
591  YTARGP=DSQRT(RTARG**2-P1P(3)**2) TR
  DO 592 J=1,3 TR
592  PTARG(J)=L(2,J)*YTARGP+L(3,J)*P1P(3) TR
  TAU=RTARG*DSQRT(1.00-(RY/RTARG)**2) TR
  PPTOT=PPTOT+TAU TR
  GPTOT=GPTOT+TAU TR
  INUSE=INUSE-1 TR
  IF(.NOT.HITS) GO TO 600 TR
  TAU=-R0*DSQRT(1.00-(RY/R0)**2) TR
  PPTOT=PPTOT+TAU TR
  GPTOT=GPTOT+TAU TR
  GO TO 600 TR
593  TTARG=DSQRT((RTARG**2-MRX1SQ)/MC1PSQ) TR
  YTARGP=C12P*TTARG+Y6P TR
  ZTARGP=C13P*TTARG+Z6P TR
  DO 594 J=1,3 TR
  PTARG(J)=L(2,J)*YTARGP+L(3,J)*ZTARGP TR
  B1(J)=L(2,J)*C12P+L(3,J)*C13P TR
594  TAU=(MR3-HF1A)*DSQRT(1.00-(COS02/(1.00-HF1A/MR3))**2) TR
  PPTOT=PPTOT+DPP1+TAU TR
  GPTOT=GPTOT+DGP1+TAU TR
  INUSE=INUSE-1 TR
  IF(.NOT.HITS) GO TO 600 TR
  TAU=-R0*DSQRT(1.00-((MR2-HEA)/R0*COS01)**2) TR
  PPTOT=PPTOT+TAU TR
  GPTOT=GPTOT+TAU TR
  GO TO 600 TR
595  TTARG=DSQRT((RTARG**2-Y10P**2-Z10P**2)/(C22P**2+C23P**2)) TR
  YTARGP=C22P*TTARG+Y10P TR
  ZTARGP=C23P*TTARG+Z10P TR
  DO 596 J=1,3 TR
  PTARG(J)=L(2,J)*YTARGP+L(3,J)*ZTARGP TR
  B1(J)=L(2,J)*C12P+L(3,J)*C13P TR
  TAU=(MR2-HEA)*DSQRT(1.00-(COS01/(1.00-HEA/MR2))**2)+PP2A TR
  PPTOT=PPTOT+PPEF1A+PPF2/2.00+TAU TR
  GPTOT=GPTOT+GPEF1A+GPF2/2.00+TAU TR
  IF(.NOT.ASC) GO TO 600 TR

```

!ROUTINE TRISL 74/74 OPT=1 FTN 4.5+414 04/27/

 INUSE=INUSE-1 TR2
 TAU=-R0*DSQRT(1.00-((MR2-HEA)/R0*COS01)**2) TR2
 PPTOT=PPTOT+TAU TR2
 GPTOT=GPTOT+TAU TR2
 GO TO 600 TR2
 598 RS2=MAG(A1) TR2
 00 599 I=1,3 TR2
 599 PTARG(I)=A1(I) TR2
 GO TO 601 TR2
 600 IF(.NOT.HITS) RS2=MAG(PTARG) TR2
 601 IF(GPONLY) RETJRN TR2
 NL TARG=RTD*DASIN(PTARG(3)/RS2) TR2
 WLTARG=RTD*WLON(PTARG(2),PTARG(1)) TR2
 EAST(1)=-PTARG(2) TR2
 EAST(2)=PTARG(1) TR2
 EAST(3)=0.00 TR2
 CALL CROSS(PTARG,EAST,NORTH) TR2
 CNST1=DOT(PTARG,B1)/RS2 TR2
 ELF=RTD*DASIN(CNST1/MAG(B1)) TR2
 ME=MAG(EAST) TR2
 MN=MAG(NORTH) TR2
 CNST=DOT(EAST,B1)/ME TR2
 AZF=RTD*DATAN2(CNST, DOT(NORTH,B1)/MN)+180.00-DSIGN(180.00,CNST) TR2
 B1(1)=PTARG(1)-A11(1) TR2
 B1(2)=PTARG(2)-A11(2) TR2
 B1(3)=PTARG(3)-A11(3) TR2
 SRANGE=MAG(B1) TR2
 EL SR=RTD*DASIN(DOT(A11,B1)/(SRANGE*MA1)) TR2
 DIST=R0*DACOS(DOT(A11,PTARG)/(RS2*MA1)) TR2
 CNST=DOT(EAST1,B1) TR2
 BEAR=RTD*DATAN2(CNST, DOT(NORTH1,B1))+180.00-DSIGN(180.00,CNST) TR2
 RETURN TR2
 7310 IGOBAK=1 TR2
 IF(IWRITE.EQ.1) WRITE(6,7309) MESSPR(ISTOP) TR2
 7309 FORMAT(11H MESSUP---,A10) TR2
 RETURN TR2
 7311 IGOBAK=2 TR2
 RETURN TR2
 END TR2

UNCTION MAG 74/74 OPT=1 FTN 4.5+414 04/27/

```
DOUBLE PRECISTON FUNCTION MAG(A)
IMPLICIT DOUBLE PRECISION(A-Z)
DIMENSION A(3)
MAG=DSORT(A(1)*A(1)+A(2)*A(2)+A(3)*A(3))
RETURN
END
```

MAG
MAG
MAG
MAG
MAG
MAG

UNCTION DOT 74/74 OPT=1 FTN 4.5+414 04/27/

```
DOUBLE PRECISION FUNCTION DOT(A,B)
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
DIMENSION A(3),B(3)
DOT=A(1)*B(1)+A(2)*B(2)+A(3)*B(3)
RETURN
END
```

DOT
DOT
DOT
DOT
DOT
DOT

ROUTINE CROSS 74/74 OPT=1 FTN 4.5+414 04/27/

```
SUBROUTINE CROSS(A,B,C)
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
DIMENSION A(3),B(3),C(3)
C(1)=A(2)*B(3)-A(3)*B(2)
C(2)=A(3)*B(1)-A(1)*B(3)
C(3)=A(1)*B(2)-A(2)*B(1)
RETURN
END
```

VEC
VEC
VEC
VEC
VEC
VEC
VEC
VEC
VEC

ROUTINE PRVSTO 74/74 OPT=1

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```
      SUBROUTINE PRVSTO          PRV
      DOUBLE PRECISION P1,P2      PRV
      LOGICAL LP1,LP2            PRV
      COMMON/CPREV/P1(56),P2(56),LP1(6),LP2(6)  PRV
      DO 1 I=1,56                PRV
      1 P2(I)=P1(I)              PRV
      DO 2 I=1,6                 PRV
      2 LP2(I)=LP1(I)            PRV
      RETURN                      PRV
      ENTRY PRVGET               PRV
      DO 3 I=1,56                PRV
      3 P1(I)=P2(I)              PRV
      DO 4 I=1,6                 PRV
      4 LP1(I)=LP2(I)            PRV
      RETURN                      PRV
      END                         PRV
```

ROUTINE HTGRDF 74/74 OPT=1

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```
      SUBROUTINE HTGRDF (NOFLAG,FREQ,NLAT,HLONG,ANGLE1,ANGLE2,RANG12,RMU HTG
      *,RTU,RTMU,DNDR,DNOT,DNCP,PNTFLG)          HTG
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)          HTG
      DOUBLE PRECISION NLAT,NLATR                 HTG
      LOGICAL TILT,FAST                          HTG
      COMMON/TILT/TC/TILT,FAST                  HTG
      NLATR=NLAT/57.2957795130823200            HTG
      HLONGR=HLONG/57.2957795130823200          HTG
      CALL RIIP(6370.00,NLATR,HLONGR,EN)          HTG
      CALL RTFIND(NOFLAG,FREQ,ANGLE1,ANGLE2,RANG12,RTU,RTMU,RMU,PNTFLG) HTG
      IF(TILT) GO TO 1                           HTG
      DNDR=1.000                         HTG
      DNCP=0.000                          HTG
      DNDT=0.000                          HTG
      RETURN                      HTG
      1 CALL DENSE(RTU,NLAT,HLONG,EN,DNDR,DNDT,DNCP)  HTG
      RETURN                      HTG
      END                         HTG
```

```

      SUBROUTINE RTFIND(NDFLAG,FREQ,ANGLE1,ANGLE2,RANG12,RTU,RMU,RTMU,P RTF
      *NTFLG) RTF
C   NDFLAG FLAG TO INDICATE WHICH PASS RTF
C   =0 FIRST PASS RTF
C   =1 SUBSEQUENT PASSES RTF
C   NOTE - THIS ROUTINE REQUIRES INITIALIZATION . RTF
C           ON FIRST PASS, ANGLE1 MUST = THE INITIAL TAKE OFF ANGLE ON RTF
C           GROUND, ANGLE2 MUST =0, RANG12 MUST = RADIUS OF EARTH RTF
C   FREQ-OPERATING FREQUENCY IN MHZ. RTF
C   ANGLE1 - ANGLE (DEG) BETWEEN TILTED LAYER AND RAY INCIDENT ON THE LAY RTF
C   ANGLE2 - TILT ANGLE (DEG) - THAT IS, ANGLE BETWEEN TILTED LAYER AND A RTF
C           EXACTLY HORIZONTAL LAYER AT THE REFLECTION POINT RTF
C   RANG12 - DISTANCE FROM CENTER OF EARTH (KM) OF REFLECTION POINT USED RTF
C           COMPUTE ANGLE1+2 RTF
C   RTU-COMPUTED DISTANCE FROM CENTER OF EARTH IN KM. OF POINT OF INTERES RTF
C   RMU-DISTANCE FROM CENTER OF EARTH TO LAYER IN KM. RTF
C   PNTFLG-PENETRATION FLAG RTF
C           =0. REFLECTION RTF
C           =1. PENETRATION RTF
C           IMPLICIT DOUBLE PRECISION (A-H,O-Z) RTF
C           DOUBLE PRECISION M3000 RTF
C           DIMENSION RM(3),H(3),FC(3),RTM(3) RTF
C           COMMON/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAE,HME,HAF1,HMF1,HAF2,HMF2, RTF
C           1DUM(13),ID(3) RTF
C           COMMON/RTCOM/COSBO,NUSE RTF
C           DATA RAD/0.1745329251994330D-01/ RTF
C           DACOS(DUMMY)=DATAN2(DSQRT(1.000-DUMMY*DUMMY),DUMMY) RTF
C           PNTFLG=0.000 RTF
C           IF(NDFLAG)4,4,44 RTF
4.           IF(ANGLE2.EQ.0.000)GO TO 44 RTF
        WRITE(6,100)ANGLE2 RTF
100      FORMAT(2H THE VALUE OF ANGLE2 =,015.8,13H IS IN ERROR.) RTF
        PNTFLG=1.000 RTF
44      FC(1)=FCE RTF
        FC(2)=FCF1 RTF
        FC(3)=FCF2 RTF
        H(1)=HAE RTF
        H(2)=HAF1 RTF
        H(3)=HAF2 RTF
        RM(3)=6370.00+HMF2 RTF
        RM(2)=RM(3)-H(3) RTF
        RM(1)=RM(2)-H(2) RTF
        IF(NDFLAG.GT.0) GO TO 45 RTF
        COSBO=(DCOS(ANGLE1*RAD)*RANG12/6370.00) RTF
45      DO 10 N=1,3 RTF
C   COMPUTE RTM FOR EACH LAYER RTF
        IF(FC(N).EQ.0.0D0)GO TO 6 RTF
        FAC=(RM(N)**2)/16.00-(H(N)**2/2.00)*((FREQ/FC(N))**2-1.00) RTF
        IF(FAC)6,5,5 RTF
5.       RTM(N)=0.7500*RM(N)+DSQRT(FAC) RTF
        GO TO 10 RTF
6.       RTM(N)=RM(3) RTF
10      CONTINUE RTF
C   FIND MAX RTM RTF
        RMM=RTM(3) RTF
        IF(RTM(3).EQ.RM(3))RMM=RM(3)/2.0D0 RTF
3000    IF(NDFLAG.GT.0) GO TO 14 RTF

```

ROUTINE RTFIND 74/74 OPT=1

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C   IF ALL RTM ARE EQUAL, USE F2 LAYER           RTF
    IF(RTM(2).NE.RTM(3).OR.RTM(1).NE.RTM(3))GO TO 12  RTF
    NUSE=3  RTF
    RTMUSE=RTM(3)  RTF
    GO TO 14  RTF
C   FIND MINIMUM RTM  RTF
12    RTMUSE=RTM(1)  RTF
    NUSE=1  RTF
    DO 13 I=2,3  RTF
    IF(RTMUSE.LT.RTM(I))GO TO 13  RTF
    RTMUSE=RTM(I)  RTF
    NUSE=I  RTF
13    CONTINUE  RTF
    IF(NDFLAG.GT.0) GO TO 14  RTF
123   ANGLE1=(DACOS(COSB0*6370.00/RANG12))/RAD  RTF
C   USE PARAMETERS ASSOC. WITH MIN RTM  RTF
14    RTMUSE=RTM(NUSE)  RTF
    RMUSE=RM(NUSE)  RTF
    HUSE=H(NUSE)  RTF
    FCUSE=FC(NUSE)  RTF
144   CBTM=DCOS(ANGLE1*RAD)*RANG12/RTMUSE  RTF
    IF(CBTM-1.0D0)15,15,16  RTF
15    BTM=DACOS(CBTM)  RTF
17    X=1.0D0-((FREQ/FCUSE)**2)*((DSIN(BTM))**2)  RTF
    IF(X.GE.0.0D0)GO TO 20  RTF
16    IF(RTMUSE.NE.RM(3))GO TO 18  RTF
C   PENETRATION  RTF
185   RTU=RMM  RTF
    PNTFLG=1.0D0  RTF
    RMU=RM(3)  RTF
    RTMU=RTMUSE  RTF
2000  RETURN  RTF
18    IF(NUSE-3)19,185,185  RTF
C   ELIMINATE RTM USED AND FIND NEXT SMALLEST RTM  RTF
19    NUSE=NUSE+1  RTF
    GO TO 123  RTF
C   REFLECTION  RTF
20    RT=RTMUSE-HUSE*DSQRT(X)  RTF
    RMU=RMUSE  RTF
    RTMU=RTMUSE  RTF
    A=RMU-RT  RTF
    B=A/DCOS(ANGLE2*RAD)  RTF
    IF(B.GE.HUSE)B=HUSE  RTF
    RTU=RMU-B  RTF
    END  RTF

```

ROUTINE DENSE

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      SUBROUTINE DENSE(R,THETA,PHI,EN,DNDR,DNOT,DNDP)          DEN
C   R-DISTANCE FROM CENTER OF EARTH IN KM.                  DEN
C   THETA-NORTH LATITUDE IN DEGREES                         DEN
C   PHI-WEST LONGITUDE IN DEGREES                          DEN
C   EN-VALUE OF ELECTRON DENSITY AT GIVEN POINT           DEN
C   DNDR-PARTIAL DERIVATIVE OF ELEC. DEN. WITH RESPECT TO R  DEN
C   DNOT-PARTIAL DERIVATIVE OF ELEC. DEN. WITH RESPECT TO THETA  DEN
C   DNDP-PARTIAL DERIVATIVE OF ELEC. DEN. WITH RESPECT TO PHI  DEN
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)                      DEN
      DIMENSION RX(9),RY(9),ALPHA(9),FN(9)                      DEN
      COMMON/RPERT/RRIIP,ITIP                                DEN
      DATA RAD/.0174532925199433D0/                          DEN
10   RY(1)=R                                         DEN
      RX(1)=THETA*RAD                                     DEN
      ALPHA(1)=PHI*RAD                                    DEN
      NSIG=1                                         DEN
20   CALL DERV(NSIG,FN,RY,RX,ALPHA,DNDR,DNOT,DNDP)        DEN
      IF(NSIG.EQ.3) GO TO 30                           DEN
      DO 25 I=2,5                                     DEN
      CALL RIIP(RY(I),RX(I),ALPHA(I),FN(I))           DEN
      GO TO (22,23),ITIP                           DEN
22   CALL NFROMR(RY(I+4),FN(I+4))                     DEN
      GO TO 25                                         DEN
23   CALL RIIP(RY(I+4),RX(I+4),ALPHA(I+4),FN(I+4))        DEN
25   CONTINUE                                         DEN
      CALL RIIP(RY(1),RX(1),ALPHA(1),FN(1))           DEN
      NSIG=2                                         DEN
      GO TO 20                                         DEN
30   EN=FN(1)                                         DEN
      RETURN                                         DEN
      END                                         DEN

```

```

      SUBROUTINE DERV(NSIG,FN,RY,RX,ALPHA,DNDR,DNDT,DNOP)      DER
C  NSIG-SWITCH TO INDICATE WHETHER POINTS OR DERIVATIVES ARE REQUIRED DER
C  FN-ARRAY OF 9 VALUES OF ELEC. DEN.                               DER
C  RY-ARRAY OF 9 VALUES OF R IN KM.                                DER
C  RX-ARRAY OF 9 VALUES OF THETA IN RAD.                            DER
C  ALPHA-ARRAY OF 9 VALUES OF PHI IN RAD.                           DER
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)                          DER
      DIMENSION FN(9),RY(9),RX(9),ALPHA(9),DF(3)                 DER
      DATA S/1.0D0/                                              DER
      IF(NSIG-2)10G,200,200                                         DER
C FIND 8 POINTS ON CUBIC SURROUNDING RY(1),RX(1),ALPHA(1)      DER
100  X1=S/(0.17320508D+01)                                       DER
      X2=X1/RY(1)                                              DER
      C=RY(1)*DCOS(RX(1))                                       DER
      IF(C.EQ.0.0D0)C=100.0D0                                     DER
      X3=X1/C                                              DER
      DO 10 I=2,5                                              DER
      RY(I)=RY(1)+X1                                         L
      RY(I+4)=RY(1)-X1
10   CONTINUE
      DO 20 I=2,8,2                                         DER
      RX(I)=RX(1)+X2                                         DER
      RX(I+1)=RX(1)-X2                                         DER
20   CONTINUE
      DO 30 I=2,6,4                                         DER
      ALPHA(I)=ALPHA(1)+X3                                     DER
      ALPHA(I+1)=ALPHA(I)                                     DER
      ALPHA(I+2)=ALPHA(1)-X3                                     DER
      ALPHA(I+3)=ALPHA(I+2)                                     DER
30   CONTINUE
      RETURN
C FIND PARTIALS
200  AM=0.125000                                         DER
      DF(1)=AM*(FN(2)-FN(6)+FN(3)-FN(7)+FN(4)-FN(8)+FN(5)-FN(9)) DER
      DF(2)=AM*(FN(2)-FN(3)+FN(4)-FN(5)+FN(6)-FN(7)+FN(8)-FN(9)) DER
      DF(3)=AM*(FN(2)-FN(4)+FN(3)-FN(5)+FN(6)-FN(8)+FN(7)-FN(9)) DER
240  DNDR=DF(1)/X1                                         DER
      DNDT=DF(2)/X2                                         DER
      DNOP=DF(3)/X3                                         DER
      NSIG=3                                              DER
      RETURN
      END

```

Appendix C

Block Diagram, Flow Chart, and Program Listing for WIMP Driving Program OBLFACT

Explanation:

C1. OBLFACT BLOCK DIAGRAM

This presentation illustrates the communication and iteration network employed to generate the $M(3000)F_2$ and $f_0 F_2$ gradient correction factors required to match the predicted leading edge to the given oblique ionogram. The function of the various blocks is generally described as follows:

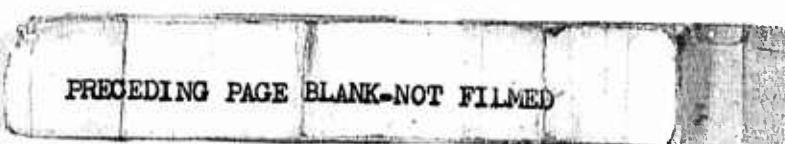
- BLOCK I: Initialization and Input Procedures.
- BLOCK II: Refinement of $M(3000)F_2$ Gradient Correction Factor.
- BLOCKS III and IV: Refinement of $f_0 F_2$ Gradient Correction Factor.
- BLOCK V: Termination and Output Procedures.

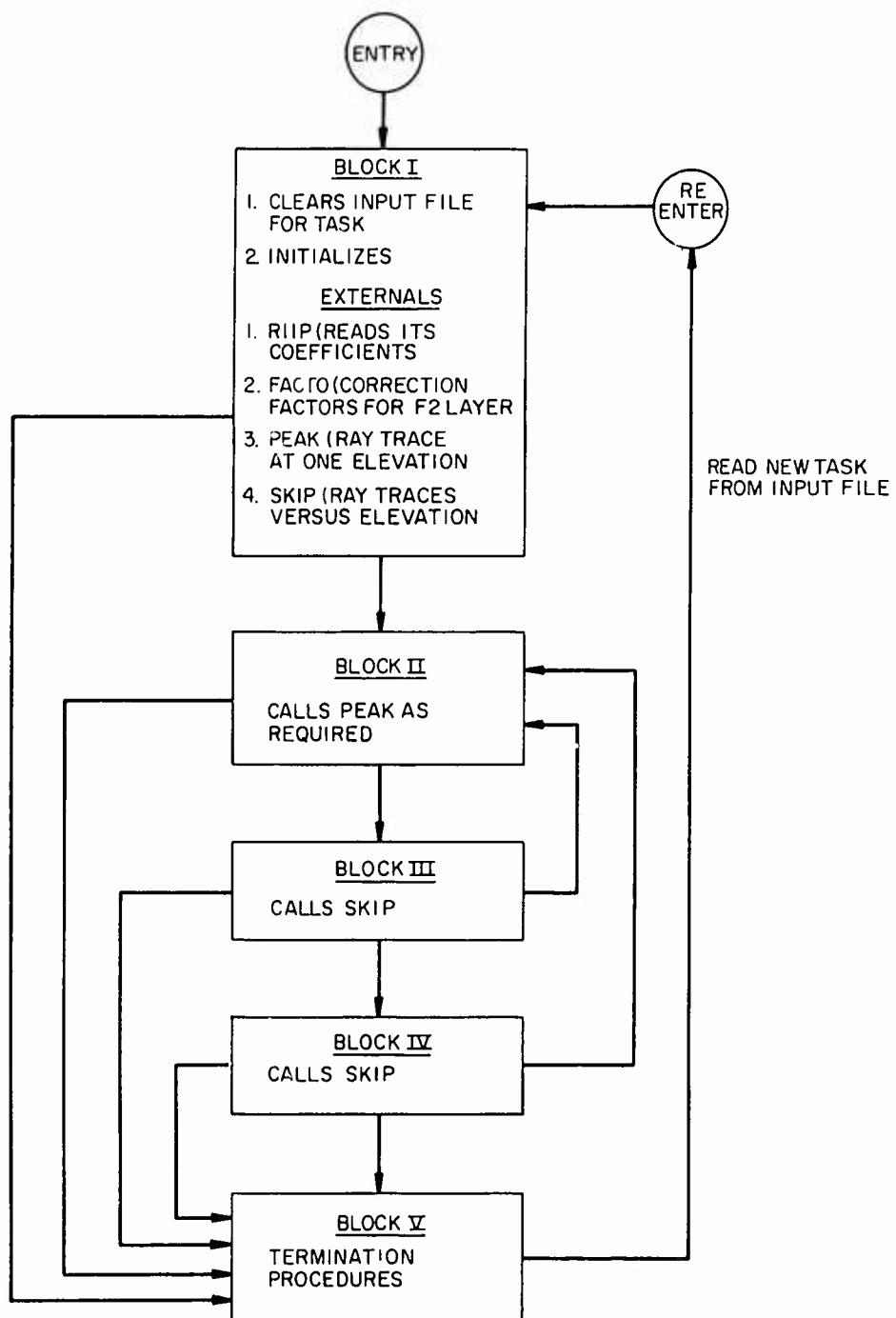
C2. DETAILED FLOW CHARTS

Detailed flow charts are presented for each block. Symbols and conventions are the same as described in Appendix A.

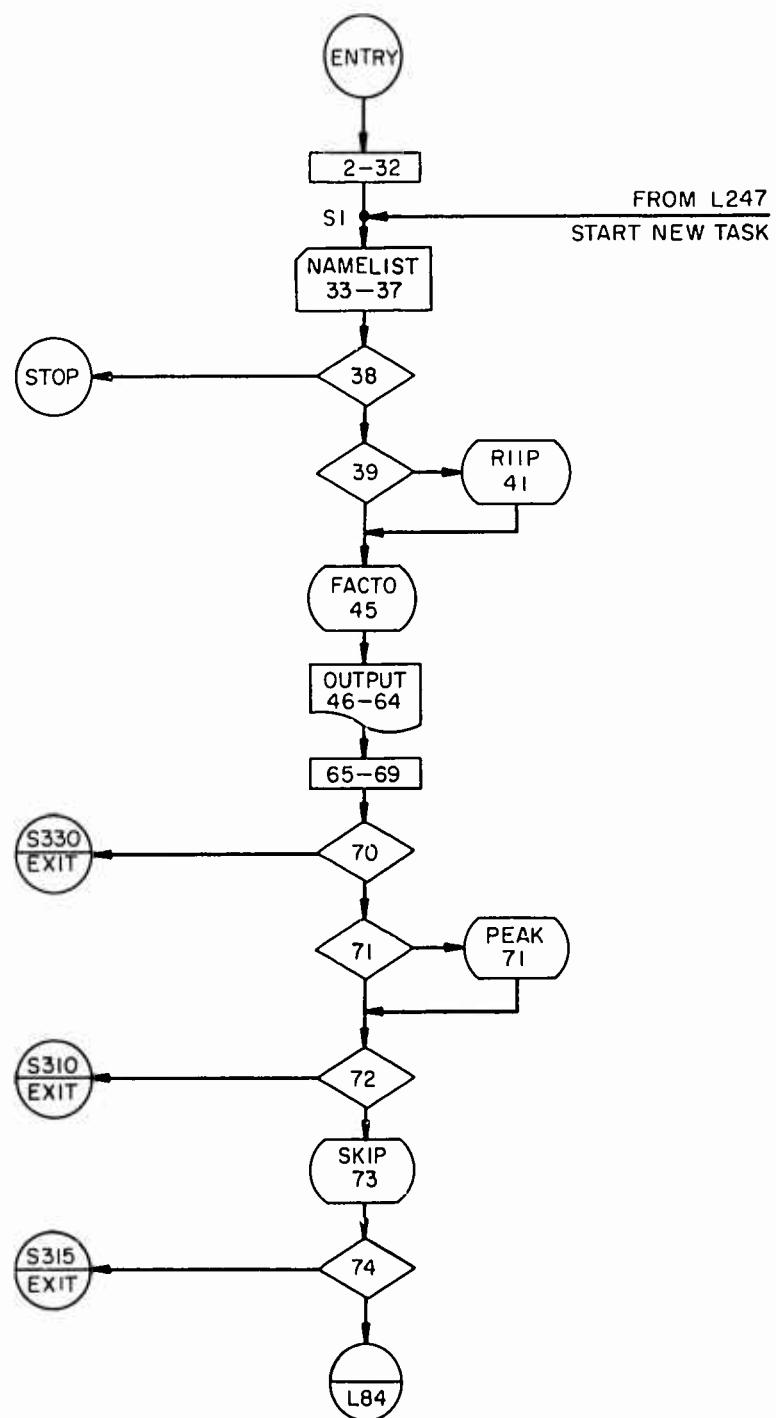
C3. PROGRAM LISTING

Listings are included for OBLFACT, PEAK, and SKIP.

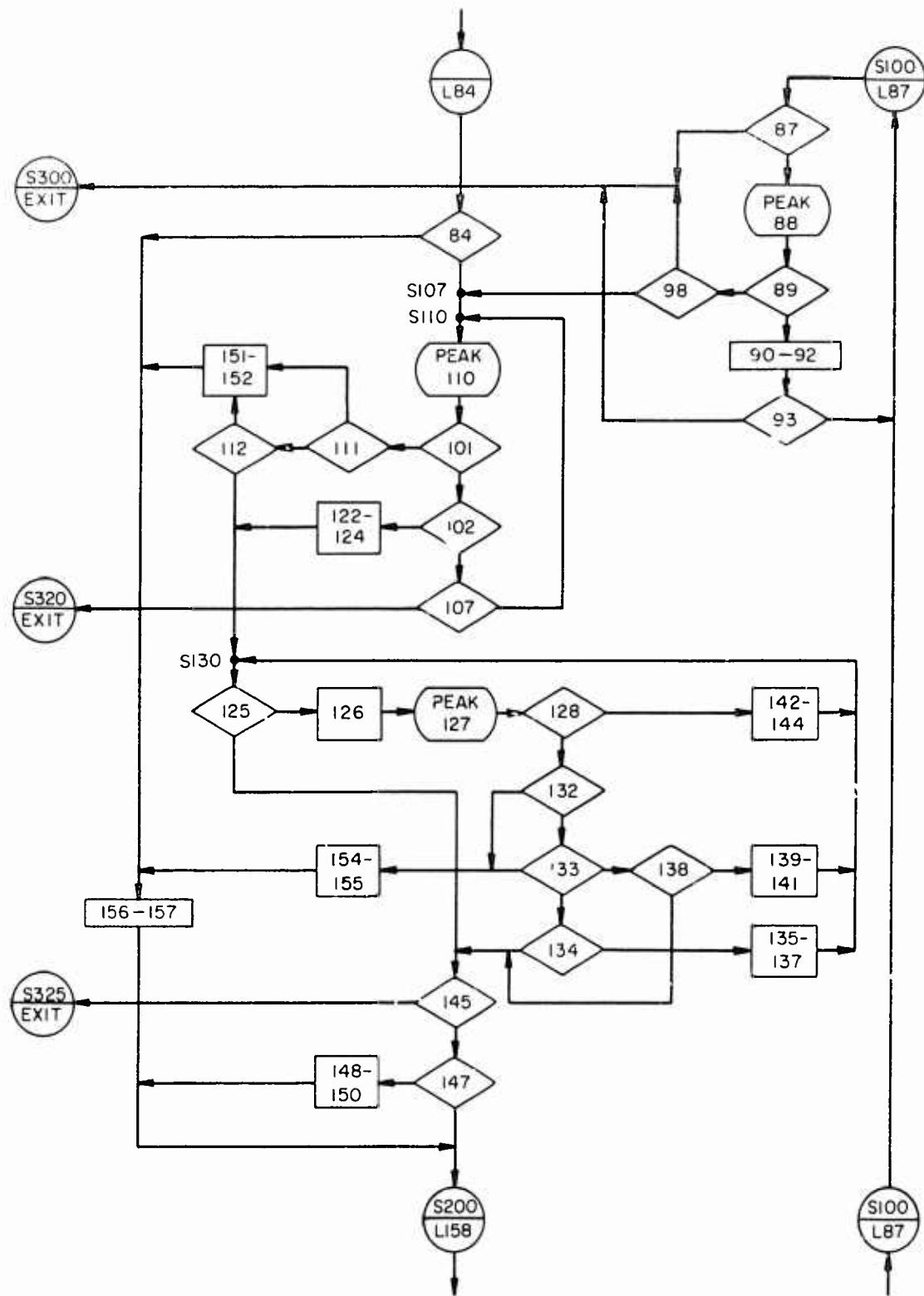




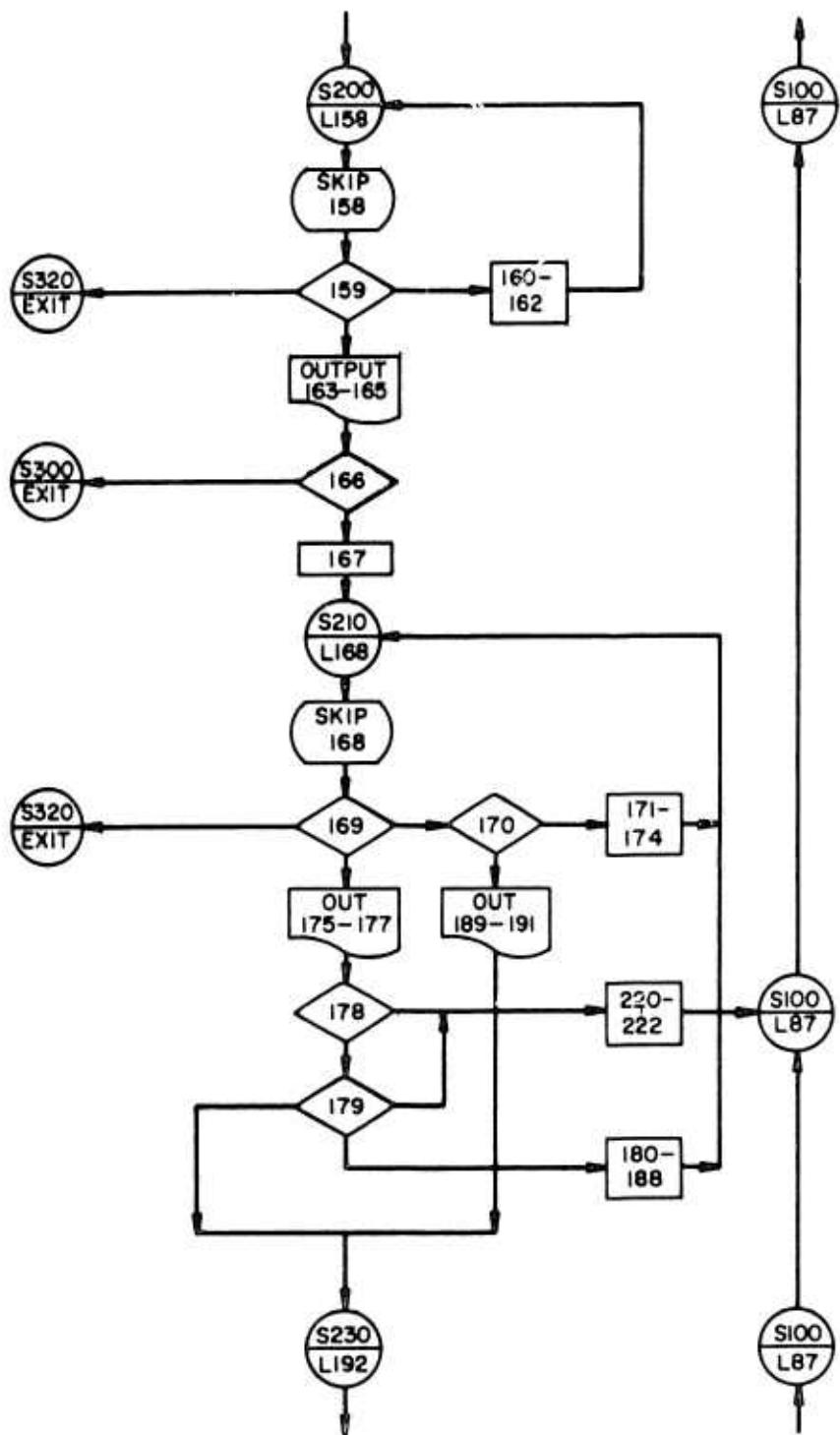
OBLFACT Block Diagram



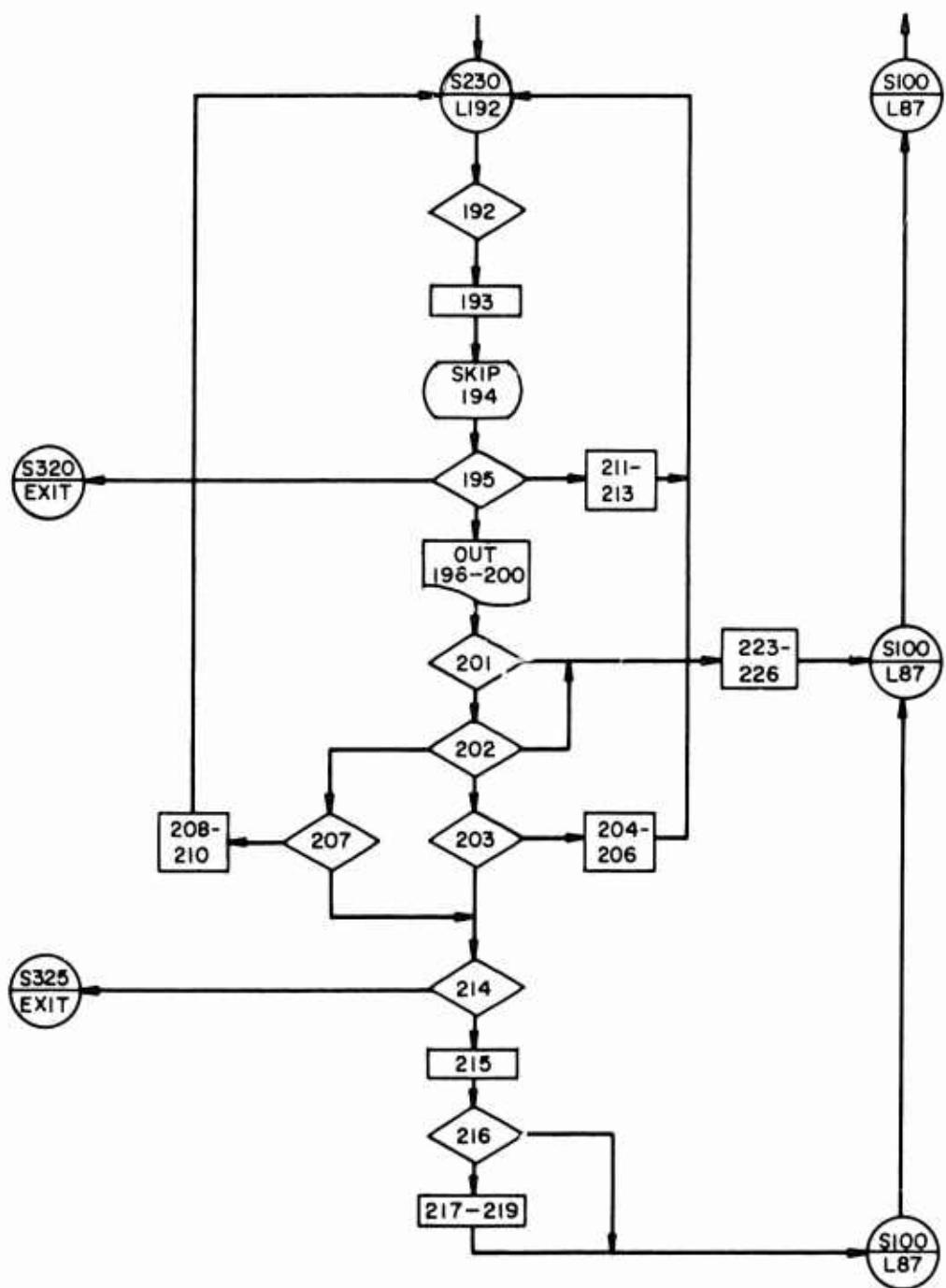
Block I, Detailed Flowchart



Block II, Detailed Flowchart



Block III, Detailed Flowchart



Block IV, Detailed Flowchart

ROUTINE OBL

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```

      SUBROUTINE OBL
C      PROGRAM OBLFACT(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)          OBL
      IMPLICIT DOUBLE PRECISION(A-H,M,O-Z)                            OBL
      INTEGER MODE                                                    OBL
      DOUBLE PRECISION NL1,NLREF                                     OBL
      LOGICAL SMOOTH,GPONLY                                       OBL
      COMMON/GPFLAG/GPONLY, IWRITE                                 OBL
      COMMON/FIDDLE/FP,FS,R1,NL1,HL1,AZ,RS,ELSTEP,MODE,NSKPCL    OBL
      COMMON/PERTC/NLREF, HLREF,PERTP(14)                           OBL
      COMMON/RIIPAR/DUM1(11),SN,ZT,YRMO,DOY,HAESET,MFAC,F2FAC,   OBL
      1 EFAC,H2FAC,DUM2(3),ID,IA,SMOOTH                           OBL
      NAMELIST/INPUT/SN,ZT,YRMO,DOY,MFAC,F2FAC,                 OBL
      1NL1,HL1,R1,NLREF,HLREF,RS,AZ,ELSTEP,MODE,                 OBL
      1FCF2R,HMINR,OCHK,FP,DELP,FS,DELS,MRO,FR0                 OBL
      3,IRSTRT,ZTREF                                           OBL
      IRSTRT=1                                                 OBL
      GPONLY=.TRUE.                                            OBL
      IWRITE=0                                                 OBL
      ID=1                                                   OBL
      TA=0                                                   OBL
      R1=6370.00                                             OBL
      RS=6370.00                                             OBL
      MODE=-1                                                OBL
      NL1=                                                   OBL
      HL1=                                                   OBL
      OCHK=10.00                                              OBL
      SN30=0.00                                              OBL
      NLREF=NL1                                              OBL
      HLREF=HL1                                              OBL
      AZ=                                                   OBL
      ELSTEP=1.00                                             OBL
      1 FR0=0.00                                              OBL
      MRO=0.00                                              OBL
      FP= 0.00                                              OBL
      DELP=0.00                                              OBL
      READ(5,INPUT)                                           OBL
      IF(IRSTRT.EQ.0) STOP                                     OBL
      IF(SN30.EQ.YRMO) GO TO 4                                OBL
      SN30=YRMO                                              OBL
      CALL RIIP(0.00,0.00,0.00,0.00)                           OBL
      4 IPKCNT=0                                              OBL
      FCF2R= DABS(FCF2R)                                       OBL
      HMINR= DABS(HMINR)                                       OBL
      CALL FACTO(NLREF,HLREF,FCF2R,HMINR,ZTREF)               OBL
CCCC  WRITE(6,INPUT)                                         OBL
      WRITE(6,900) SN,ZT,YRMO,DOY,MFAC,F2FAC                 OBL
      900 FORMAT(1X,[SN      =[,11X,D24.18/1X,[ZT      =[,11X,D24.18/
      *      1X,[YRMO    =[,11X,D24.18/1X,[DOY    =[,11X,D24.18/
      *      1X,[MFAC    =[,11X,D24.18/1X,[F2FAC =[,11X,D24.18)    OBL
      WRITE(6,901) NL1,HL1,R1,NLREF,HLREF,RS                  OBL
      901 FORMAT(1X,[NL1    =[,11X,D24.18/1X,[HL1    =[,11X,D24.18/
      *      1X,[R1      =[,11X,D24.18/1X,[NLREF =[,11X,D24.18/
      *      1X,[HLREF   =[,11X,D24.18/1X,[RS   =[,11X,D24.18)    OBL
      WRITE(6,902) AZ,ELSTEP,MODE,FCF2R,HMINR,OCHK            OBL
      902 FORMAT(1X,[AZ      =[,11X,D24.18/1X,[ELSTEP =[,11X,D24.18/
      *      1X,[MODE    =[,16X,I3      /1X,[FCF2R =[,11X,D24.18/
      *      1X,[HMINR   =[,11X,D24.18/1X,[OCHK =[,11X,D24.18)    OBL

```

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      WRITE(6,903)FP,DELP, FS,DELS, MR0,FR0          OBL
903  FORMAT(1X,[FP      =[,11X,024.18/1X,[DELP     =[,11X,024.18/
      *      1X,[FS      =[,11X,024.18/1X,[DELS     =[,11X,024.18/
      *      1X,[MR0      =[,11X,024.18/1X,[FR0     =[,11X,024.18)
      WRITE(6,904)IRSTRT,ZTREF                      OBL
904  FORMAT(1X,[IRSTRT =[,16X,I3      /1X,[ZTREF   =[,11X,024.18) OBL
      IM01=0                                         OBL
      IF01=0                                         OBL
      NSKpcl=0                                       OBL
      IGobak=0                                       OBL
      Gpp0=0.00                                       OBL
      IF(DABS(DELP).LT.DCHK.AND.DABS(DELS).LT.DCHK) GO TO 330 OBL
      IF(FP.GE.5.7400) CALL PEAK(FR0,MR0,GPP0,IGobak) OBL
      IF(IGobak.GT.0) GO TO 310                      OBL
      CALL SKIP(FR0,MR0,GPSS0,0,IGobak)              OBL
      IF(IGobak.GT.0) GO TO 315                      OBL
      GPPdes=GPP0+DELP                            OBL
      GPSSdes=GPSS0+DELS                          OBL
      WRITE(6,111) GPPdes,GPSSdes                  OBL
111   FORMAT(1  DESIRED GPP=[,4P015.2,1,  GPS=[,015.2) OBL
      DELP1=DELP                                     OBL
      DELS1=DELS                                     OBL
      DELP0=DELP                                     OBL
      DELS0=DELS                                     OBL
      MR1=MR0                                       OBL
      IF(DABS(DELP).LT.DCHK) GO TO 197             OBL
      GO TO 107                                     OBL
C MR FIDDLE
100   IF(FP.LT.5.7400) GO TO 300                  OBL
      CALL PEAK(FR0,MR0,GPP0,IGobak)              OBL
      IF(IGobak.EQ.0) GO TO 105                   OBL
      MR1=MR0                                       OBL
      MR0=MR1+.001D0                                OBL
      IPKcnt=IPKcnt+1                            OBL
      IF(IPKcnt-100) 100,320,320                  OBL
105   DELP0=GPPdes-GPP0                           OBL
      NSTMT=105                                     OBL
      WRITE(6,1111) NSTMT,FR0,MR0,DELP0           OBL
1111  FORMAT(I10,1P3D15.7)                      OBL
      IF(DABS(DELP0).LT.DCHK) GO TO 300             OBL
107   MR1=MR0-DSIGN(.001D0,DELP0)                OBL
110   CALL PEAK(FR0,MR1,GPP1,IGobak)              OBL
      IF(IGobak.EQ.0) GO TO 115                   OBL
      IF(DELP0.GT.0.00) GO TO 128                 OBL
      MR0=MR1                                       OBL
      MR1=MR0-DSIGN(.001D0,DELP0)                OBL
      DELP0=-10000.00                                OBL
      IPKcnt=IPKcnt+1                            OBL
      IF(IPKcnt-100) 110,320,320                  OBL
115   DELP1=GPPdes-GPP1                           OBL
      NSTMT=115                                     OBL
      WRITE(6,1111) NSTMT,FR0,MR1,DELP1           OBL
      IF(DABS(DELP1).LT.DCHK) GO TO 190             OBL
      IF(DELP1*DELP0) 130,190,120                  OBL
120   MRR=DELP1*(MR1-MR0)/(DELP0-DELP1)          OBL
      IF(DABS(MRR).GT.0.1D0) MRR=DSIGN(0.1D0,MRR) OBL
      MRR=MR1+MRR                                    OBL

```

ROUTINE OBL

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      IF(-DELP0.EQ.10000.D00.OR.(MR1-MRR)*DELP0.LE.0.D0)
1 MRR=MR1-DSIGN(.001D0,DELP1)          OBL
      MR0=MR1          OBL
      MR1=MRR          OBL
      DELP0=DELP1          OBL
      GO TO 110          OBL
128 DELP1=-10000.D0          OBL
      NSTMT=128          OBL
      WRITE(6,1111) NSTMT,FR0,MR1,DELP1          OBL
130 IF(DABS(MR1-MR0).LT..0001D0) GO TO 180          OBL
      MRR=(MR1+MR0)*.500          OBL
      CALL PEAK(FR0,MRR,GPPR,IGOBANK)          OBL
      IF(IGOBANK.GT.0) GO TO 160          OBL
      DELPR=GPPDES-GPPR          OBL
      NSTMT=130          OBL
      WRITE(6,1111) NSTMT,FR0,MRR,DELPR          OBL
      IF(DABS(DELPR).LT.DCHK) GO TO 195          OBL
      IF(DELPR*DELP0) 150,195,140          OBL
140 IF(DABS(DELPR).GT.DABS(DELP0)) GO TO 180          OBL
      DELP0=DELPR          OBL
      MR0=MRR          OBL
      GOTO 130          OBL
150 IF(DABS(DELPR).GT.DABS(DELP1)) GO TO 180          OBL
      DELP1=DELPR          OBL
      MR1=MRR          OBL
      GOTO 130          OBL
160 DELP1=-10000.D0          OBL
      MR1=MRR          OBL
      GO TO 130          OBL
180 IF(IM01*IF01.EQ.1) GOTO 325          OBL
      IM01=1          OBL
      IF(DABS(DELP1).GE.DABS(DELP0)) GO TO 200          OBL
      DELP0=DELP1          OBL
      MR0=MR1          OBL
      GOTO 200          OBL
190 MR0=MR1          OBL
      DELP0=DELP1          OBL
      GOTO 197          OBL
195 MR0=MRR          OBL
      DELP0=DELPR          OBL
197 IM01=0          OBL
C   FR FIDDLE          OBL
200 CALL SKIP(FR0,MR0,GP50,1,IGOBANK)          OBL
      IF(IGOBANK-1) 205,201,320          OBL
201 FR1=FR0          OBL
      FR0=FR1+.001D0          OBL
      GO TO 200          OBL
205 DELS0=GPSDES-GPS0          OBL
      NSTMT=205          OBL
      WRITE(6,1111) NSTMT,FR0,MR0,DELS0          OBL
      IF(DABS(DELS0).LT.DCHK) GO TO 300          OBL
      FR1=FR0-DSIGN(.001D0,DELS0)          OBL
210 CALL SKIP(FR1,MR0,GP51,1,IGOBANK)          OBL
      IF(IGOBANK-1) 215,211,320          OBL
211 IF(DELS0.GT.0.D0) GO TO 228          OBL
      FR0=FR1          OBL
      FR1=FR0-DSIGN(.001D0,DELS0)          OBL

```

ROUTINE OBL

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DELS0=-10000.00          OBL
GO TO 210                OBL
215 DELS1=GPSOES-GPS1    OBL
NSTMT=215                OBL
WRITE(6,1111) NSTMT,FR1,MRO,DELS1          OBL
IF(DABS(DELS1).LT.DCHK) GO TO 290          OBL
IF(DELS1*DELS0) 230,290,220                OBL
220 FRR=DELS1*(FR1-FR0)/(DELS0-DELS1)      OBL
IF(DABS(FRR).GT.0.1D0) FRR=DSIGN(0.100,FRR) OBL
FRR=FR1+FRR                  OBL
IF(-DELS0.EQ.10000.000.0R.(FR1-FRR)*DELS0.LE.0.00) OBL
1 FRR=FR1-DSIGN(.00100,DELS1)             OBL
FR0=FR1                  OBL
FR1=FRR                  OBL
DELS0=DELS1                OBL
GOTO 210                  OBL
228 DELS1=-10000.00          OBL
NSTMT=228                OBL
WRITE(6,1111) NSTMT,FR1,MRO,DELS1          OBL
230 IF(DABS(FR1-FR0).LT..000100) GO TO 280  OBL
FRR=(FR1+FR0)*.500            OBL
CALL SKIP(FRR,MRO,GPSR,1,IGOBANK)          OBL
IF(IGOBANK-1) 235,260,320                OBL
235 DELSR=GPSOES-GPSR                OBL
NSTMT=235                  OBL
WRITE(6,1111) NSTMT,FRR,MRO,DELSR          OBL
OBL

IF(DABS(DELSR).LT.DCHK) GO TO 295          OBL
IF(DELSR*DELS0) 250,295,240                OBL
240 IF(DABS(DELSR).GT.DABS(DELS0)) GO TO 280 OBL
DELS0=DELSR                OBL
FR0=FRR                  OBL
GOTO 230                  OBL
250 IF(DABS(DELSR).GT.DABS(DELS1)) GO TO 280 OBL
DELS1=DELSR                OBL
FR1=FRR                  OBL
GOTO 230                  OBL
260 DELS1=-10000.00          OBL
FR1=FRR                  OBL
GO TO 230                  OBL
280 IF(IM01*IF01.EQ.1) GO TO 325          OBL
IF01=1                    OBL
IF(DABS(DELS1).GE.DABS(DELS0)) GO TO 100  OBL
DELS0=DELS1                OBL
FR0=FR1                  OBL
GOTO 100                  OBL
290 FR0=FR1                OBL
DELS0=DELS1                OBL
GOTO 297                  OBL
295 FR0=FRR                OBL
DELS0=DELSR                OBL
297 IF01=0                  OBL
GOTO 100                  OBL
300 WRITE(6,305) MRO,FR0,DELPO,DELS0          OBL
305 FORMAT(0 CONVERGENT VALUES\ MR=[,1PD15.7,], FR=[,015.7/ OBL
1 10X,I MISS DIST. PEAK=[,010.3,], SKIP=[,010.3]) OBL

```

ROUTINE OBL

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GOTO 1	OBL
310 WRITE(6,312)	OBL
312 FORMAT([0 PEAK RAYTRACE FAILS ON INPUT CASE, TRY DIFFERENT INPUT()	OBL
GOTO 1	OBL
315 WRITE(6,317)	OBL
317 FORMAT([0 SKIP RAYTRACES FAIL ON INPUT CASE, TRY DIFFERENT INPUT()	OBL
GOTO 1	OBL
320 WRITE(6,322)	OBL
322 FORMAT([0 100 ITERATIONS DONE BUT DOESN'T CONVERGE, [OBL
1[TRY DIFFERENT INPUT()	OBL
GOTO 300	OBL
325 WRITE(6,327)	OBL
327 FORMAT([0 CONVERGENCE PROBLEMS, TRY DIFFERENT INPUT()	OBL
GOTO 300	OBL
330 WRITE(6,332)	OBL
332 FORMAT([0 YOUR ORIGINAL INPUT CONVERGES()	OBL
GOTO 1	OBL
END	OBL

OUTINE SKIP

74/74 OPT=1

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```

SUBROUTINE SKIP(FRR,MRR,GP,IOPT,IGOBK)          SKI
IMPLICIT DOUBLE PRECISION (A-H, O-Z)          SKI
REAL OUT(3)          SKI
DOUBLE PRECISION MRR,MR,NL1,NLT,NLREF,GP(42),RS2(42)  SKI
COMMON/PERTC/NLREF,HLREF,FR,FD,MR,DUM(11)  SKI
COMMON/FIDDLE/FP,FS,R1,NL1,HL1,AZ,RS,ELSTEP,MODE,NSKPCL  SKI
COMMON/REMHEN/INUSE,NNUSE(20),FCREF(20)  SKI
NSKPCL=NSKPCL+1          SKI
IF(NSKPCL.GT.100) GO TO 120          SKI
IGOBK=0          SKI
NELM=20.00/ELSTEP+1.00          SKI
FR=FRR          SKI
MR=MRR          SKI
DO 10 IEL=1,NELM          SKI
EL=(IEL-1)*ELSTEP          SKI
CALL TRISL(R1,NL1,HL1,AZ,EL,0.00,FS,MODE,RS,RS2IEL),NLT,HLT,  SKI
1PP,GPIEL,AZF,ELF,SRANGE,ELSR,DIST,BEAR,IRETNR)  SKI
IF(IRETNR-1) 6,8,12          SKI
6 DO 7 I=1,INUSE          SKI
IF(NNUSE(I).NE.3) GO TO 8          SKI
7 CONTINUE          SKI
GO TO 10          SKI
8 RS2IEL=1.020          SKI
GPIEL=1.020          SKI
10 CONTINUE          SKI
IEL=NELM+1          SKI
12 IFIEL.EQ.1) GO TO 110          SKI
RS2IEL=1.020          SKI
NELM=IEL-1          SKI
IMIN=1          SKI
IF=0          SKI
DO 20 IEL=1,NELM          SKI
IF(RS2IEL .GT.6378.85D0) GO TO 20          SKI
IF=1          SKI
IF(GPIEL.LT.GPIMIN) IMIN=IEL          SKI
20 CONTINUE          SKI
IF(IF.EQ.0) GO TO 110          SKI
GPS=GPIMIN          SKI
IF(IOPT.EQ.0) GO TO 130          SKI
IF(RS2IMIN+1).LT.6378.85D0) GO TO 130          SKI
IF(RS2IMIN+1).GE.0.9D20) GO TO 130          SKI
IF(GPIMIN+1).GT.GPIMIN) GO TO 130          SKI
GPS=GPIMIN+(GPIMIN+1)-GPIMIN)*(6378.85D0-RS2IMIN))/  SKI
1(RS2IMIN+1)-RS2IMIN)          SKI
GO TO 130          SKI
110 IGOBK=1          SKI
GO TO 130          SKI
120 IGOBK=2          SKI
130 OUT(1)=FR          SKI
OUT(2)=MR          SKI
OUT(3)=GPS          SKI
WRITE(6-140) OUT,IGOBK          SKI
140 FORMAT(1 SKIP,2F10.6,F10.2,I5)          SKI
RETURN          SKI
END          SKI

```

ROUTINE PEAK

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```
SUBROUTINE PEAK(FRR,MRR,GPP,IGOBAK)          PEA
IMPLICIT DOUBLE PRECISION(A-H,O-Z)          PEA
REAL OUT(3)          PEA
DOUBLE PRECISION MRR,NL1,NLT,ELP(25),NLREF,MR          PEA
COMMON/PFRTC/NLREF,HLREF,FR,FD,MR,DUM(11)          PEA
COMMON/FIDOLE/FP,FS,R1,NL1,HL1,AZ,RS,ELSTEP,MODE,NSKPCL          PEA
COMMON/REMWEN/INUSE,NNUSE(20),FCREF(20)          PEA
DATA ELP/11.900,10.3D0,8.900,7.7D0,6.7D0,5.900,5.2D0,4.6D0,          PEA
1 4.1D0,3.9D0,5.2D0,4.8D0,4.5D0,4.2D0,4.0D0,3.8D0,2*3.7D0,          PEA
2 2*3.6D0,3*3.5D0,2*3.4D0/          PEA
FR=FRR          PEA
MR=MRR          PEA
IF=FP-4.74D0          PEA
CALL TRISL(R1,NL1,HL1,AZ,ELP(IF),0.0D0,FP,MODE,RS,          PEA
1RS2,NLT,HLT,PP,GPP,AZF,ELF,SRANGE,ELSR,DIST,BEAR,IGOBAK)          PEA
IF(RS2.GT.6378.85D0) IGOBAK=1          PEA
DO 1 I=1,INUSE          PEA
IF(NNUSE(I).NE.3) IGOBAK=1          PEA
1 CONTINUE          PEA
OUT(1)=FR          PEA
OUT(2)=MR          PEA
OUT(3)=GPP          PEA
WRITE(6,11) OUT,IGOBAK          PEA
11 FORMAT(1 PEAK[,2F10.6,F10.2,I5)          PEA
RETURN          PEA
END          PEA
```